



# Effect of Negative Stress Ratio Testing and Characterization on Damage Tolerance Life Predictions

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# Overview

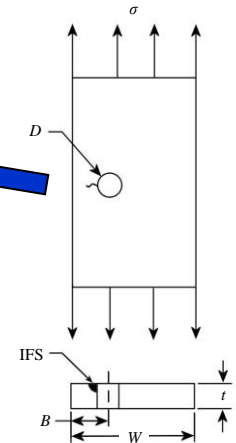
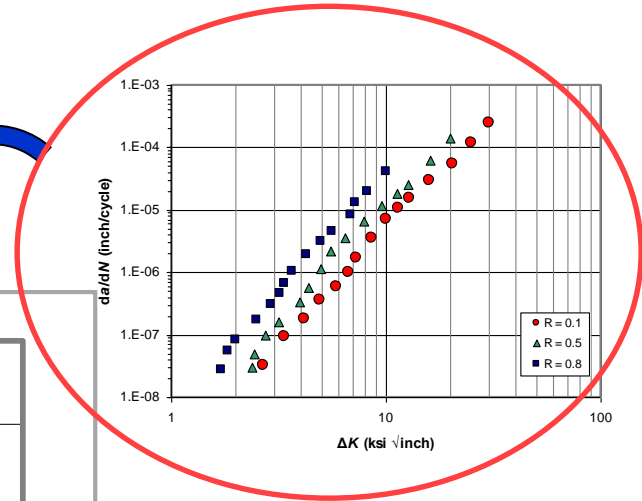
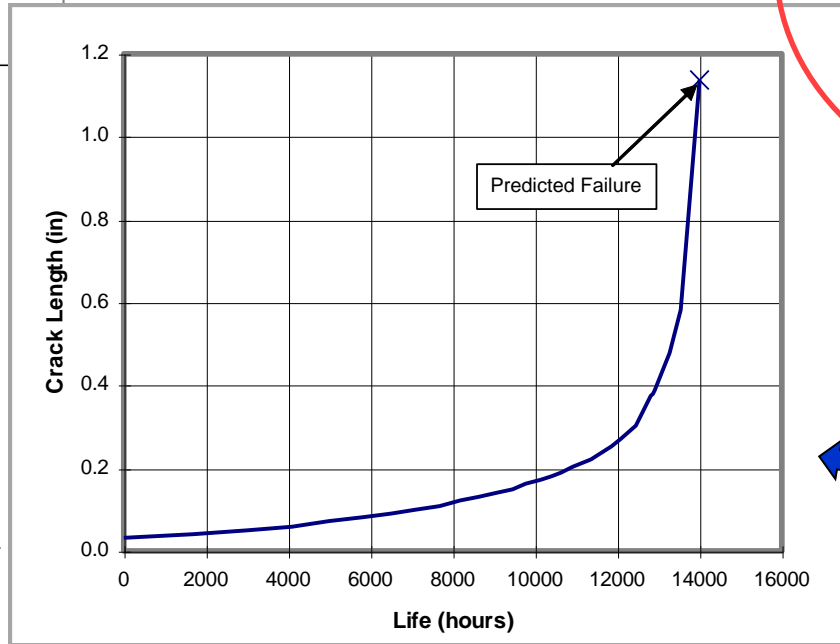
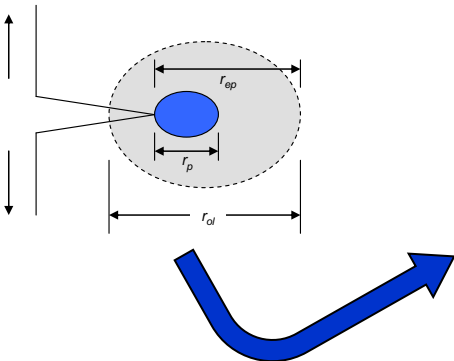
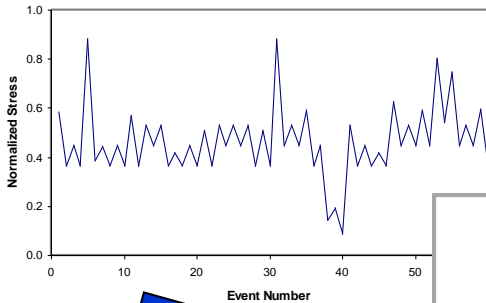
- Background
  - Generalized Willenborg,  $R_{\text{eff}}$
- Objective
- Material Curve Fitting Process for  $da/dN$
- Determination of  $R_{I_0}$
- Conclusions



# Background

## ■ Damage Tolerance Analysis

$$a_n = a_i + \sum_{j=1}^n da_j$$

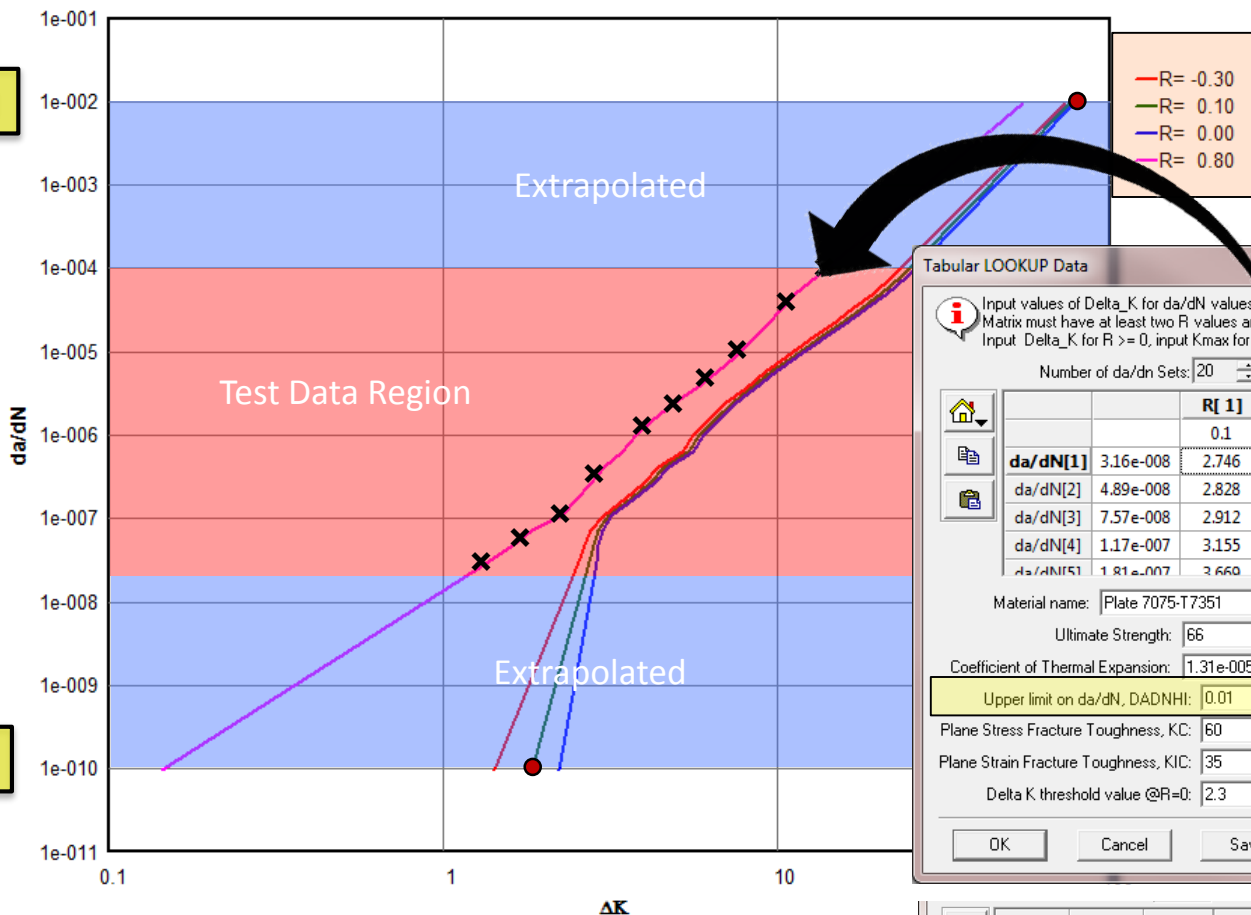


(see *Stress Ratio Influence on da/dN with the Generalized Willenborg Model* by King, 2016 AFGROW Workshop)



# Background (cont.)

### Crack Growth Rate Data



**Tabular LOOKUP Data**

Input values of Delta\_K for da/dN values and up to 10 different R(stress ratio) values. Matrix must have at least two R values and two da/dN values. Input Delta\_K for R >= 0, input Kmax for R < 0.0

Number of da/dn Sets: 20      Number of R Sets: 2

	R[ 1]	R[ 2]
da/dN[1]	2.746	1.367
da/dN[2]	2.828	1.621
da/dN[3]	2.912	1.863
da/dN[4]	3.155	2.272
da/dN[5]	3.660	2.577

Material name: Plate 7075-T7351

Ultimate Strength: 66      Young's Modulus: 10400

Coefficient of Thermal Expansion: 1.31e-005      Poisson's Ratio: 0.33

Upper limit on da/dN, DADNHI: 0.01      Lower limit on da/dN, DADNLO: 1e-010

Plane Stress Fracture Toughness, KC: 60      Yield Strength, YLD: 57

Plane Strain Fracture Toughness, KIC: 35      Lower limit on R shift (Max: 0): -0.3

Delta K threshold value @R=0: 2.3      Upper limit on R shift (0, 1): 0.8

OK      Cancel      Save      Read      Apply

Note: For R < 0.0, Kmax is used instead of Delta K

	R[ 1]	R[ 2]
da/dN[17]	17.9038	10.408
da/dN[18]	20.6614	11.4263
da/dN[19]	23.4389	13.159
da/dN[20]	26.0663	14.977



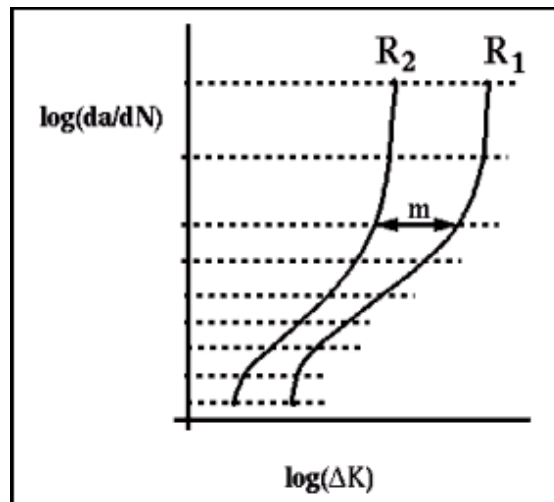
# Background (cont.)

## ■ Harter-T Method

- Shifts  $da/dN$  curves for any  $R$
- Applies Walker Equation (point-by-point basis)

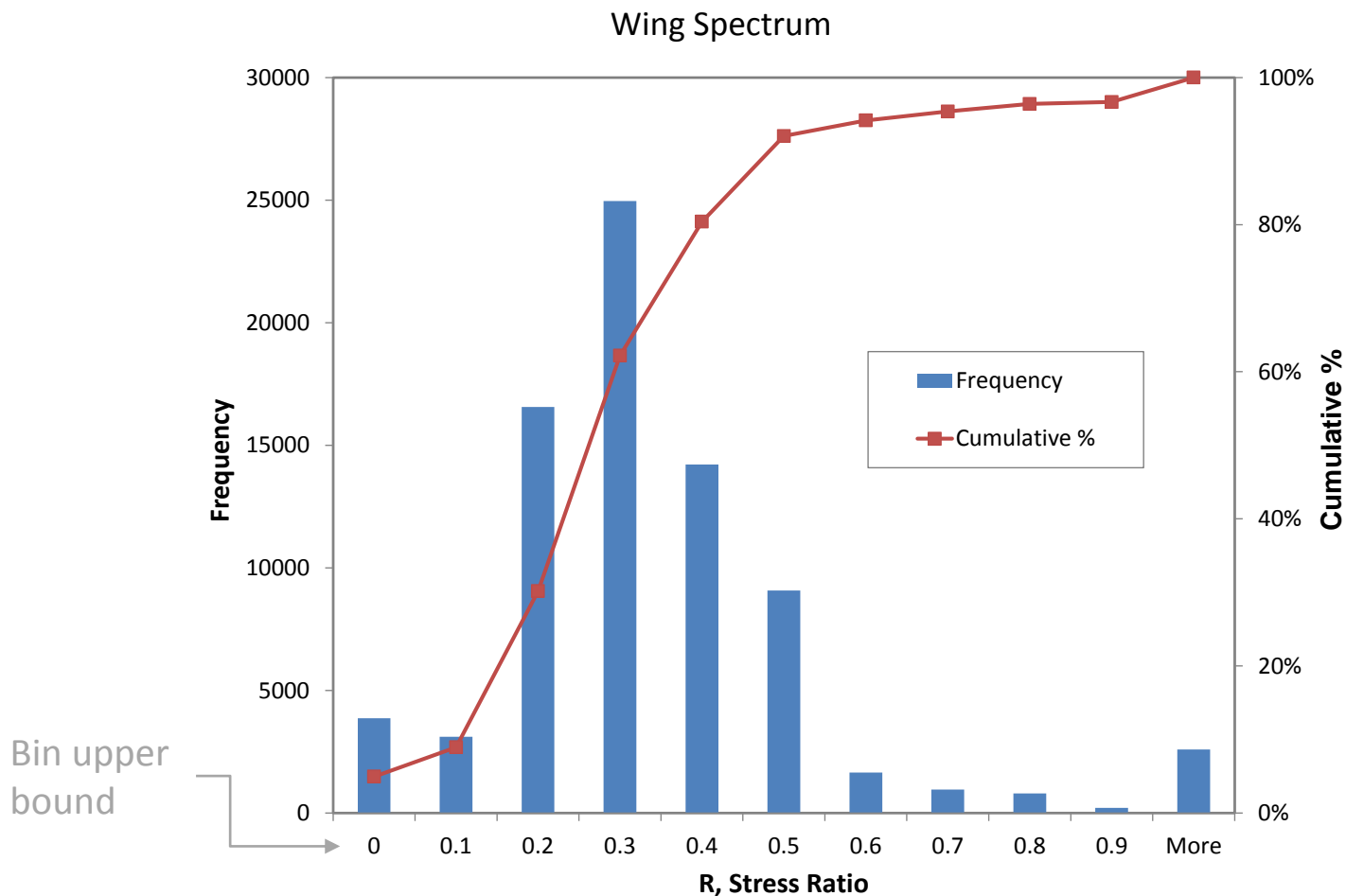
For a given crack growth rate:

$$\Delta K_1 (1 - R_1)^{(m-1)} = \Delta K_2 (1 - R_2)^{(m-1)} \quad (\text{When, } R_1 \text{ \& } R_2 > 0)$$





# Stress Ratio ( $R$ ) Histogram



**When using the Generalized Willenborg Model, this is NOT the  $R$  that is used to determine  $da/dN$**



# Generalized Willenborg Model

- Adjusts  $da/dN$  by reducing  $R$  to  $R_{eff}$

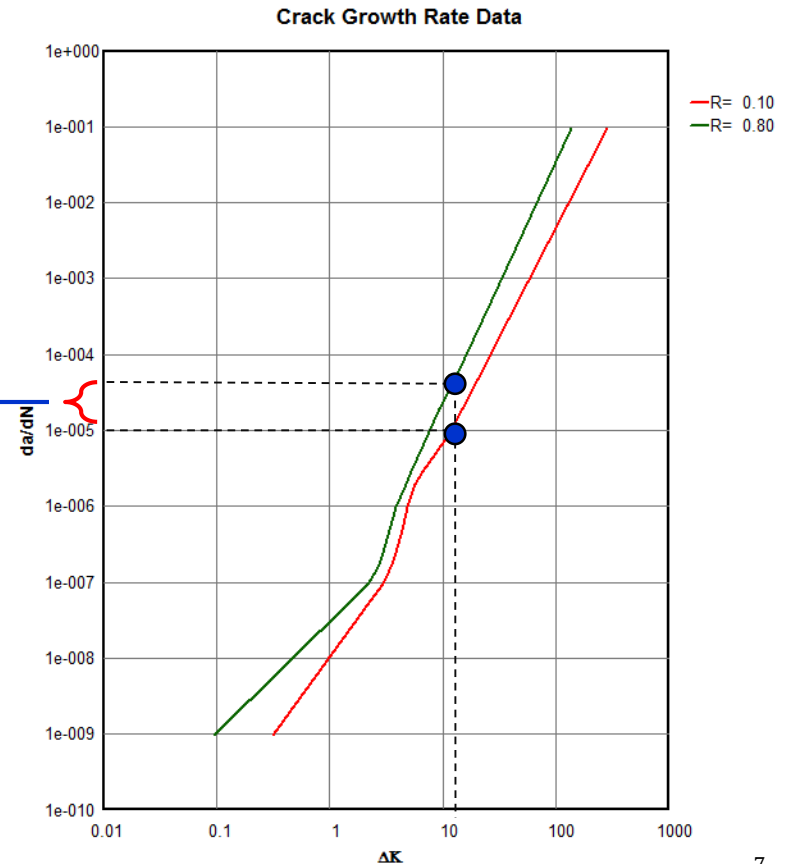
$$K_r = \frac{1 - \frac{\Delta K_{th}}{K_{max}}}{(SOLR - 1)} \left[ K_{OL} \sqrt{1 - \frac{x - x_{OL}}{r_{OL}}} - K_{max} \right]$$

$$K_{min,eff} = K_{min} - K_r$$

$$K_{max,eff} = K_{max} - K_r$$

$$R_{eff} = \frac{K_{min,eff}}{K_{max,eff}}$$

Retardation Effect:  
Reduction in  $da/dN$

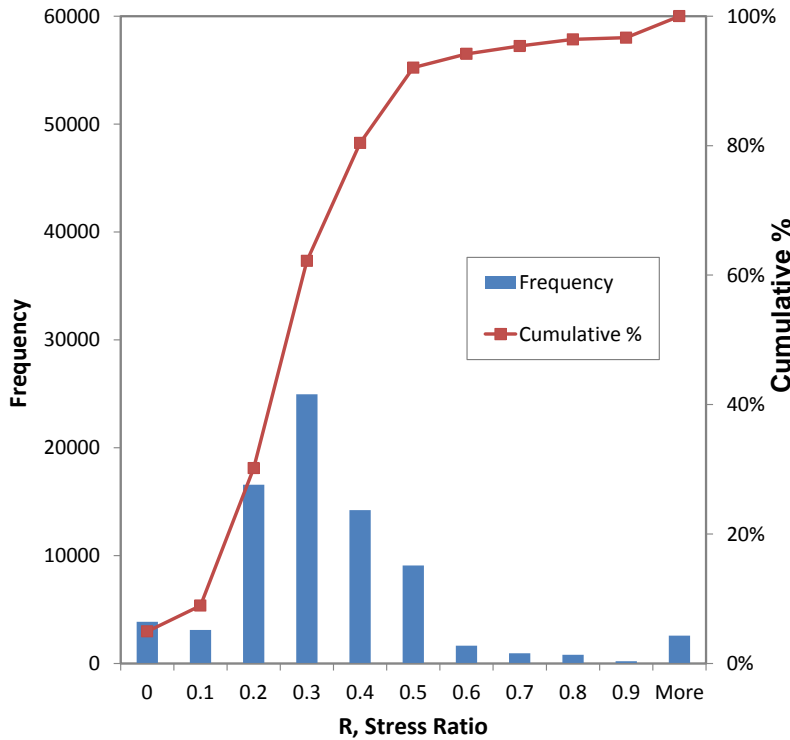


Note: For  $R < 0.0$ ,  $K_{max}$  is used instead of Delta K

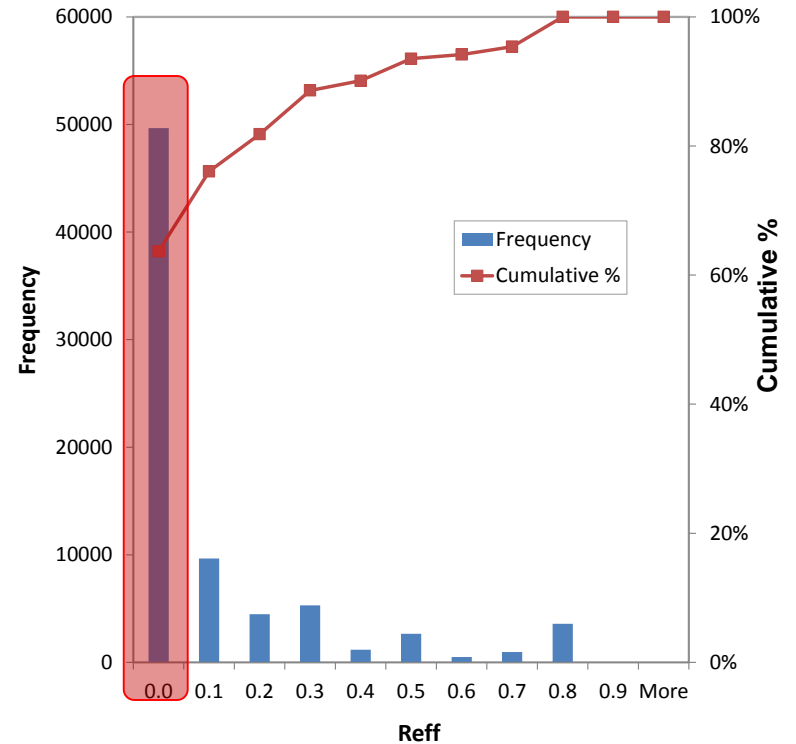


# $R$ vs $R_{eff}$

## Wing Spectrum



### $R$ , Stress Ratio



### $R_{eff}$ , Effective Stress Ratio

Accounts for > 50% of crack growth  
(based on multiple wing details)

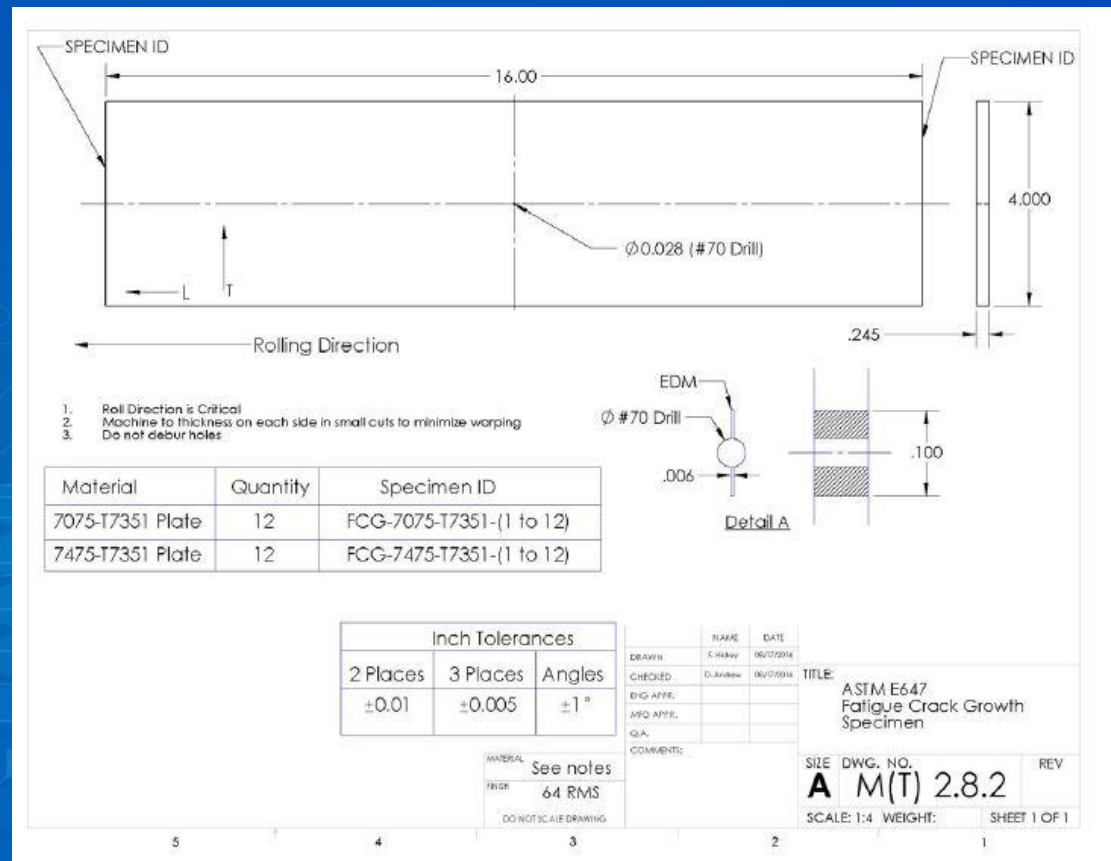


# Test Program Objectives

- Perform da/dN (E647) Tests for Negative R
  - 7075-T735 I
  - 7475-T735 I
  - 7075-T735 II
  - 4130
- Create Curve Fits to Test Data for Negative R
  - How does that compare with the extrapolation of positive R?
- Determine  $R_{10}$ 
  - How does this compare to default value previously used?
- What is the effect of the updated material model (da/dN fits and  $R_{10}$ ) on the crack growth life predictions for FCLs?

# da/dN Testing

## ■ ASTM E647 Specimen Geometry – M(T)



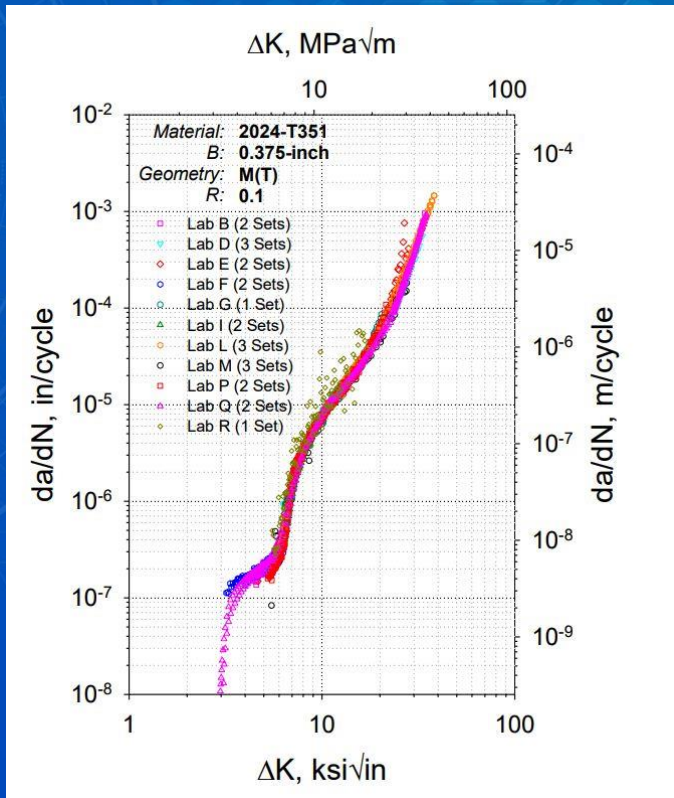
Material	R = -0.1	R = -0.2	R = -0.3	R = -0.5	R = -1
7075-T7351	3	0	3	3	3
7475-T7351	3	0	4	3	2
7075-T735111	0	6	0	5	0
4130	0	4	0	2	0

# da/dN Curve Fitting Process

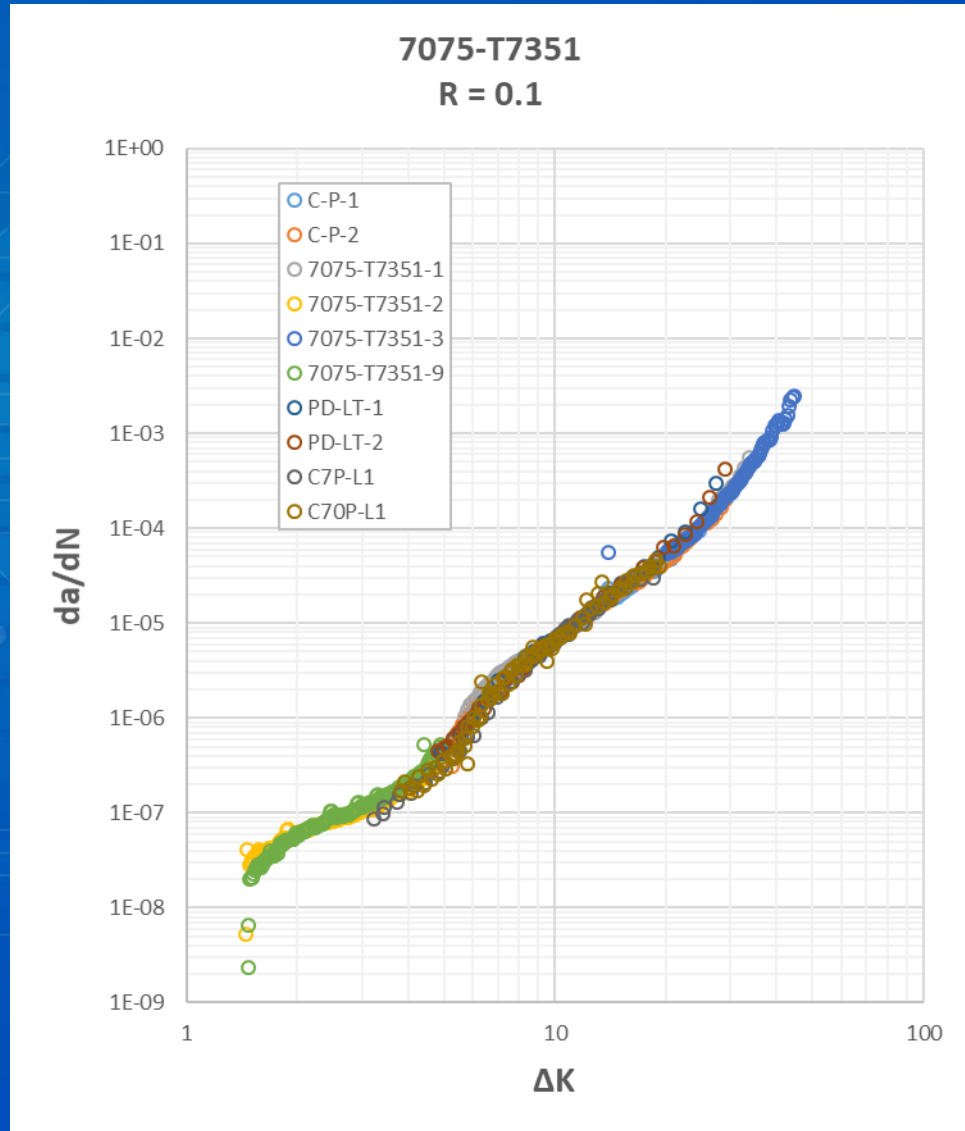
- 2017 AFGROW, *Stress Ratio Influence on da/dN...Updated Material Data & Fitting Process* – Bob Pilarczyk, Dallen Andrew
- Harter-T Method
  - Fitting data on a point-by-point basis
  - Interpolations in  $\Delta K$  and R via point-by-point Walker equation
  - Captures curvature, permits different amount of shifting for different regimes of curve
- Goals
  - Match test data
  - Smooth m-curves (ensure quality of interpolation)
  - Develop fit across range of available data, preferably from  $\Delta K_{th}$  to  $\Delta K_c$

# Fitting +R

- Variation within lot is relatively small at a given load ratio, given geometry

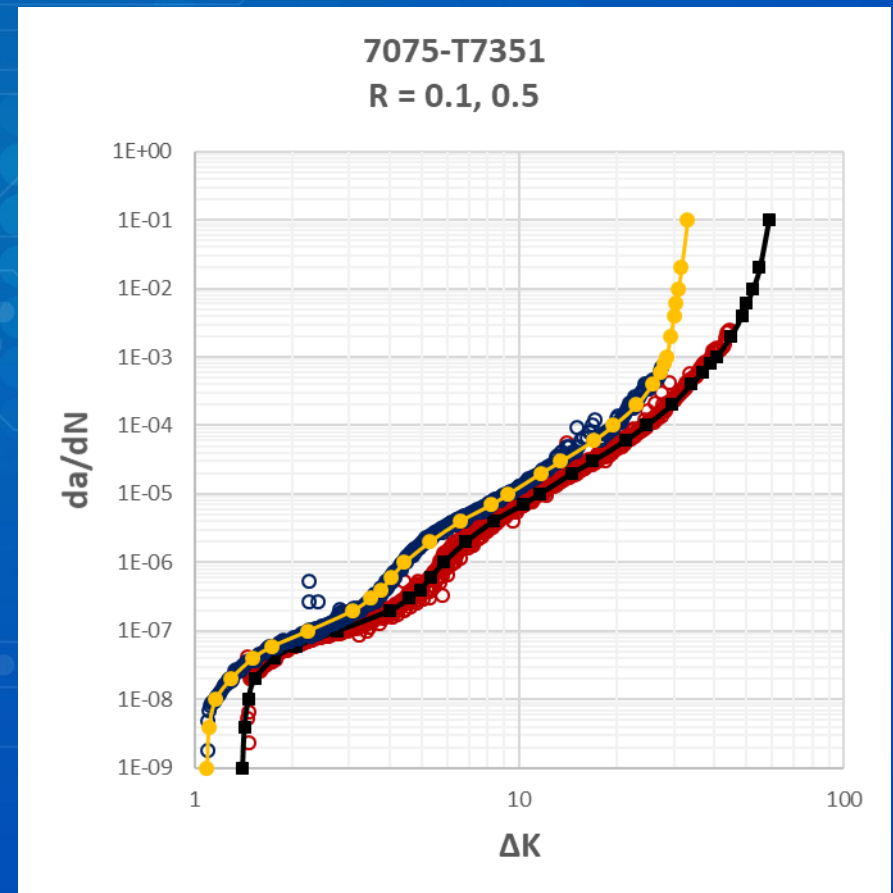
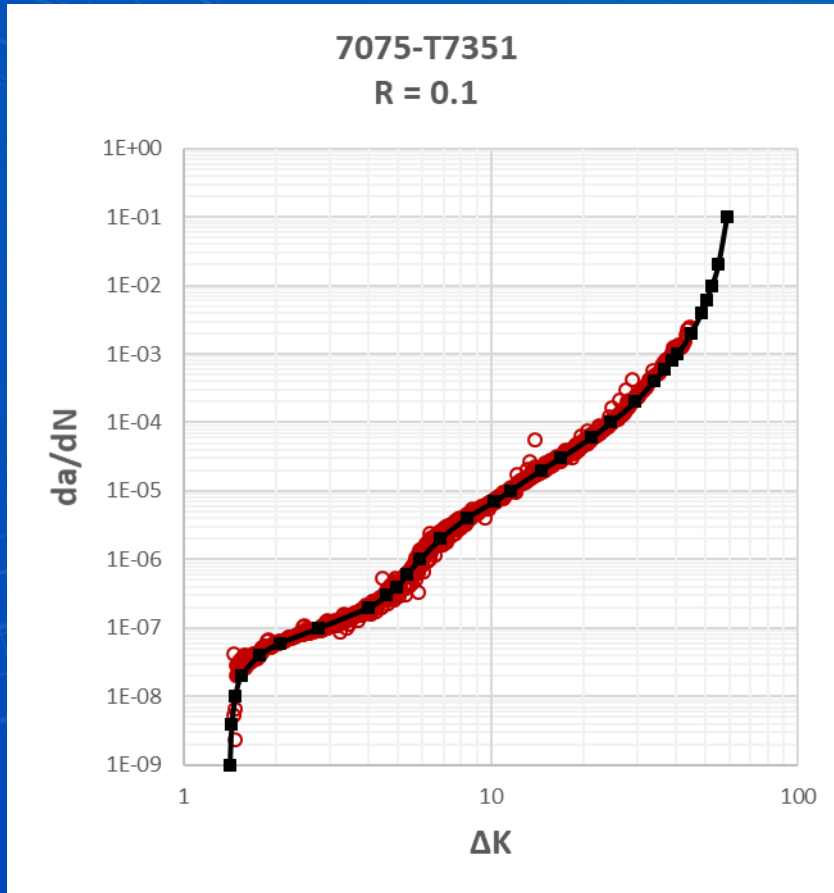


ASTM E647  
 Round Robin  
 Results

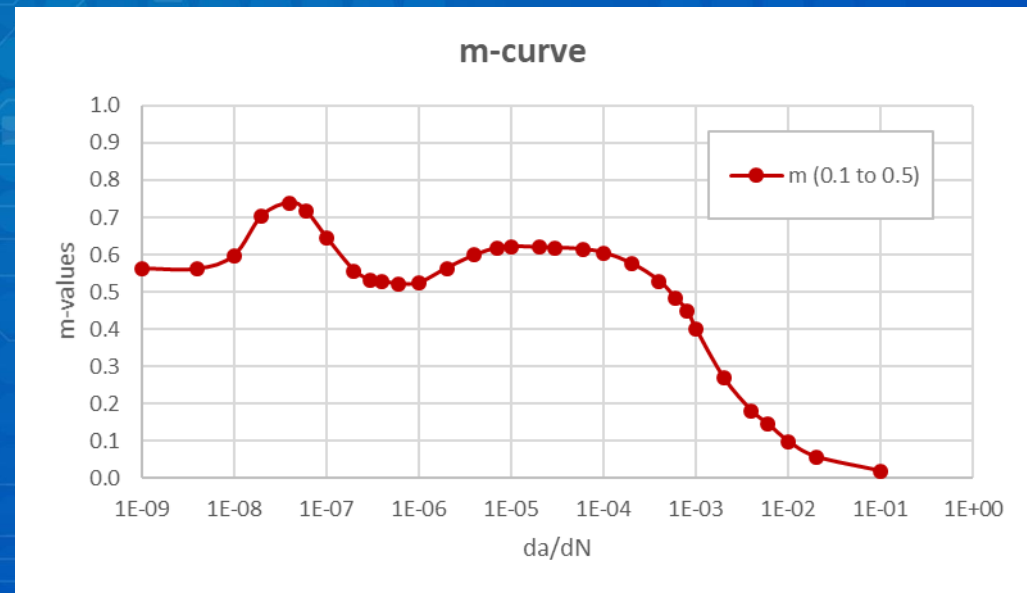
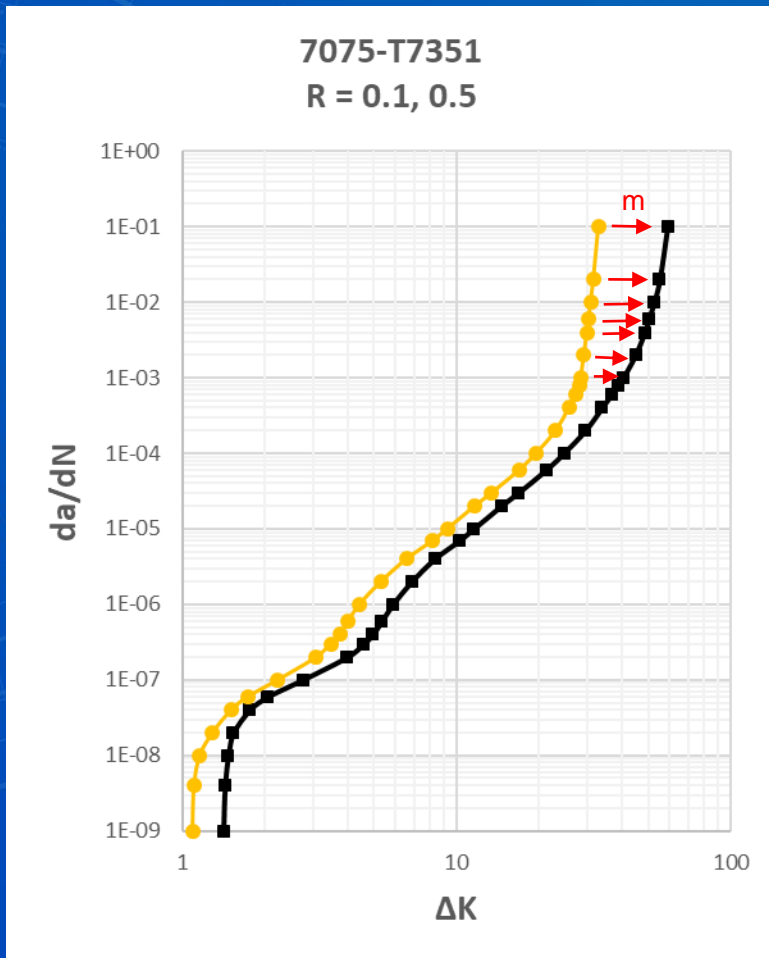


# Harter-T Method

- Fitting data on a point-by-point basis

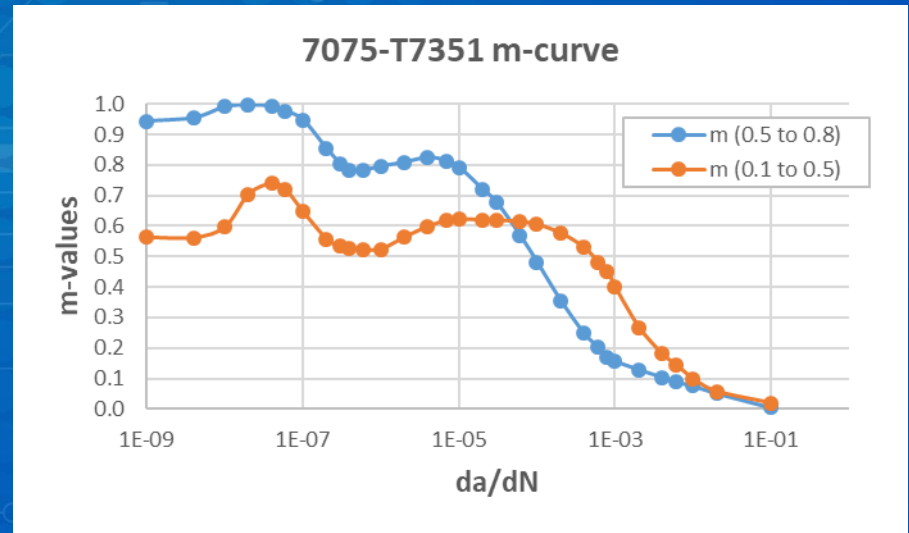
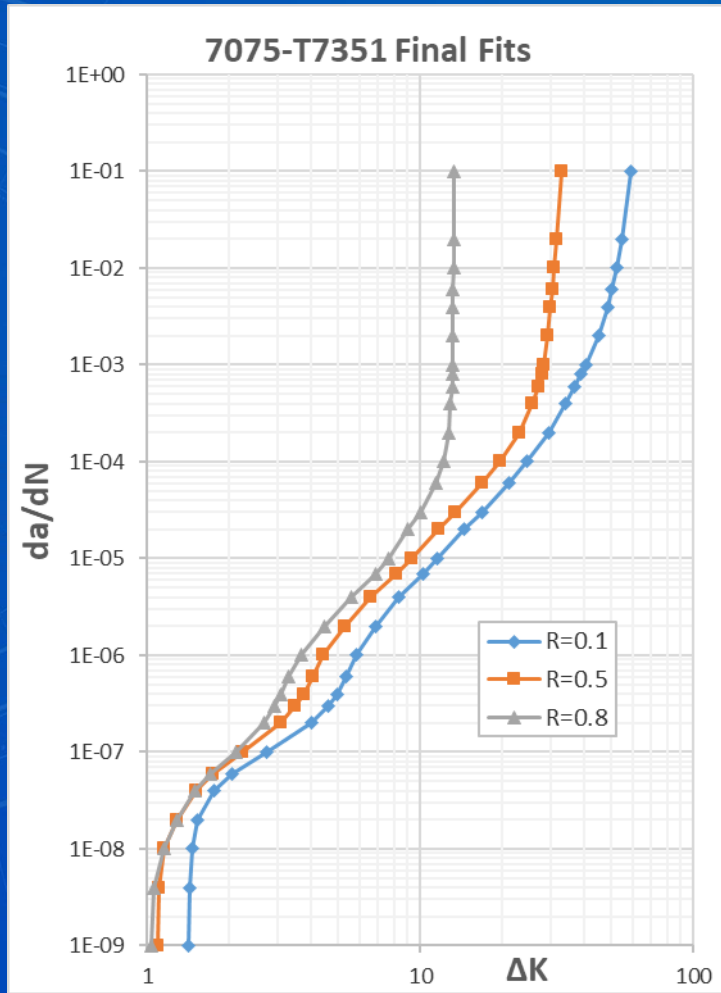


# Creating m-curves



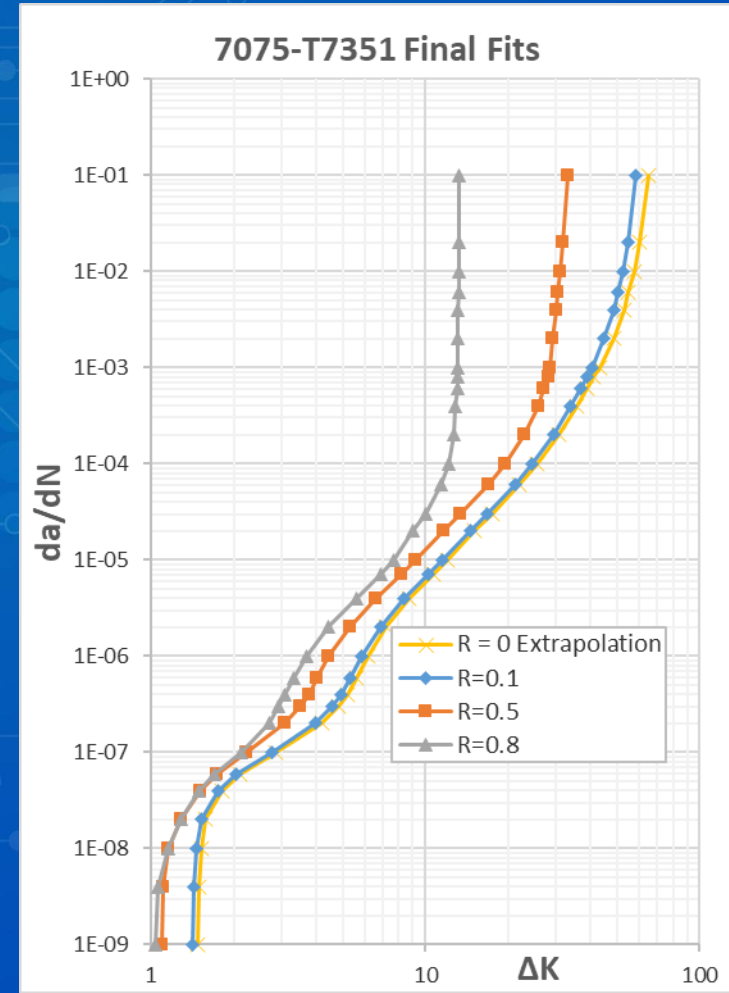
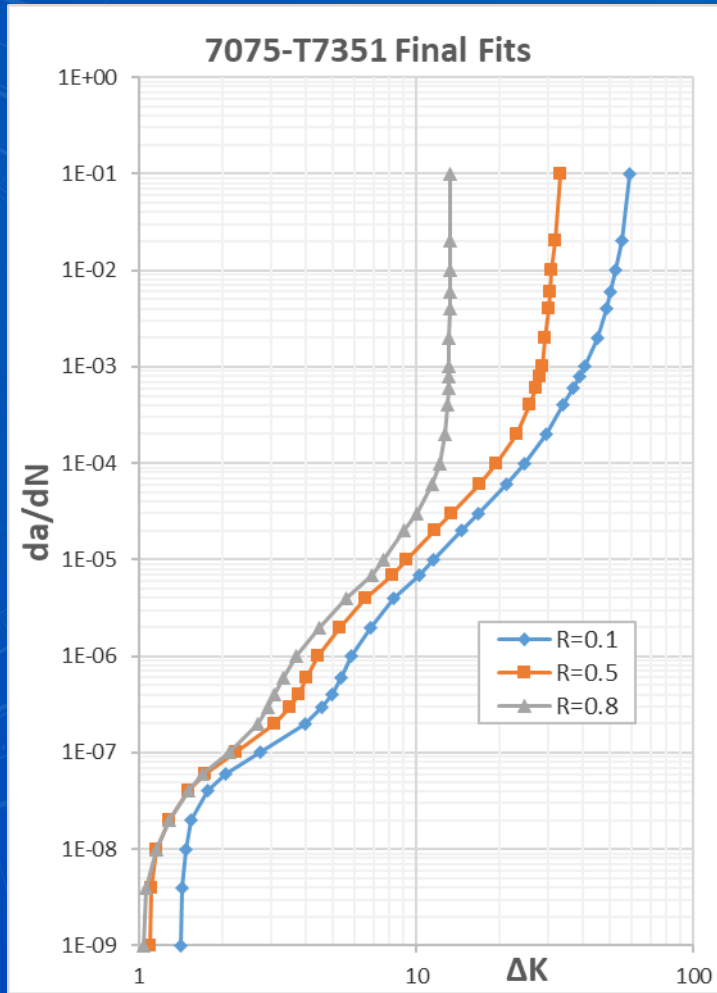
Smooth m-curve

# +R Final Fits and m-curves



# +R Final Fits and m-curves

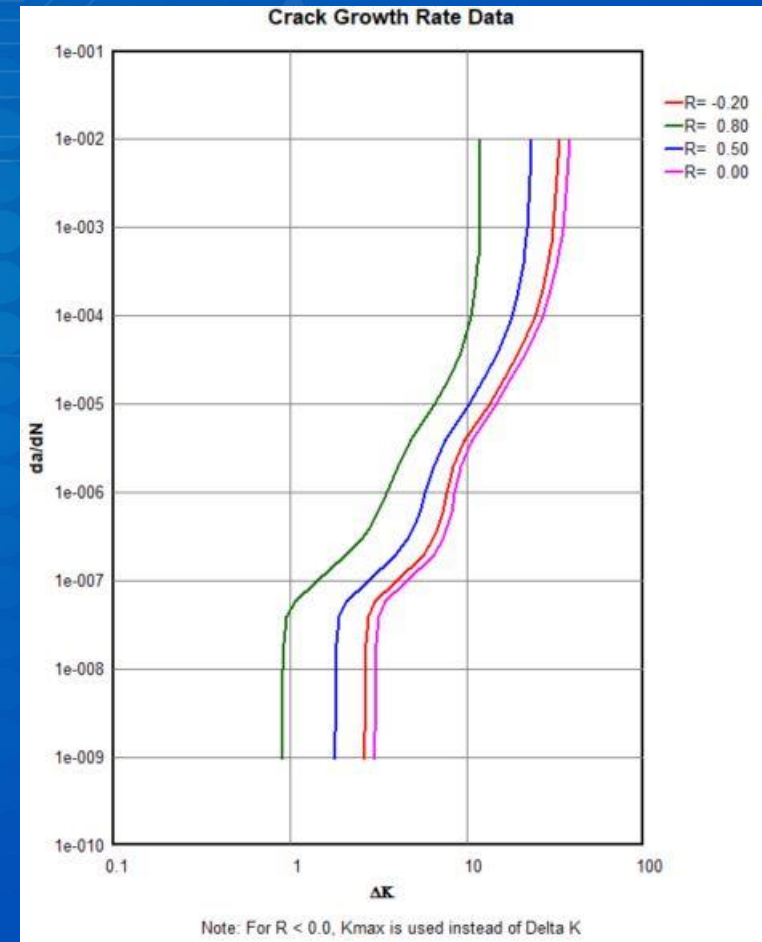
$$\Delta K(R = 0) = \Delta K(R = 0.1) \cdot (1 - R_{Shift})^{(m_{0.1} - 0.5 - 1)}$$





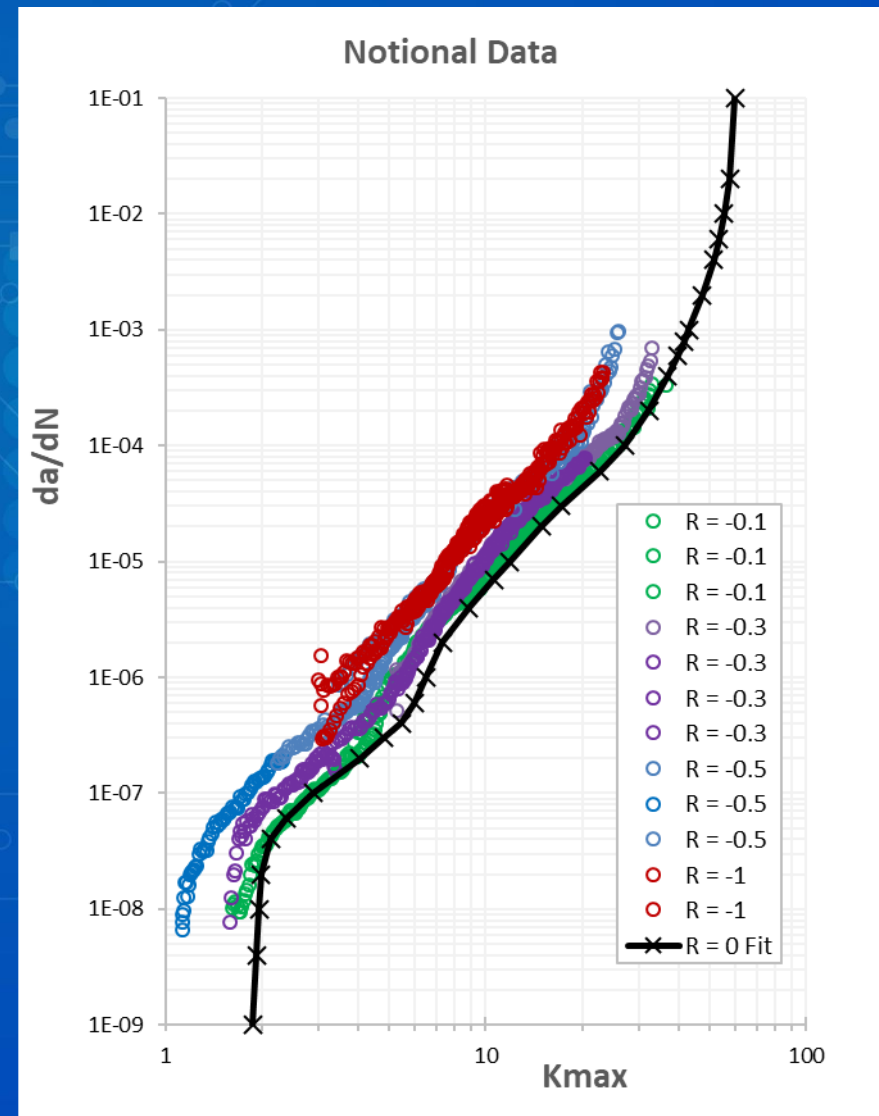
# What is $R_{I_0}$ ? – Visual Demonstration

- For negative stress ratios, fits are performed to the data when plotted against  $K_{max}$
- A leftward shift is observed for  $R < 0$ , when compared to  $R = 0$
- Shifting does not continue indefinitely, stops at  $R_{I_0}$
- Traditional wisdom is  $-0.5 < R_{I_0} < -0.2$
- All prior T-38 material curve fits used  $R_{I_0} = -0.3$

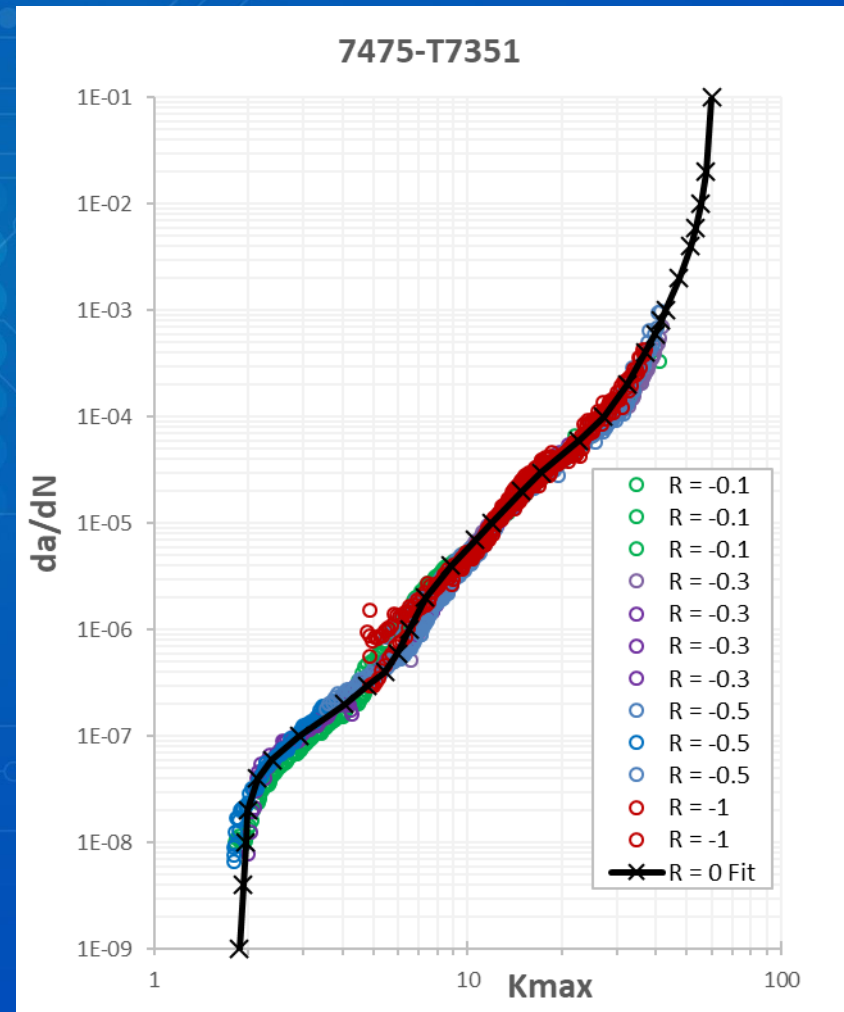
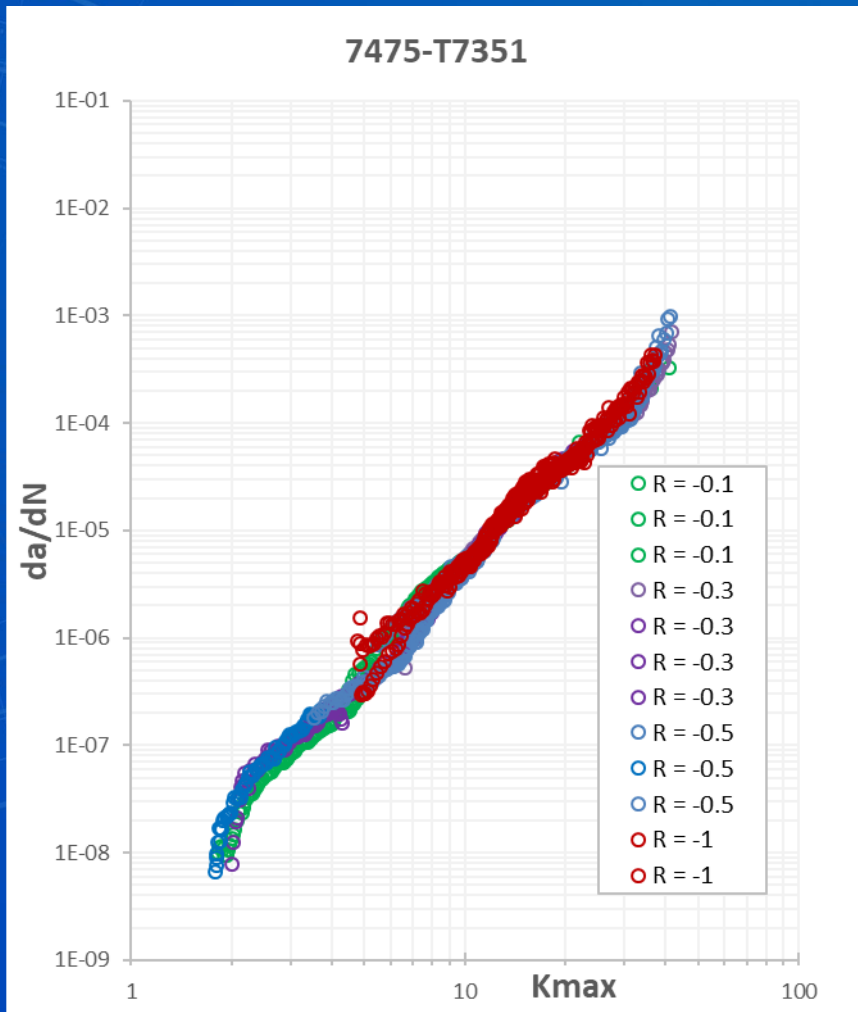


# Expected $R_{I_0}$ Behavior

- As  $R$  decreases, data shifts to left (plotted against  $K_{max}$ )
- As  $R \rightarrow R_{I_0}$ , shift in data slows
- At  $R < R_{I_0}$ , test data behaves the same as  $R = R_{I_0}$



# Example of -R Data (Real)





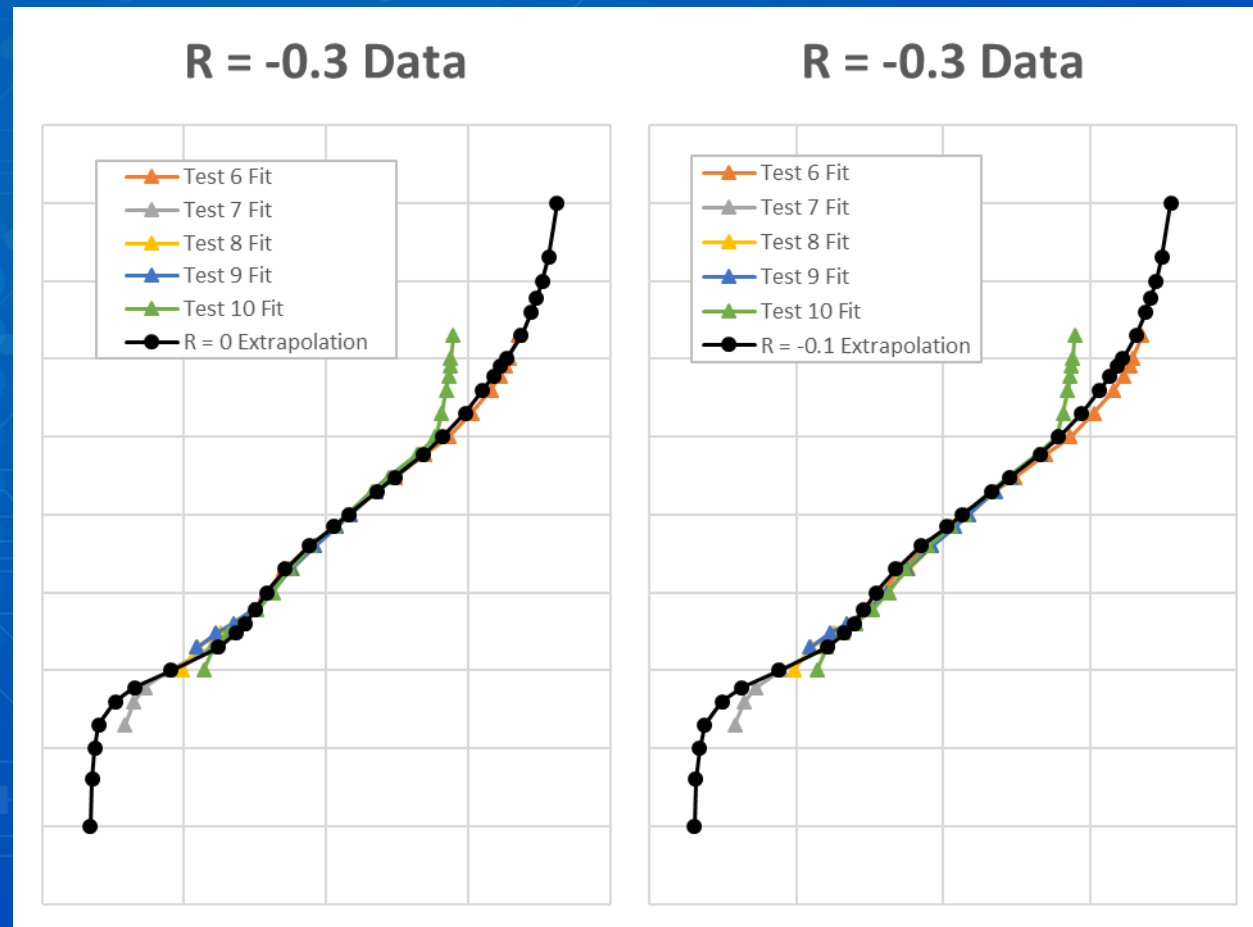
# Effect of $R_{I_0}$ on Predicted Life - Significant

- Sensitivity study on effects of  $R_{I_0}$
- $R_{I_0}$  can have a significant effect on the predicted life of a component
  - USAF: Lives drive inspection intervals – Very Important
- Wing A ( $R_{I_0} = 0$  vs.  $R_{I_0} = -0.1$ )
  - +9% Increase in Safety Limit
  - +9% Increase in Field Safety Limit
- Wing B ( $R_{I_0} = 0$  vs.  $R_{I_0} = -0.1$ )
  - +11.5% Increase in Safety Limit
  - +10.5% Increase in Field Safety Limit
- Results show that  $R_{I_0}$  is an important part of life predictions and highlight need for accurate  $R_{I_0}$  characterization.

# Quantitative Determination of $R_{I_0}$

$$K_{Shift} = \Delta K(R = 0) \cdot (1 - R_{Shift})^{(m-1)}$$

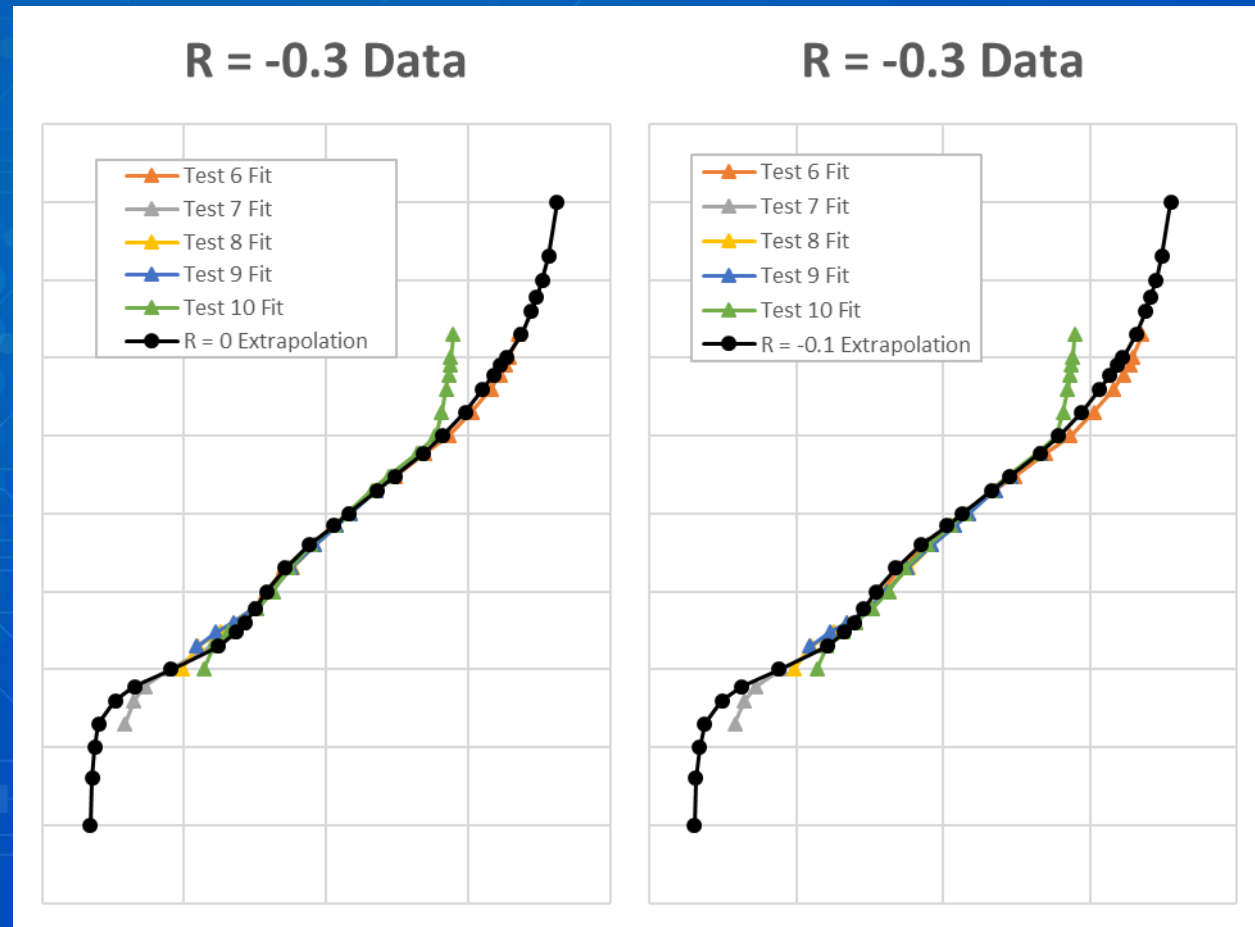
- $R_{I_0}$  calculated by extrapolating from +R fits
- $m$  determined from +R fits



Test Data smoothed for numerical handling

# Quantitative Determination of $R_{I_0}$

- Examine quality of extrapolations against a given stress ratio
- Define/determine “Best Extrapolation” – Extrapolation that minimizes error
- Plot Best Extrapolations ( $R_{I_0}$ ) vs Stress Ratio, look for behavior suggestive of  $R_{I_0}$
- At minimum, gives bounds on  $R_{I_0}$

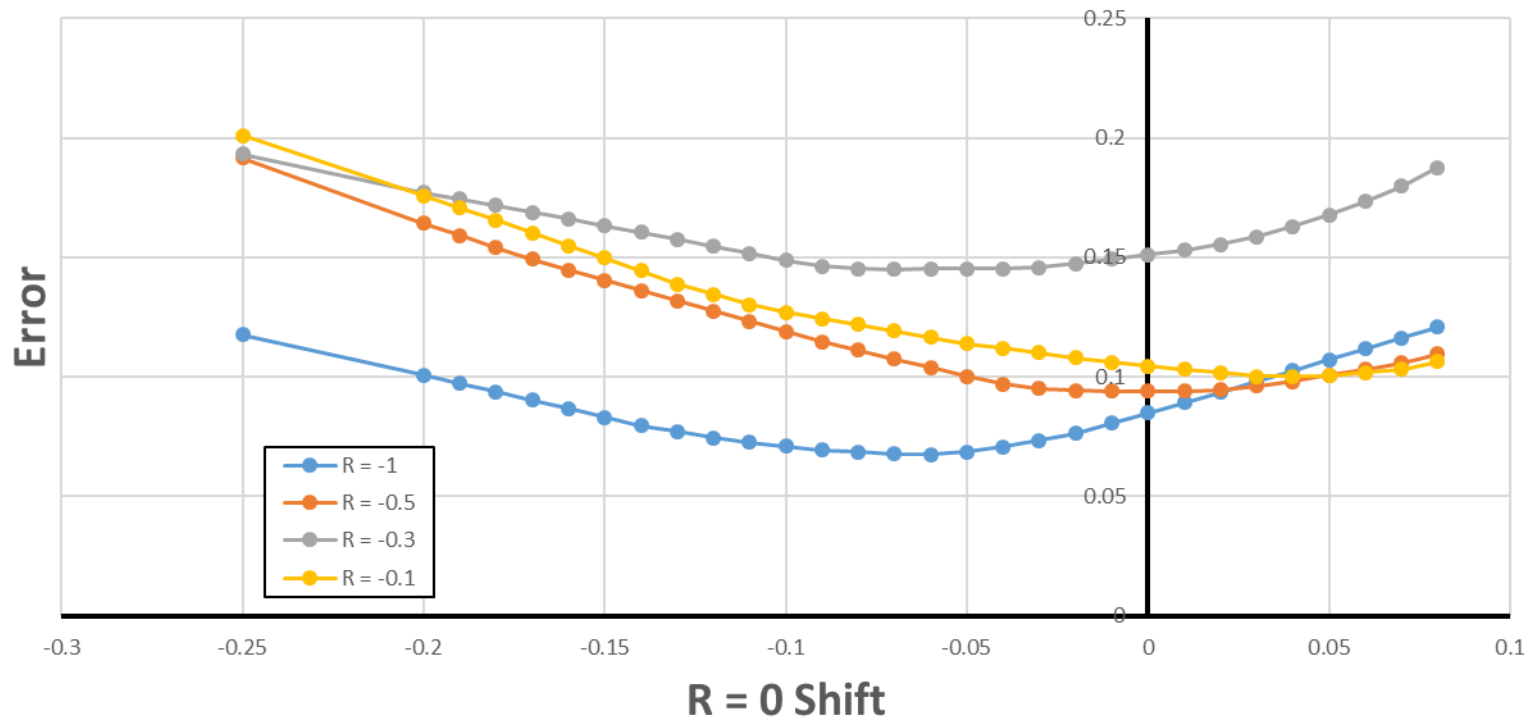


Test Data smoothed for numerical handling

# Results

7075-T735 I

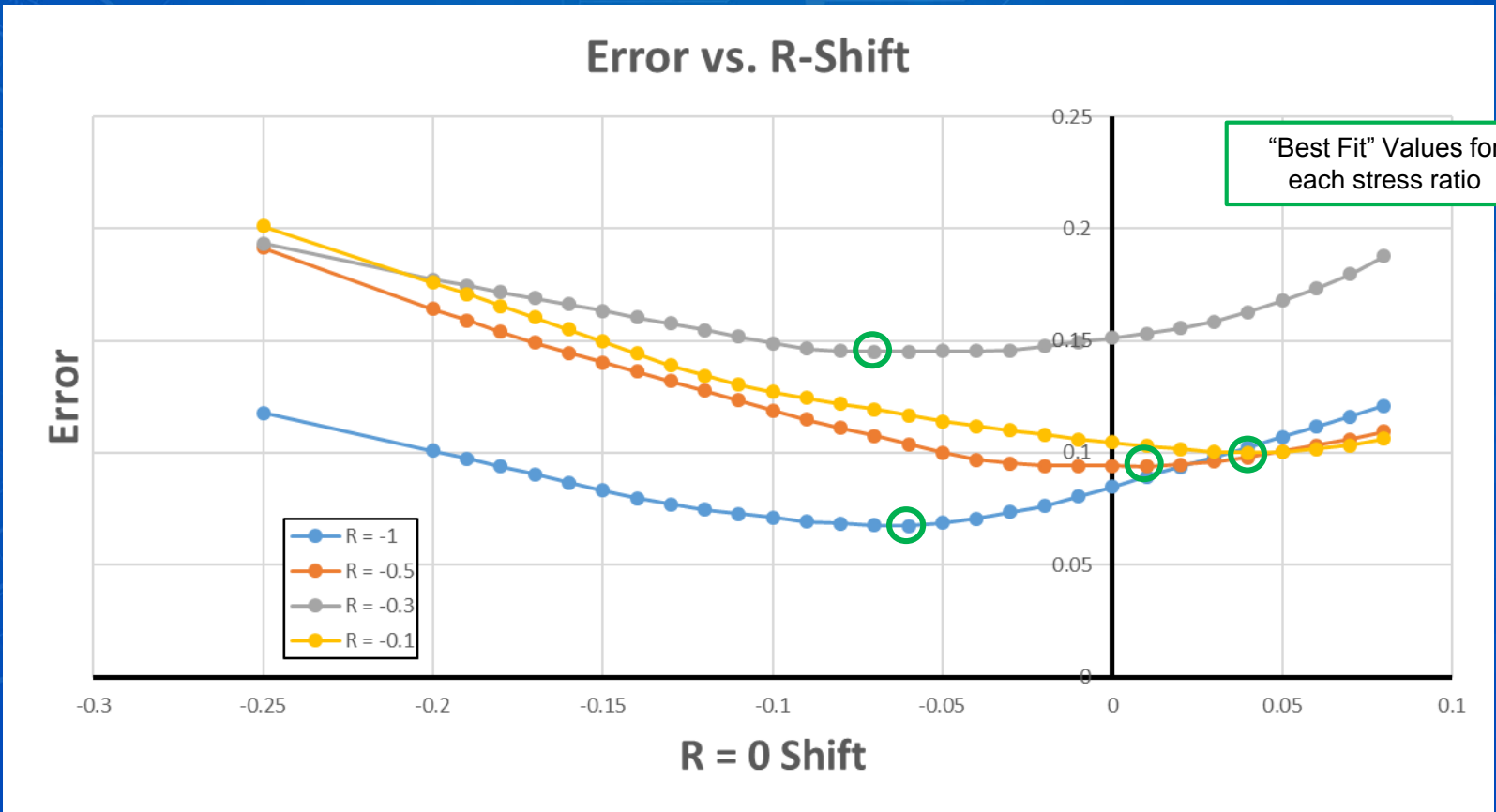
Error vs. R-Shift





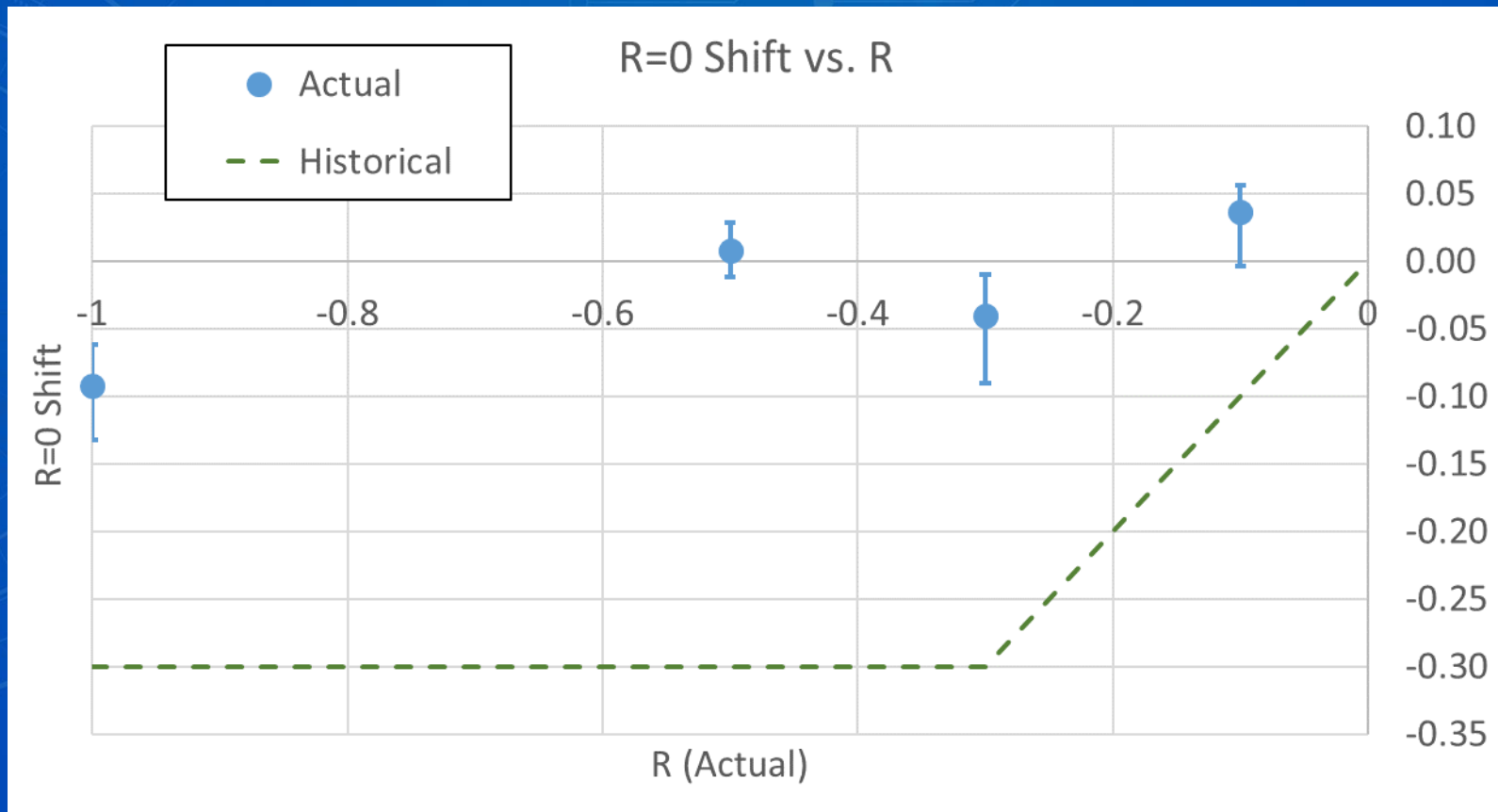
# Results

7075-T7351



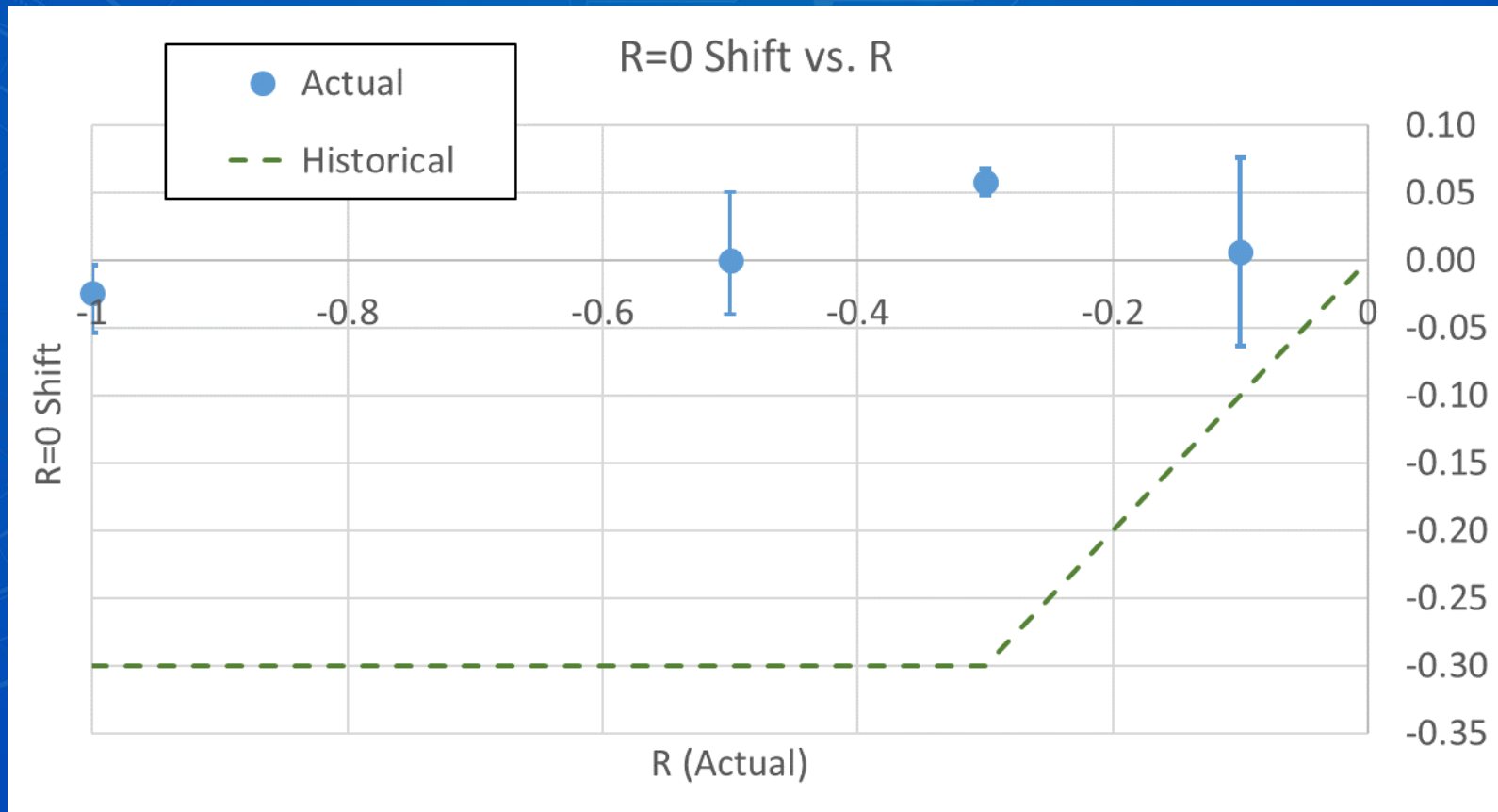
# Results

7075-T7351



# Results

## 7475-T735 I



# Results of Quantitative Determination

- Examined 5 different error metrics
- Results for  $R_{lo}$  – All Stress Ratios:
  - 7075-T735I:  $-0.13 < R_{lo} < 0.06$
  - 7475-T735I:  $-0.06 < R_{lo} < 0.08$
  - 7075-T735II:  $-0.03 < R_{lo} < 0.15$
  - 4130:  $0.19 < R_{lo} < 0.38$
- Used lowest calculated values from selected error metric or  $R_{lo} = 0$ , whichever is lower
- All results significantly higher than legacy values used in analysis

# Conclusions

- Fitting negative R data presents significant challenge
- Recommended  $R_{I_0}$  values based to T-38 tests are higher than historical values
- Continue efforts to fully characterize material behavior at negative stress ratios
  - Most frequently used data during a crack growth simulation when using Generalized Willenborg Retardation Models
- Attempt similar characterization on available data sets
- Examine the effect that higher growth rates, and less retardation has on crack growth model predictions