

2017 AFGROW Workshop



*Implementation of Bi-Variant
Polynomial Equations to
Include the Effect of a Fatigue
Crack on the Residual Stress
and Life Prediction at Cx Holes*



Presentation By:

Scott Carlson.

Co-author – Marcus Stanfield

Senior Research Engineer

Southwest Research Institute (SwRI)

A-10 & T-38 ASIP Analysis Group

Hill, AFB, Utah

Scott.Carlson@SwRI.org

2016 AFGROW Workshop

Application of Uncertainty Quantification for Residual Stress Measurement at a Cold Expanded Hole



Presentation By:

Scott Carlson

Marcus Stanfield (co-author)

Southwest Research Institute (SwRI)

A-10 & T-38 Aircraft Structural Integrity Program (ASIP) Analysis

Group

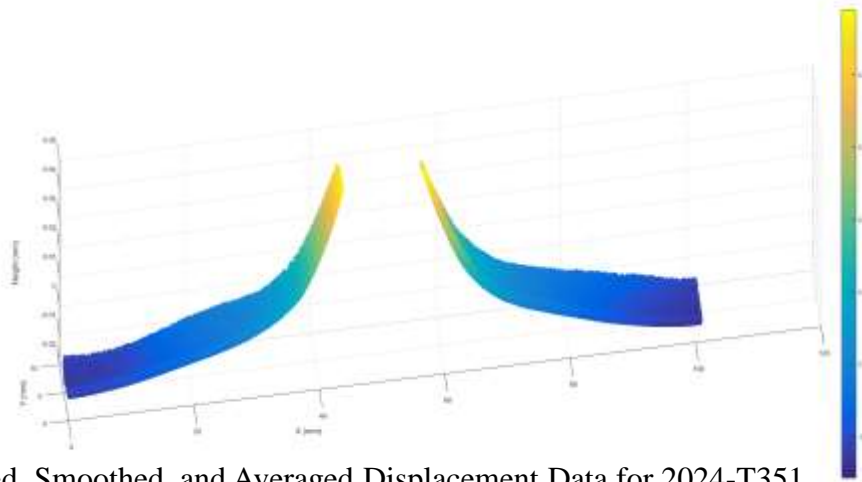
Hill AFB, UT

Email: Scott.Carlson@SwRI.org

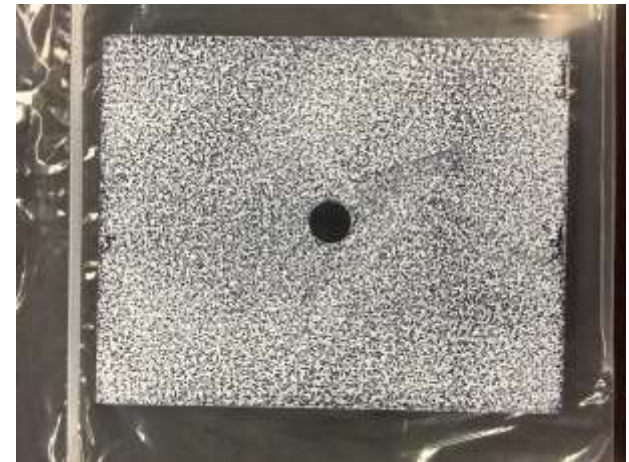
Marcus.Stanfield@SwRI.org

Questions Unanswered

- Large Displacements Along Entrance and Exit Surfaces
 - Potentially due to plane stress/plane strain effect from cutting



Aligned, Smoothed, and Averaged Displacement Data for 2024-T351, CxA2-1

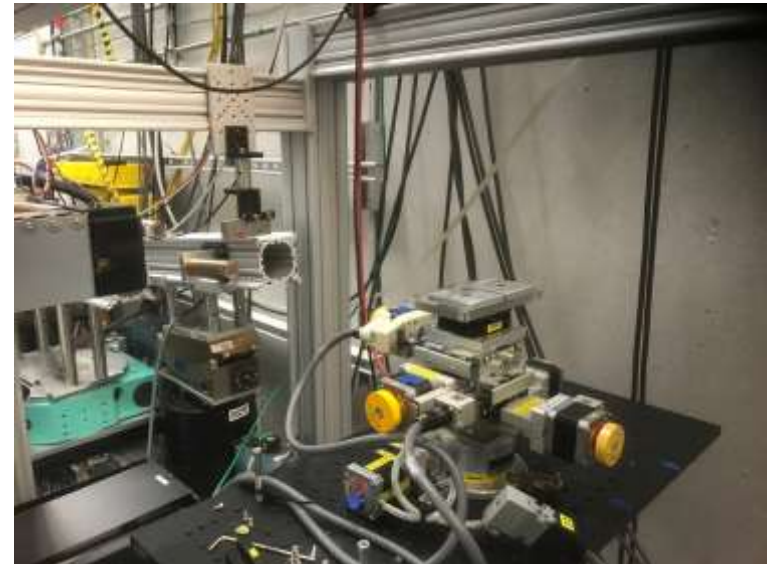
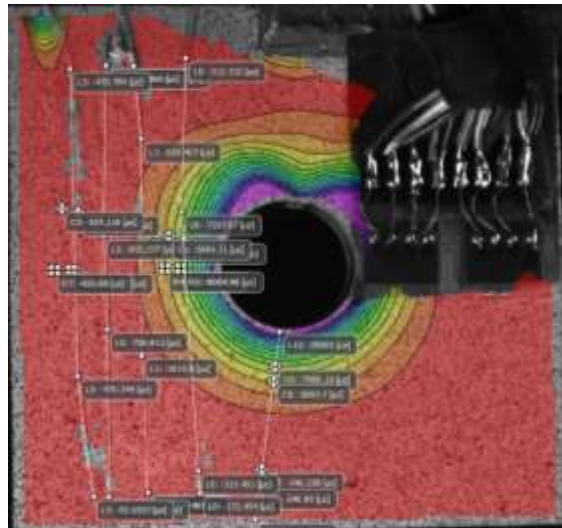
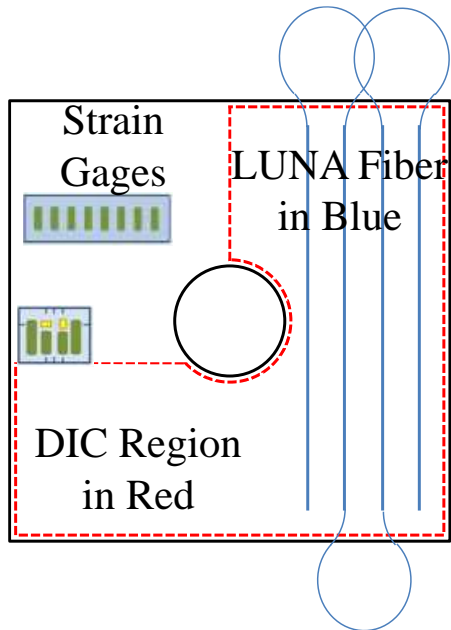


- Potential use of DIC to “Correct” for Surfaces
 - Causes higher compressive residual stresses than expected



Surface & Thru-Thickness

- Performed Surface Displacement Measurements
 - DIC, LUNA (fiber optics), and Strain Gages
- Performed Thru Thickness Displacement Measurements
 - High Energy X-ray Diffraction (Argonne) – DONE
 - X-ray Diffraction (NRC – Canada) - Currently
 - Neutron Diffraction (IMAT – UK)
 - Contour Method (Hill Engineering, LLC.)



Inter-Laboratory Cx Work

- Working to Have Multiple Labs Perform Residual Stress Measurement of Cx Condition
 - Does data processing methods make significant impact?
 - Does cutting methods cause significant impact on stress results?
- Working with 5 Labs for Inter-Laboratory Data Reduction of 4-Pt. Bend Condition^{7,8}
 - Coupons tested at SwRI, cut at Hill Eng. LLC.
 - Data sent to individuals at Hill Eng. LLC., Los Alamos Labs, StressMap (UK), Hill AFB, Hydro-Quebec Research Institute
 - Is not trying to capture cutting and displacement measurement errors
- Need to Provide Users with Understanding of Uncertainty if Contract goes to “*Lowest Cost, Technically Acceptable*”
- Potential to have Inter-Laboratory Total Uncertainty “Too High” – Would Limit Usefulness of Method

Inter-Laboratory Cx Work

- Provided FEA Simulation of 4-pt Bend and have Results
 - Post processing and comparing
- Currently in Prep for Two 4-pt Bend Tests



Future Work

- Quantification of Total Uncertainty is Essential for Future Work
 - Enables confidence in isolating out effect being investigated
- Effect of a Fatigue Crack on the Residual Stress Field
- Effect of Peak Compression Cycles on Residual Stress Field
- Effect of Steel Pin Installation During Cyclical Loading
- Effect of Bearing & Bypass Loading
- Application of DIC for Measurement of Strain/Stress During Cx-Through-Testing-Crack Propagation Process
 - Look to correlate to Contour Method data
 - Potential for surface correction to improve Contour Method data
- Integrate all Aspects into Fatigue Life Prediction at Critical Airframe Locations Across Fleet - USAF-wide

Acknowledgements

- Dr. Mark Thomsen – A-10 ASIP Manager
- Lucky Smith – SwRI Program Manager
- Joshua Hodges – Hill Engineering, LLC.
- Dr. Tom Mills - AP/ES Inc.

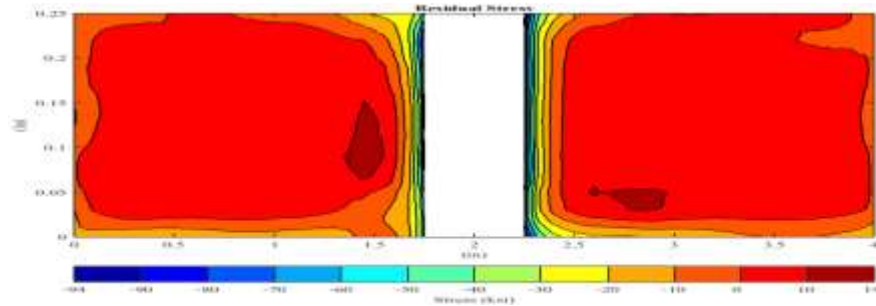


Agenda

- Perspective and Overview of Contour Method
- *Influence of Fatigue Crack on Residual Stress Field*
 - *Hypothesis and experiment set-up*
- Fatigue Crack Coupon Development
- Residual Stress Calculations for Cx Holes with Cracks
 - 2024-T351 & 7075-T651 “Low” Applied Cx
- *Integration of Effected Residual Stress State into Fatigue Crack Growth Analysis*
 - Residual stress function’s effect on life predictions
 - Outputs to help make educated decisions for the future
- Conclusions and Recommendations

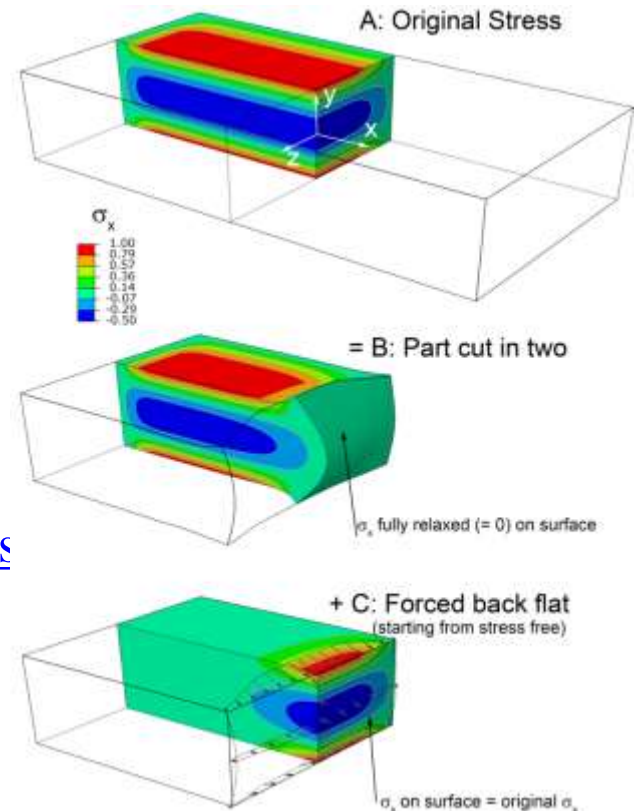
HOLSIP Perspective

- Deep Residual Stresses/Self Stresses are a Physics-based Process
 - Plastic deformation
 - Local yielding
- Define/Quantify Parameters of Influence
 - Percent expansion
 - Local stress state
 - Applied loading (tension or compression dominated?)
- Understand and Statistically Quantify Bounds of Application
 - More accurate modeling of condition
 - Ability to more accurately assess risks and benefits



Contour Method

- Developed by Prime, M, Hill, M at Los Alamos Labs
- First Published in 2001¹
- Based upon the Bueckner's Superposition Principle of Stresses²
- Composed of 4 Major Steps
 - Cut using wire EDM
 - Measure using CMM or laser profilometer
 - Perform alignment, averaging, and “fitting” or “smoothing” – [Johnson, G. Dis](#)
 - Apply final fit surface as boundary constraints to FEA
 - Solve for stresses within body



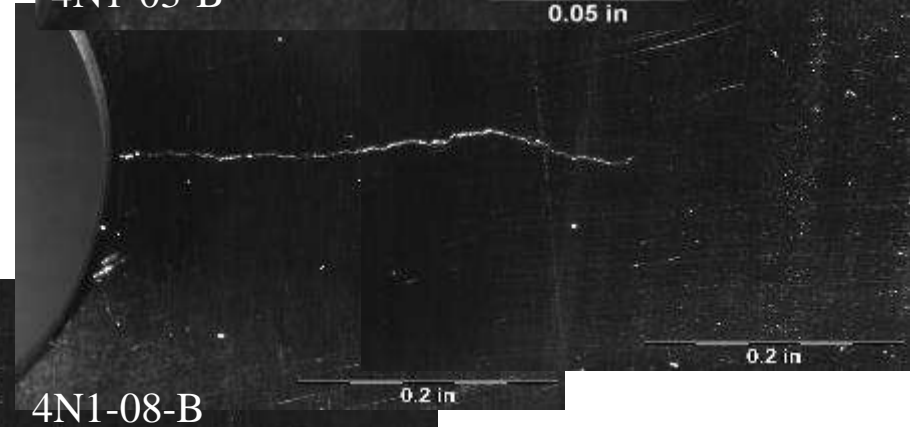
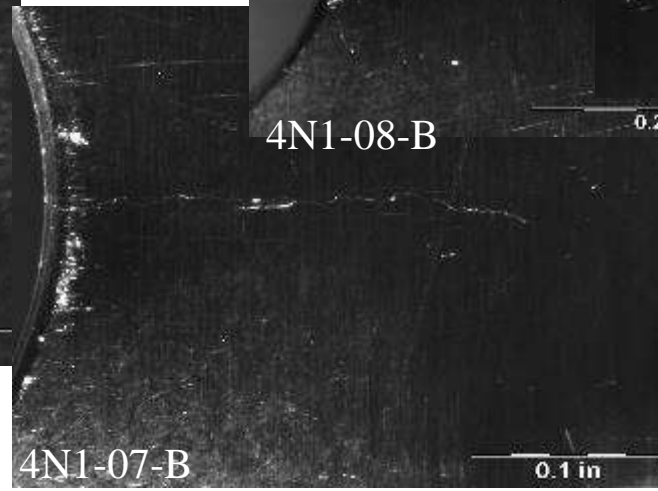
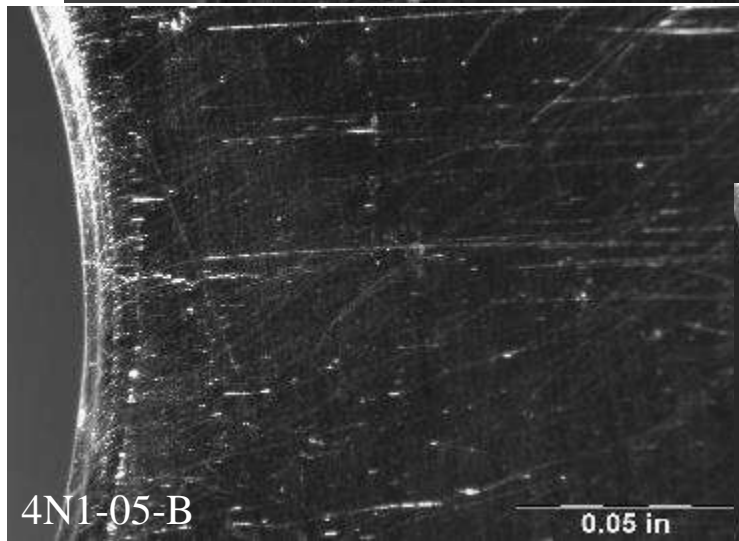
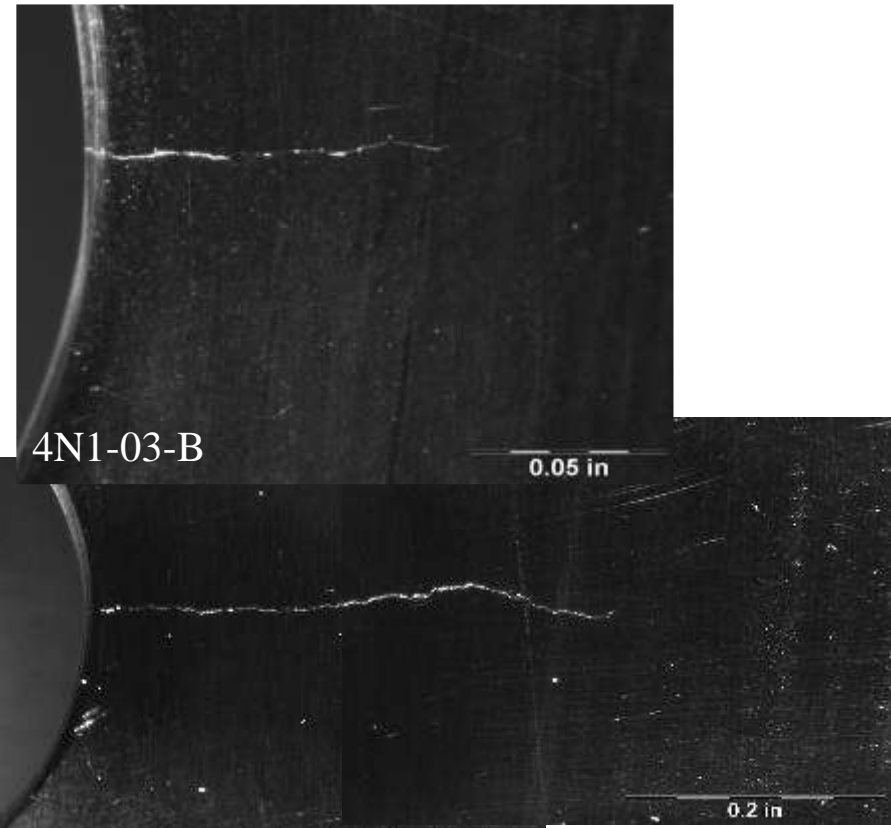
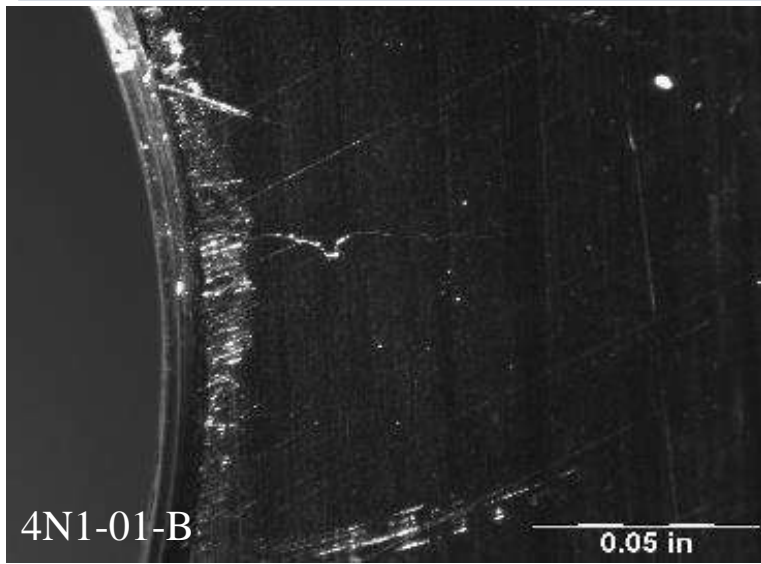
Influence of a Fatigue Crack

- Hypothesis:
 - *“The presence of a fatigue crack changes the residual stress field induced by the Cold Expansion (Cx) process within aerospace-grade aluminum alloys, namely 2024-T351 and 7075-T651”*
- Procedure for Testing Hypothesis
 - Develop baseline Cx coupons, no fatigue crack coupons
 - Develop fatigue cracks via constant amplitude loading in identical Cx coupons
 - Range of crack sizes, stress = 25ksi or 26.5ksi, R = 0.1
 - Focus on “Low” applied expansion level for all Cx holes

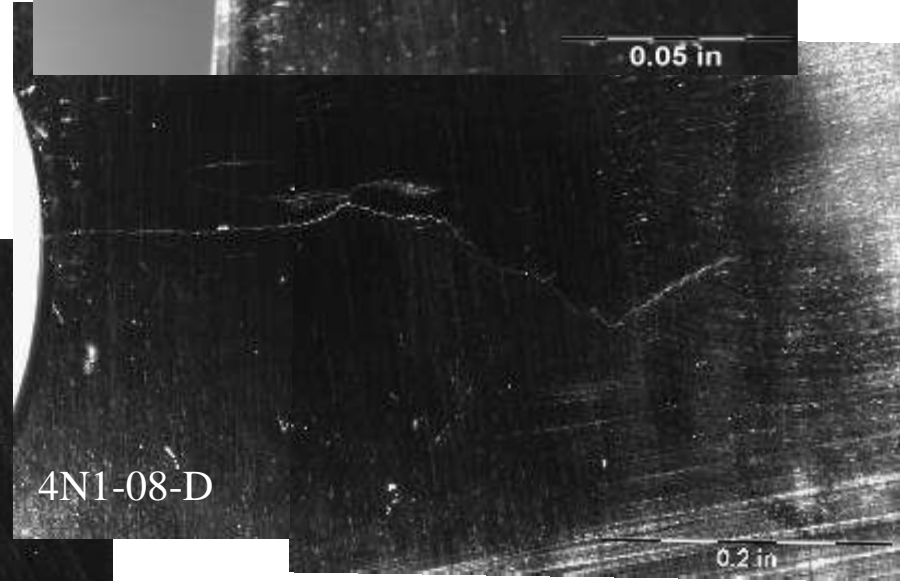
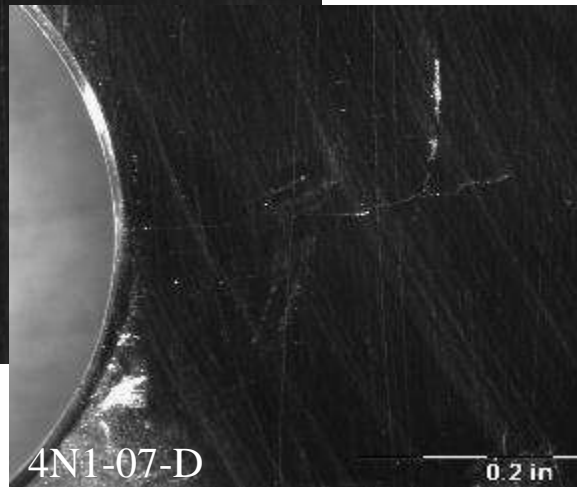
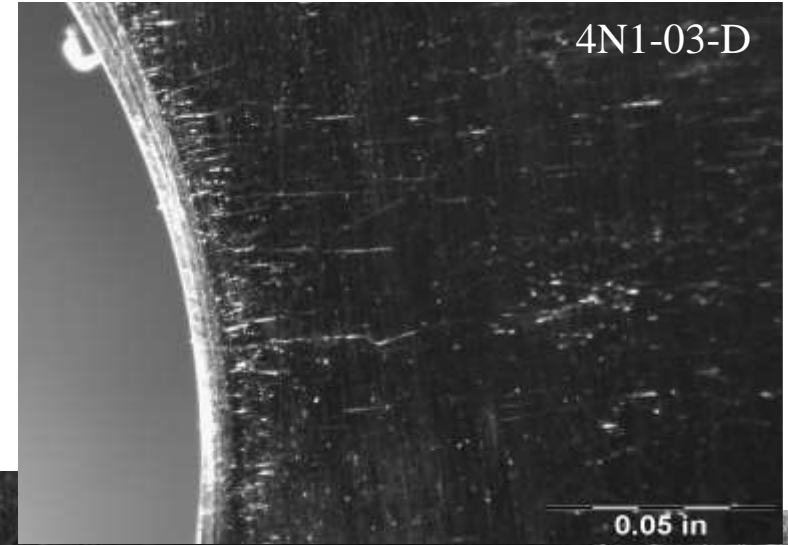
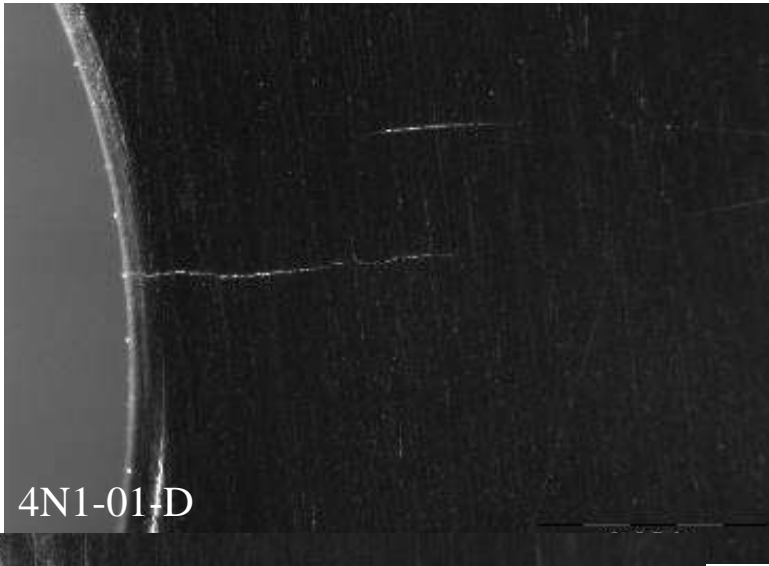
2024-T351 Coupons							
Specimen ID	Mandrel Entrance Face Crack (inch)	Gauge Width (inch)	Gauge Thickness (inch)	Initial Ream Diameter (CMM) (inch)	% CX	Final Ream Diameter (inch)	RS Specimen Length (inch)
4N1-01-B	0.0797	4.0000	0.2545	0.4771	3.23%	0.4990	5.0030
4N1-02-B	0.0798	4.0030	0.2550	0.4768	3.29%	0.4997	5.0035
4N1-03-B	0.0974	4.0025	0.2548	0.4772	3.21%	0.4997	5.0028
4N1-04-B	0.0962	4.0022	0.2555	0.4771	3.23%	0.4990	5.0022
4N1-05-B	0.1259	4.0027	0.2557	0.4771	3.23%	0.4980	5.0023
4N1-06-B	0.1214	4.0023	0.2555	0.4770	3.25%	0.4990	5.0025
4N1-07-B	0.2515	4.0020	0.2555	0.4770	3.25%	0.4995	5.0030
4N1-08-B	0.4974	4.0013	0.2550	0.4770	3.25%	0.4995	5.0030
AVERAGE		4.0020	0.2552	0.4770	3.24%	0.4992	5.0028
STDEV		0.0009	0.0004	0.0001	0.03%	0.0006	0.0004

7075-T651							
Specimen ID	Mandrel Entrance Face Crack (in)	Gauge Width (inch)	Gauge Thickness (inch)	Initial Ream Diameter (CMM) (inch)	% CX	Final Ream Diameter (inch)	RS Specimen Length (inch)
4N1-01-D	0.0793	4.0028	0.2495	0.4766	3.34%	0.4988	5.0023
4N1-02-D	0.0807	4.0023	0.2510	0.4768	3.29%	0.4990	5.0022
4N1-03-D	0.0972	4.0017	0.2508	0.4769	3.27%	0.4993	5.0020
4N1-04-D	0.1015	4.0015	0.2500	0.4770	3.25%	0.4985	5.0025
4N1-05-D	0.1253	4.0020	0.2505	0.4769	3.27%	0.4992	5.0033
4N1-06-D	0.1235	4.0027	0.2507	0.4770	3.25%	0.4980	5.0020
4N1-07-D	0.2505	4.0020	0.2505	0.4767	3.31%	0.4983	5.0023
4N1-08-D	0.5017	4.0022	0.2512	0.4769	3.27%	0.4992	5.0030
AVERAGE		4.0021	0.2505	0.4769	3.28%	0.4988	5.0025
STDEV		0.0005	0.0005	0.0001	0.03%	0.0005	0.0005

Fatigue Cracks in 2024-T351

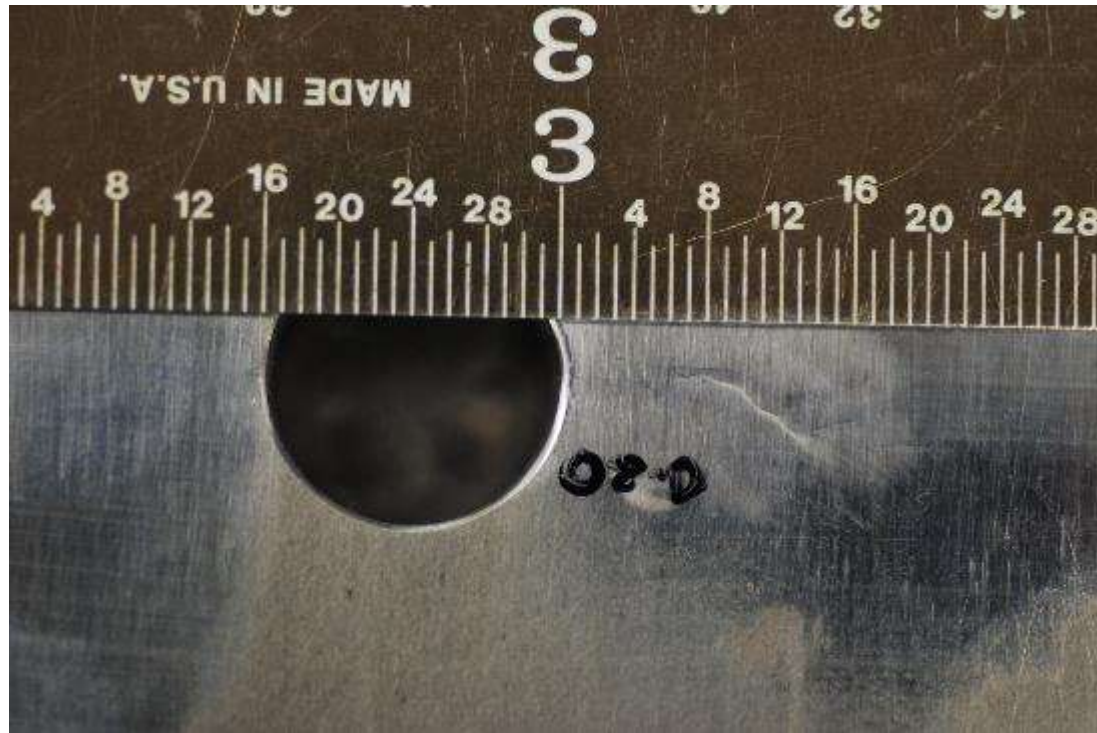


Fatigue Cracks in 7075-T651



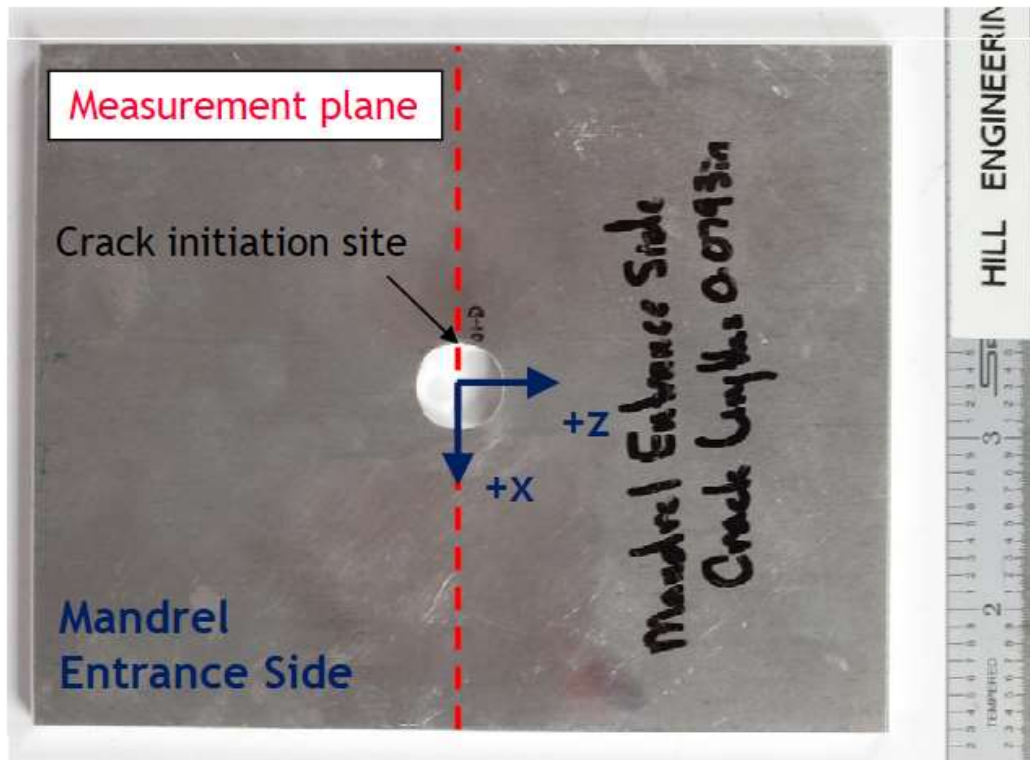
Displacement Measurements

- Macro Images of Coupons



Displacement Measurements

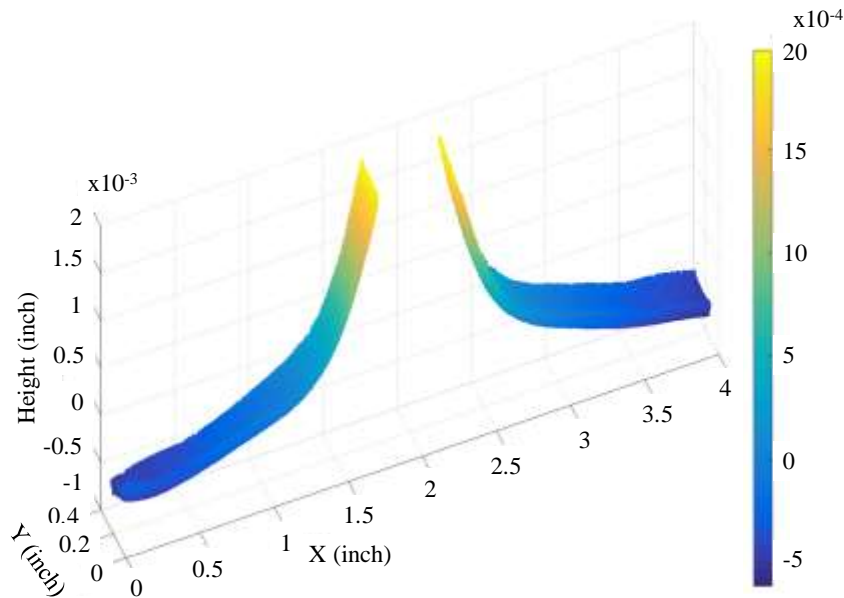
- Contour Measurements at Crack Plane
 - Cutting of coupon initiated at fatigue cracked side
 - Cut plane was as close to plane of fatigue crack
 - For larger cracks approx. 0.25-0.50inch cracks were off plane



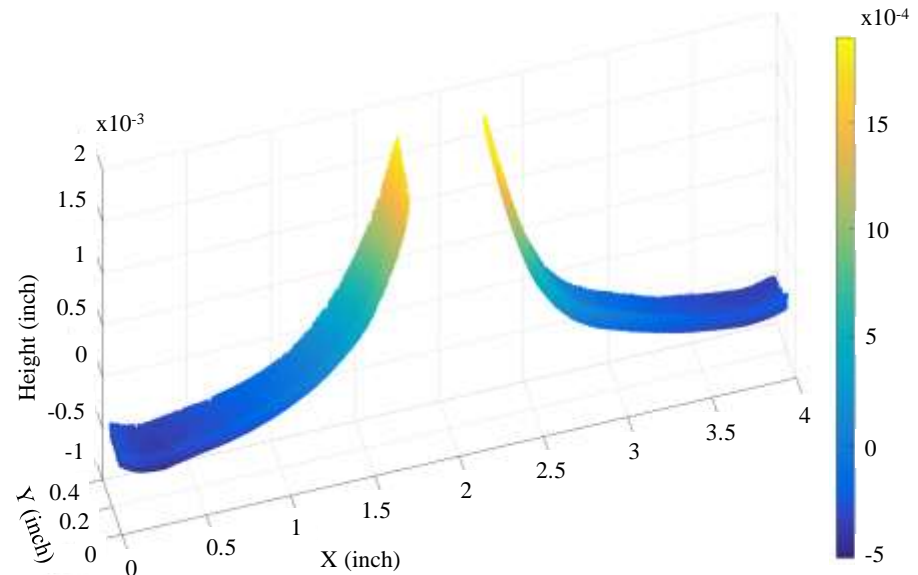
+y is into page
as shown here

Displacement Measurements

- All Displacements Provided by Hill Engineering LLC.
- Completed Data Reduction of Cracked Coupons
 - Followed same data reduction process for cracked coupons as with baseline coupons
 - Assumption: Lot-to-lot variability is negligible in these experiments



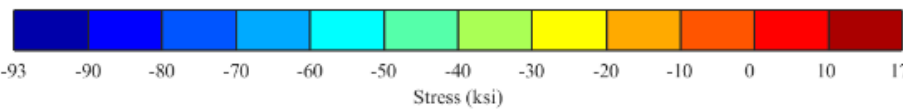
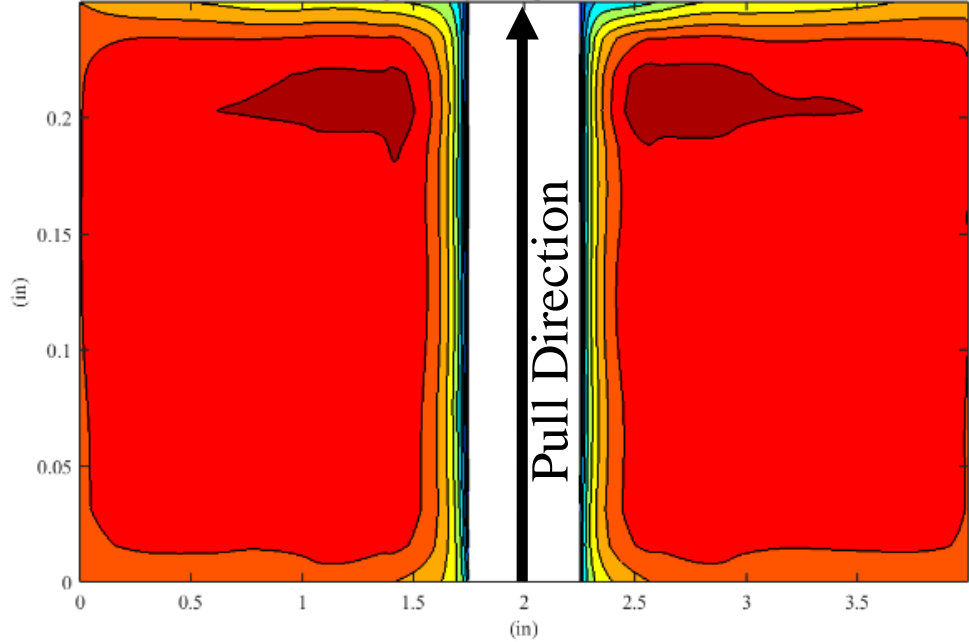
Cx-2024-T351 – Crack Size = 0.08inch



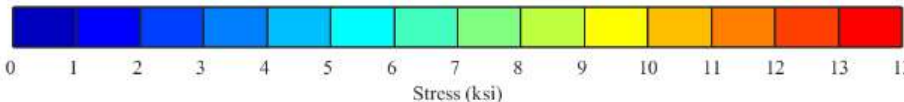
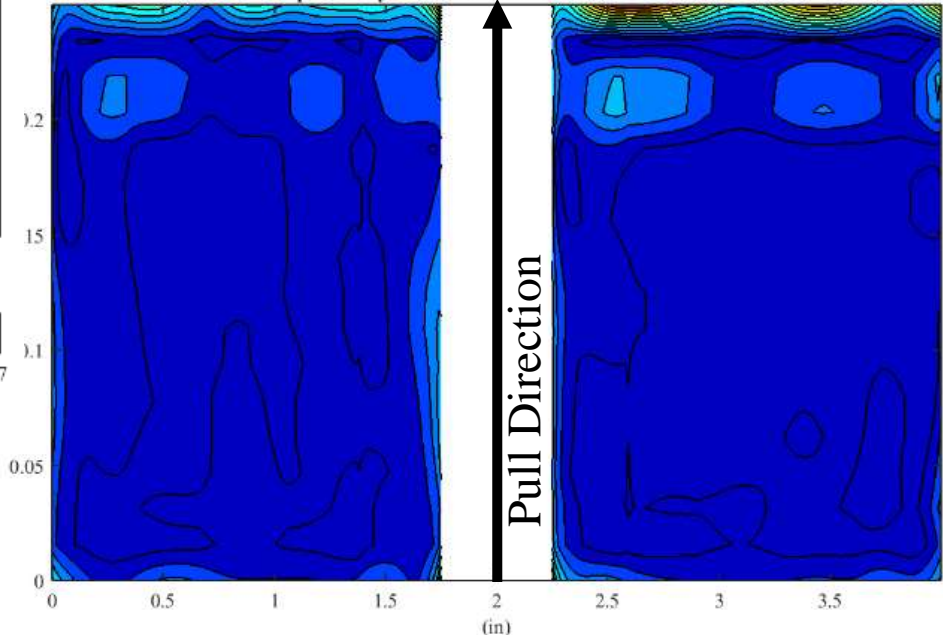
Cx-2024-T351 – Crack Size = 0.4974inch

Average Baseline 2024-T351

Repeatability Average Residual Stress

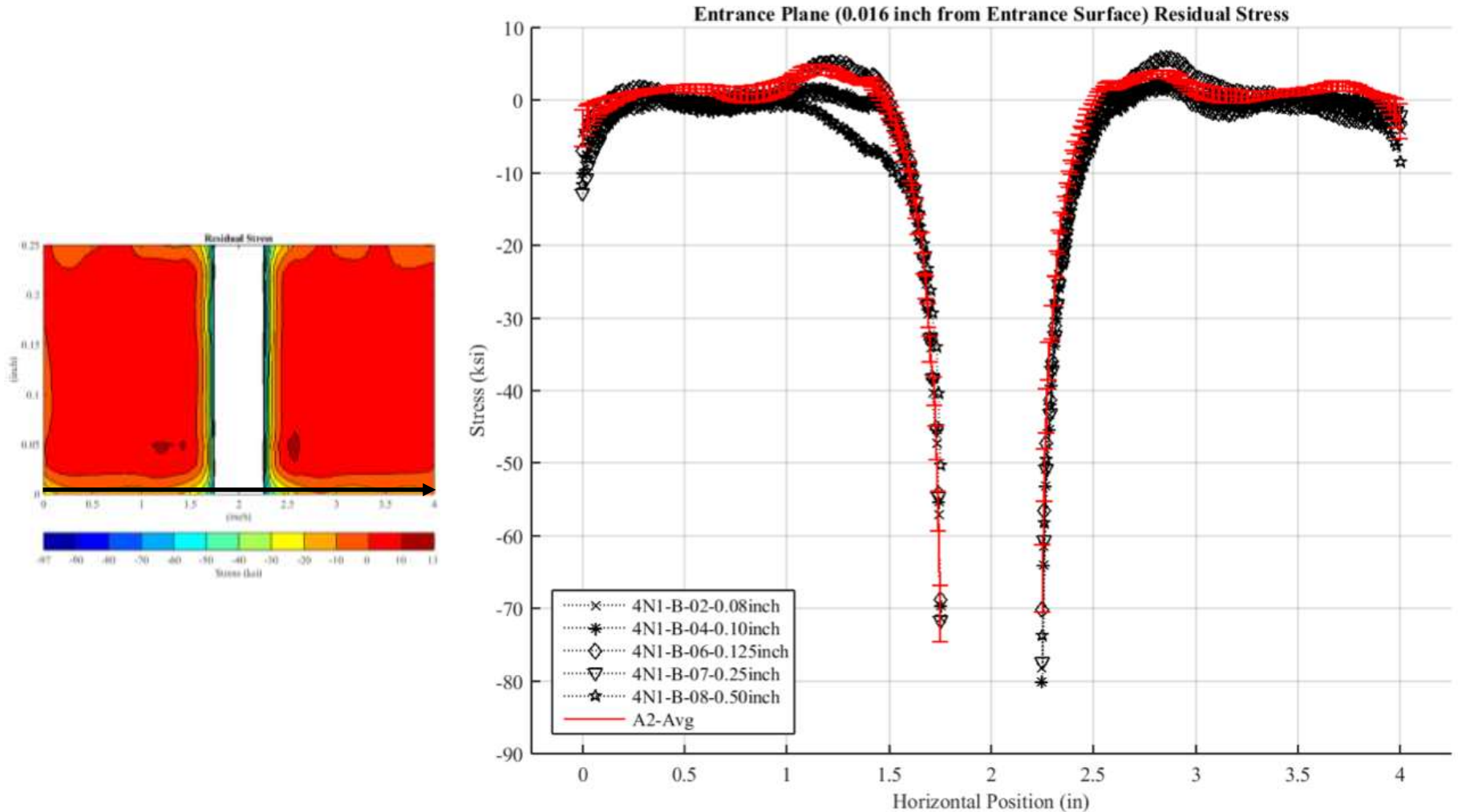


Repeatability Standard Deviation of Residual Stress



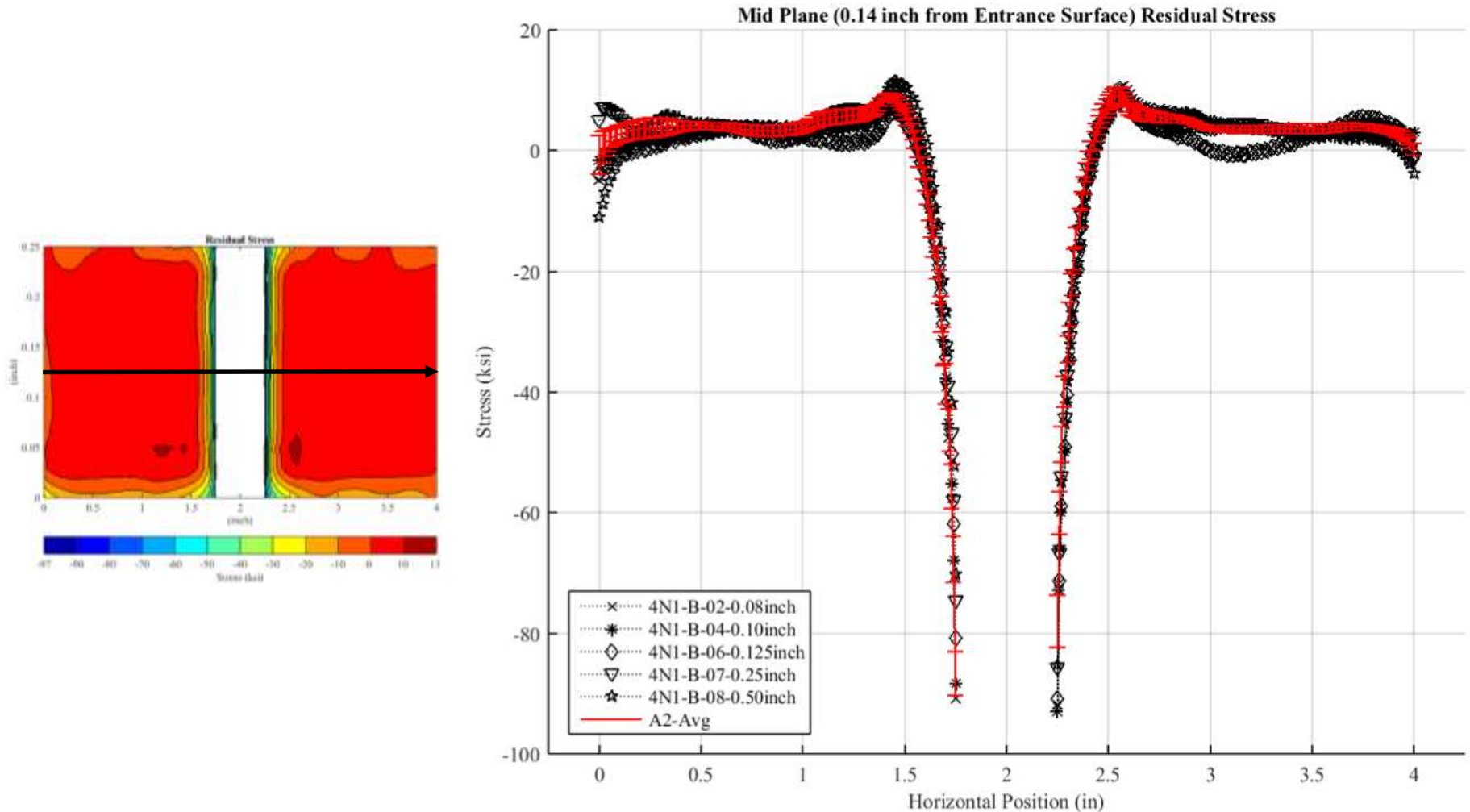
Residual Stresses in 2024-T351

- Line Plots of Stress Radially from Hole



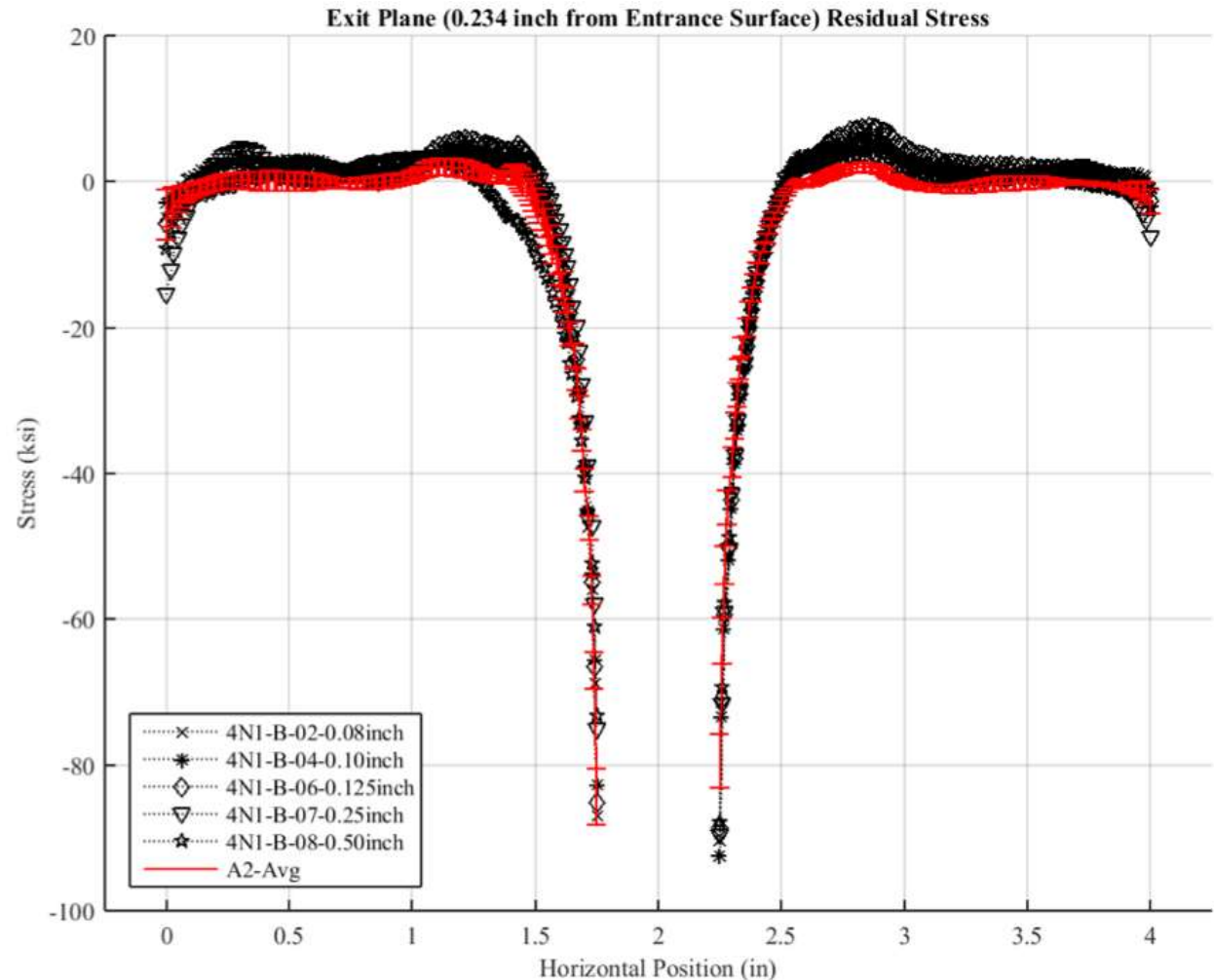
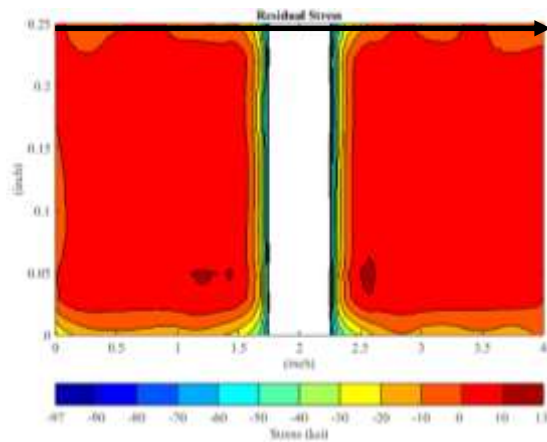
Residual Stresses in 2024-T351

- Line Plots of Stress Radially from Hole



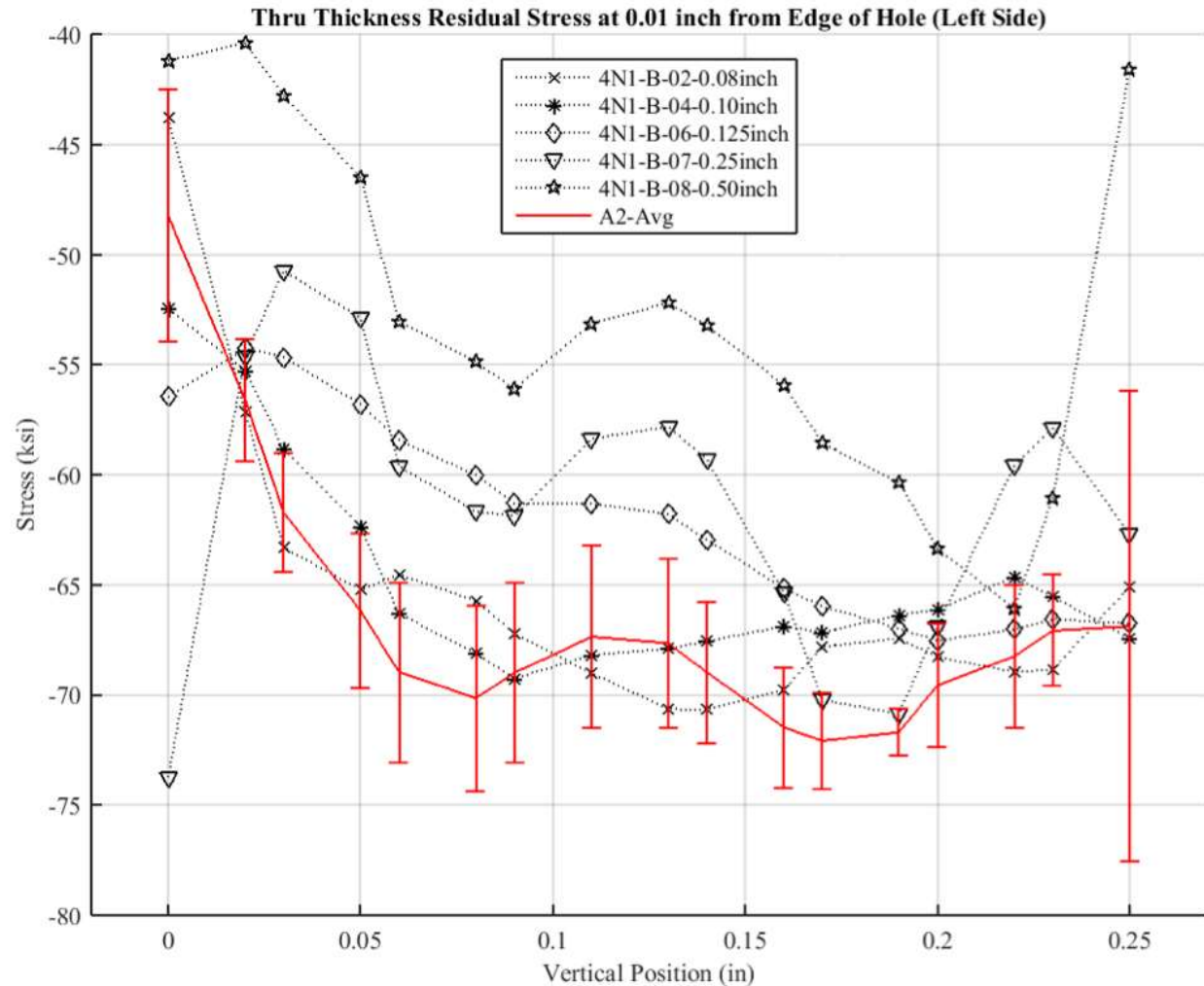
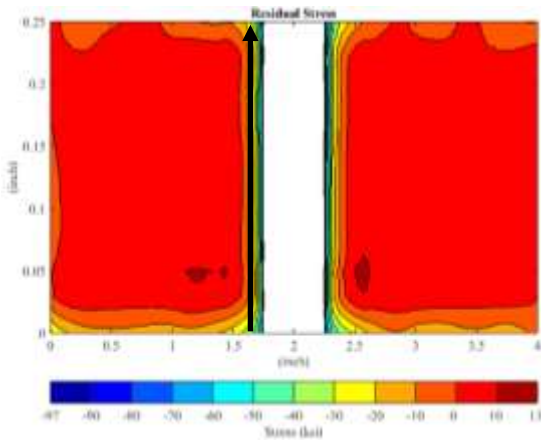
Residual Stresses in 2024-T351

- Line Plots of Stress Radially from Hole



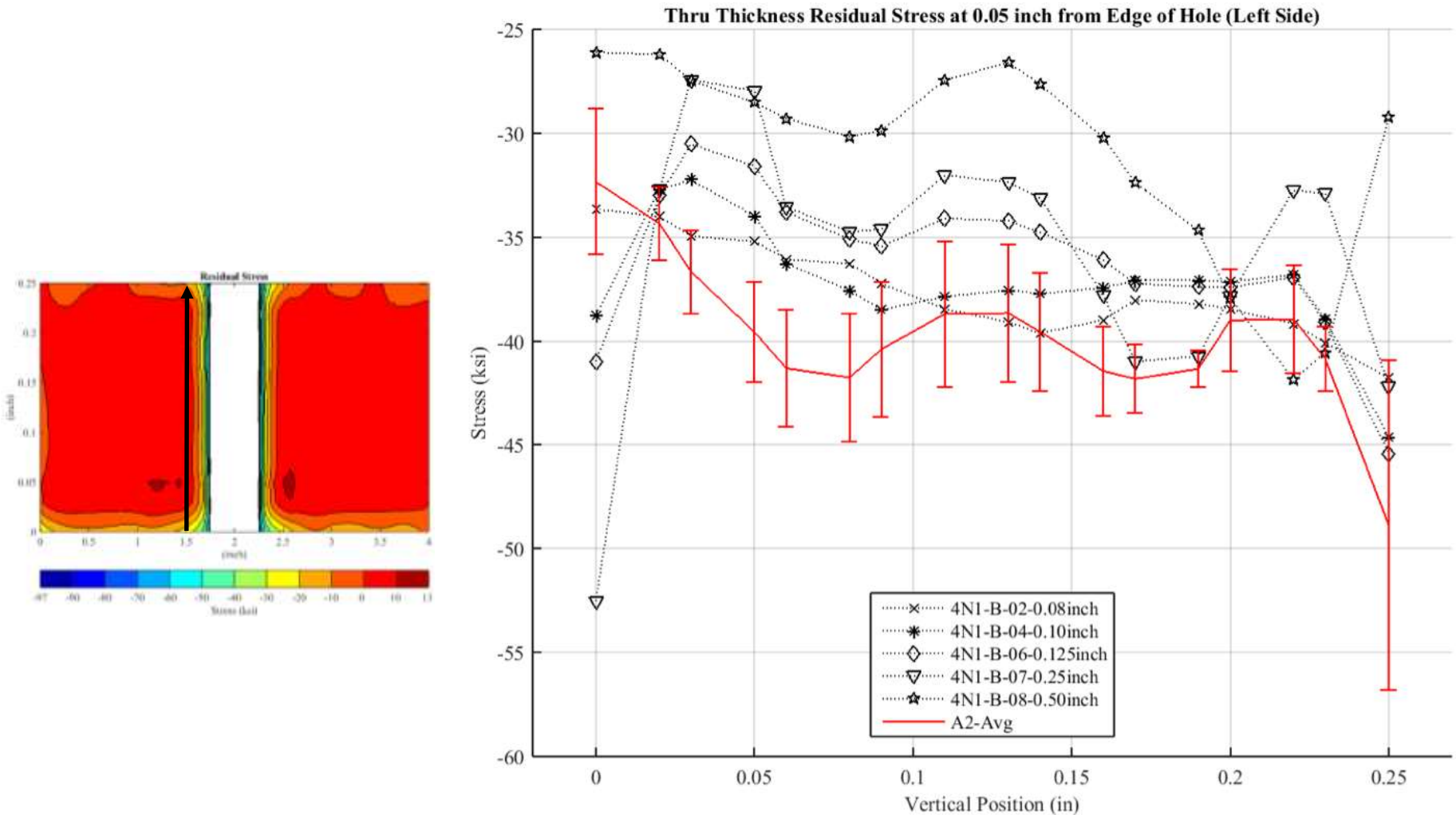
Residual Stresses in 2024-T351

- Line Plots of Stress Through Thickness Near Hole



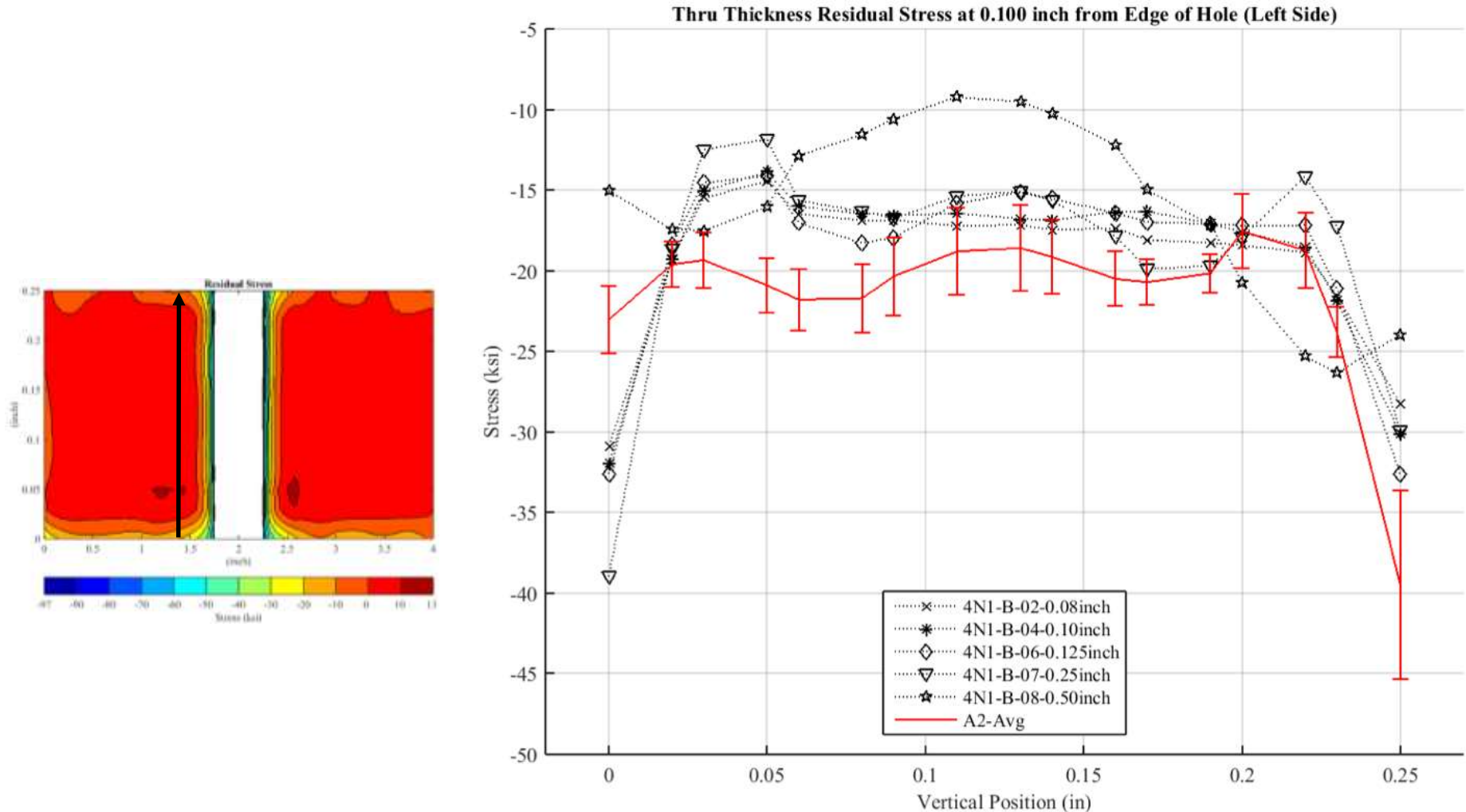
Residual Stresses in 2024-T351

- Line Plots of Stress Through Thickness Near Hole

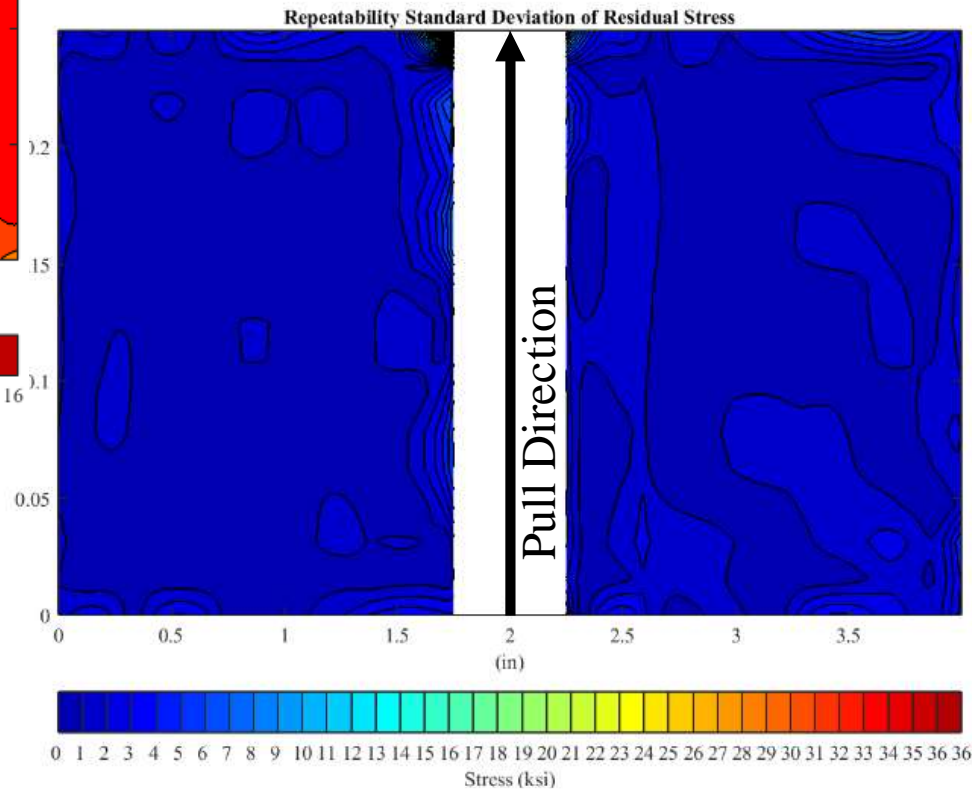
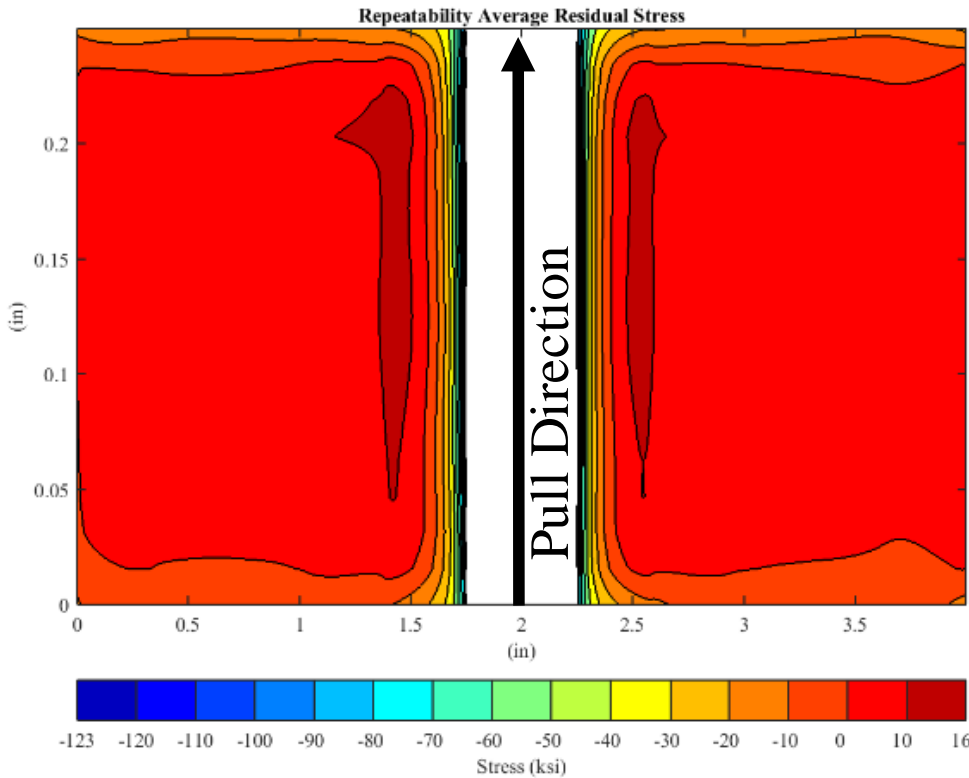


Residual Stresses in 2024-T351

- Line Plots of Stress Through Thickness Near Hole

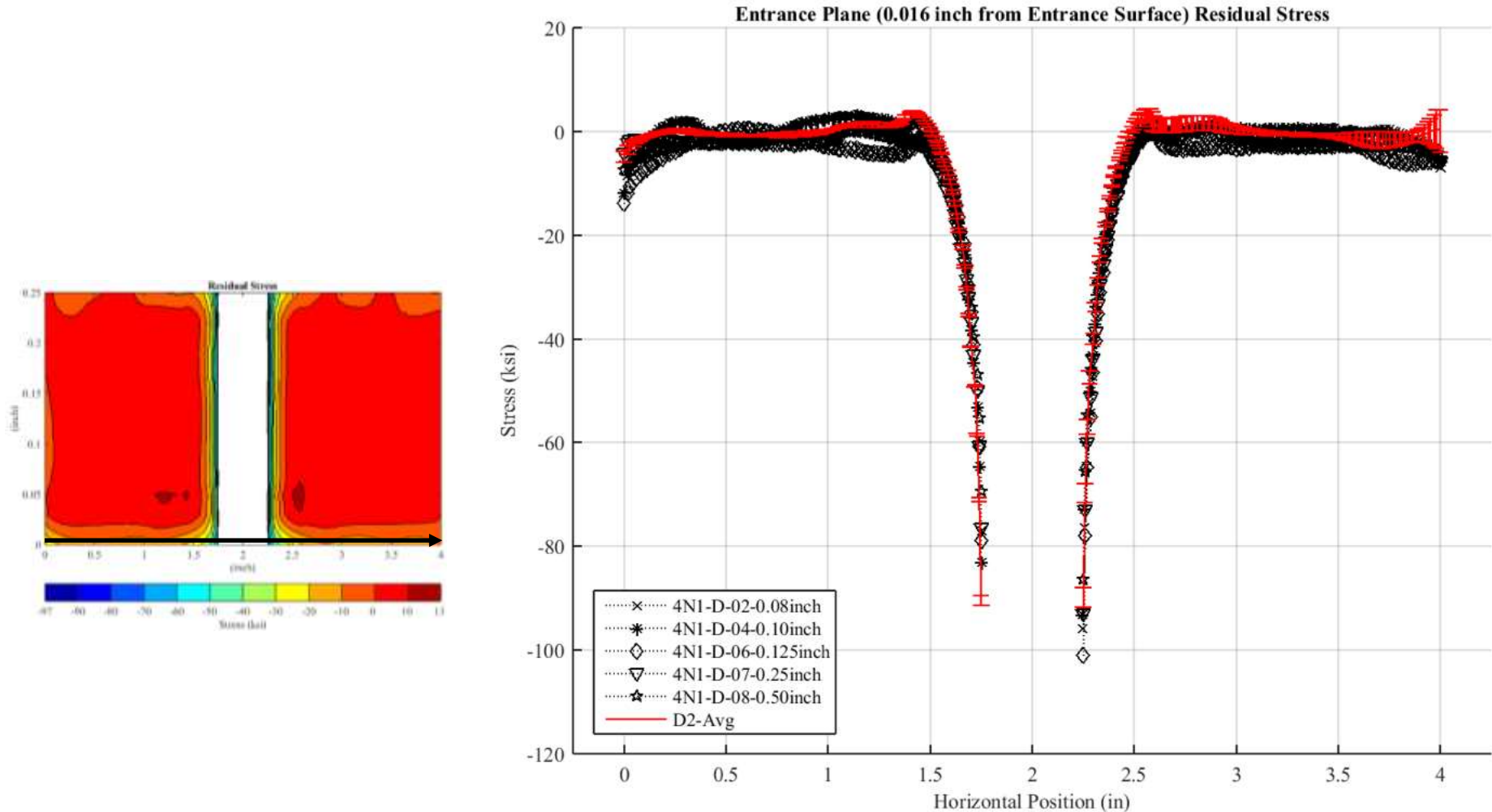


Average Baseline 7075-T651



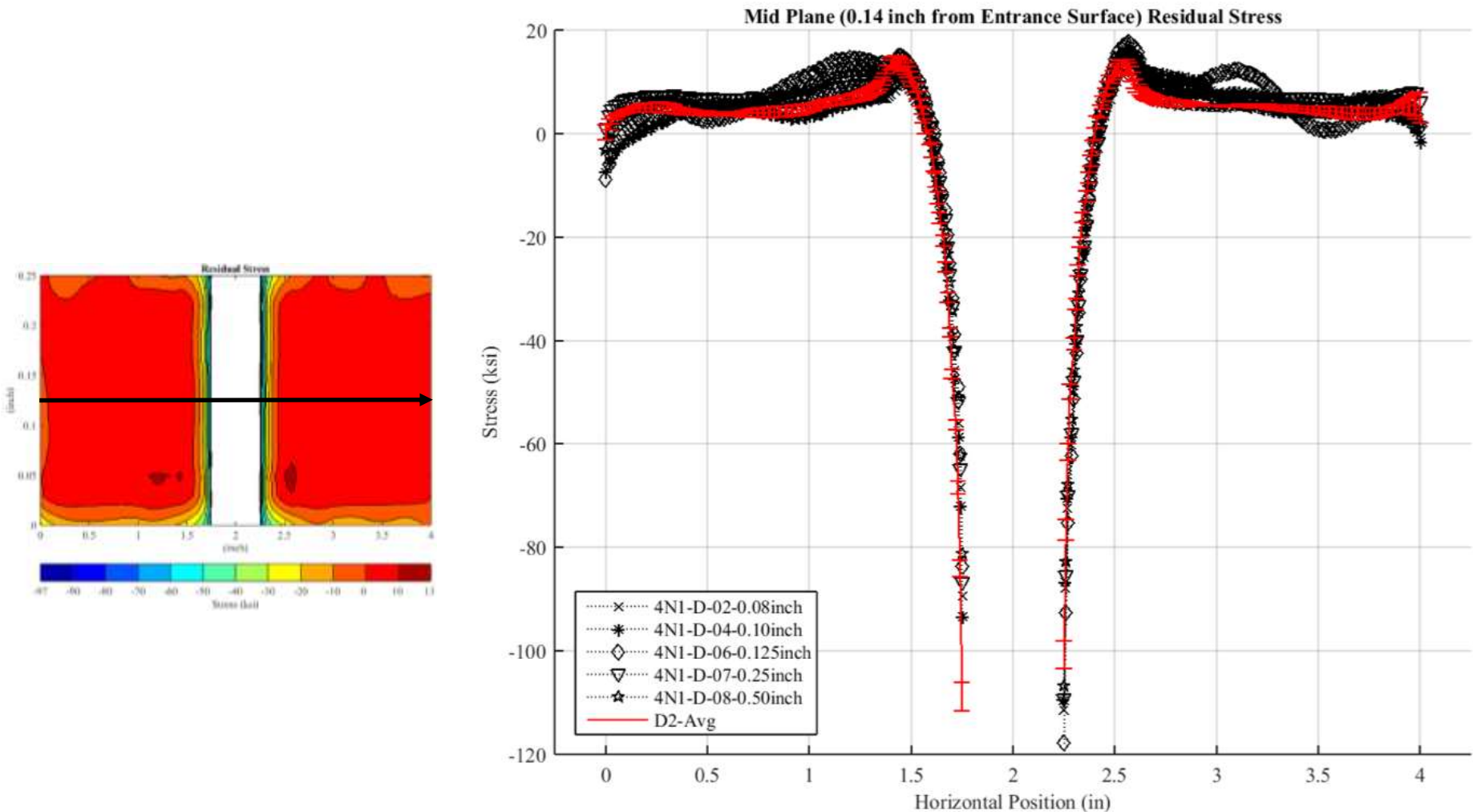
Residual Stresses in 7075-T651

- Line Plots of Stress Radially from Hole



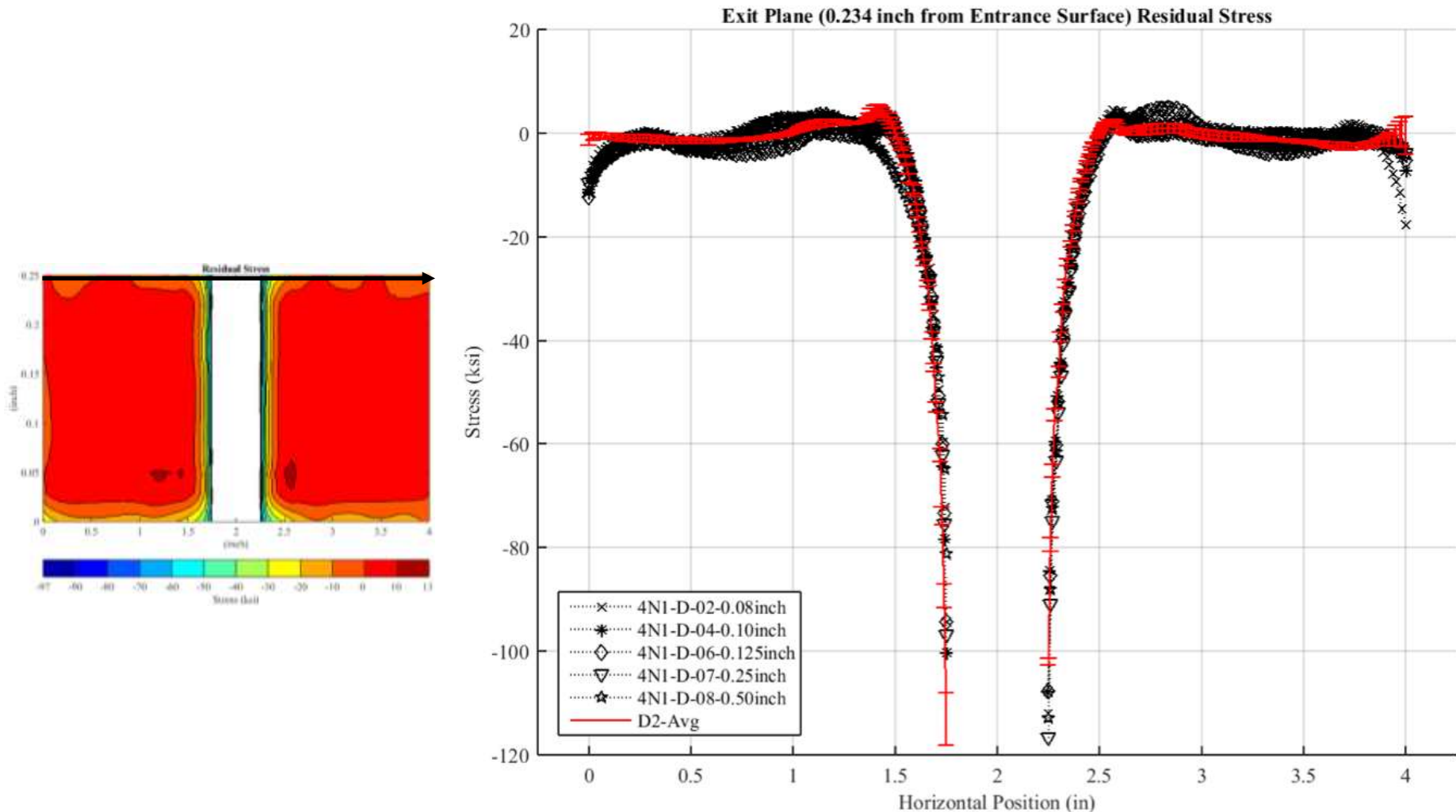
Residual Stresses in 7075-T651

- Line Plots of Stress Radially from Hole



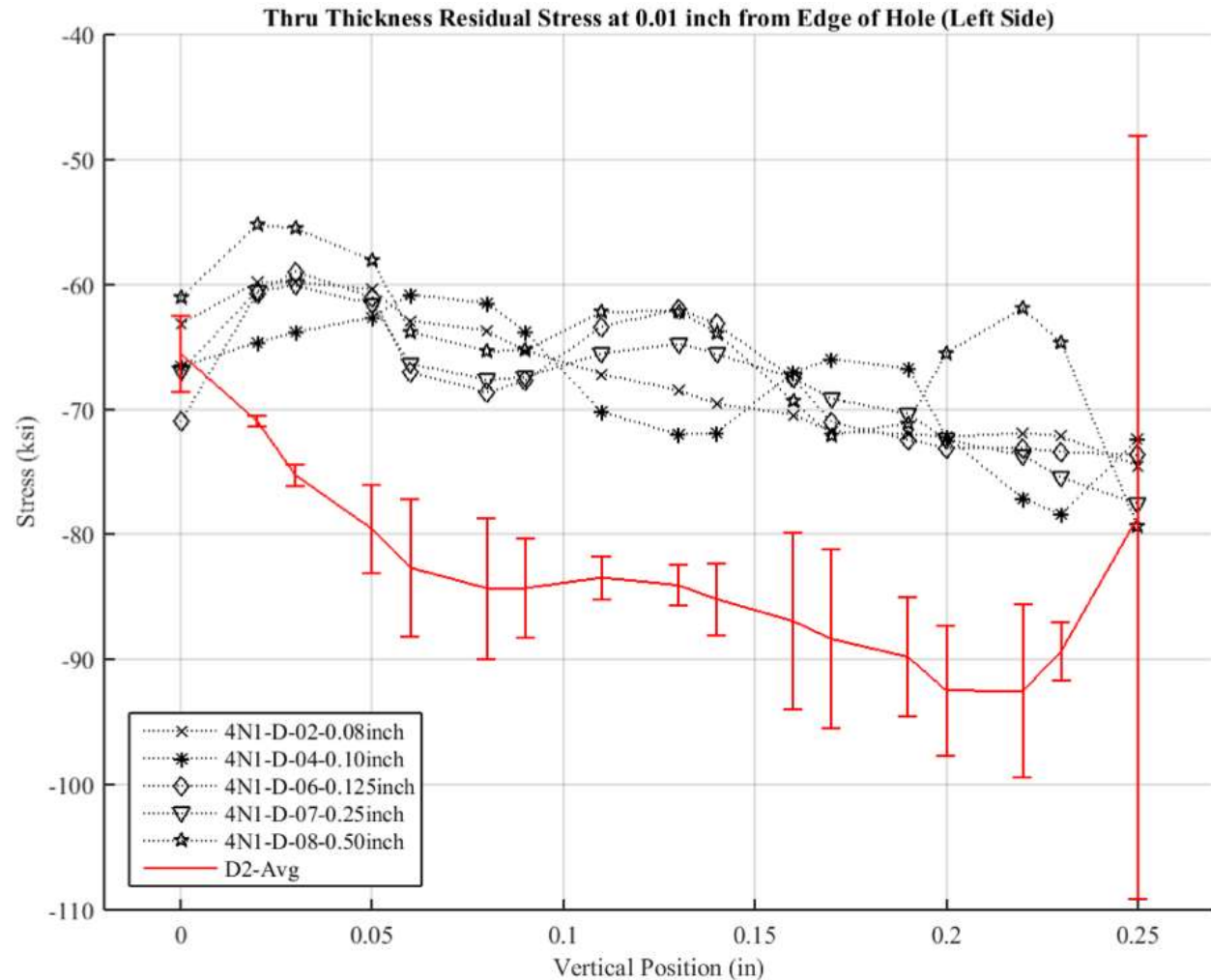
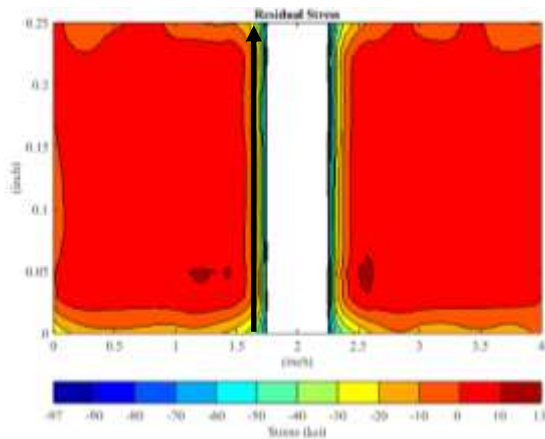
Residual Stresses in 7075-T651

- Line Plots of Stress Radially from Hole



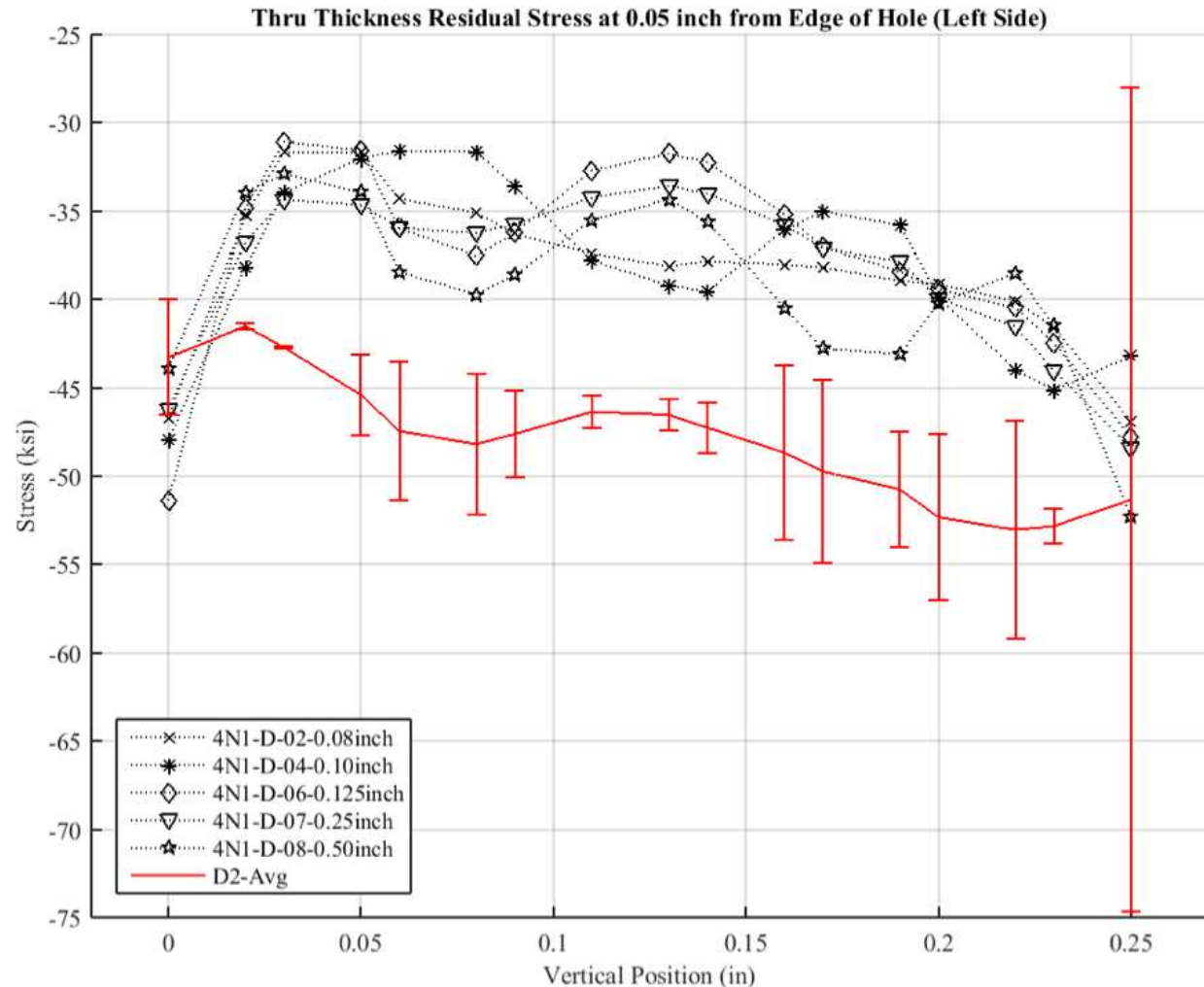
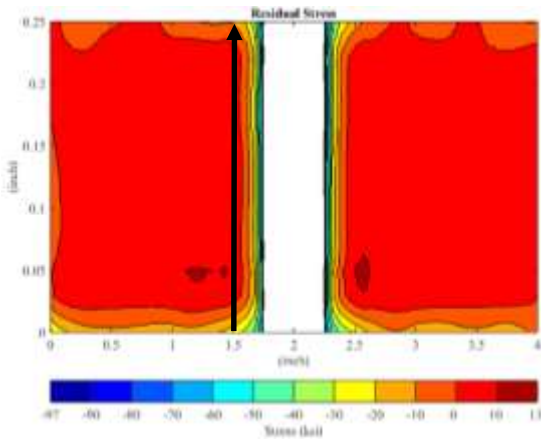
Residual Stresses in 7075-T651

- Line Plots of Stress Through Thickness Near Hole



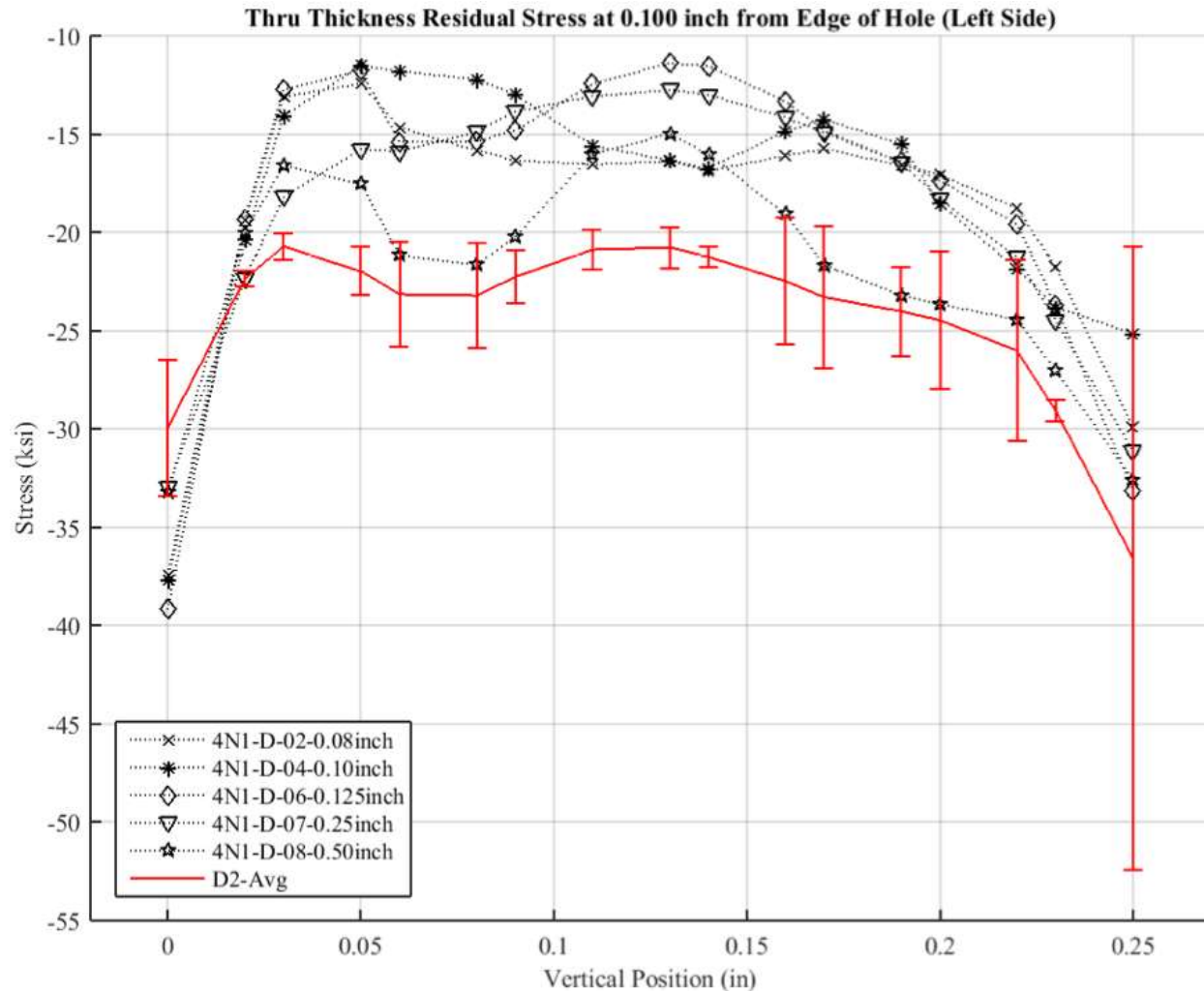
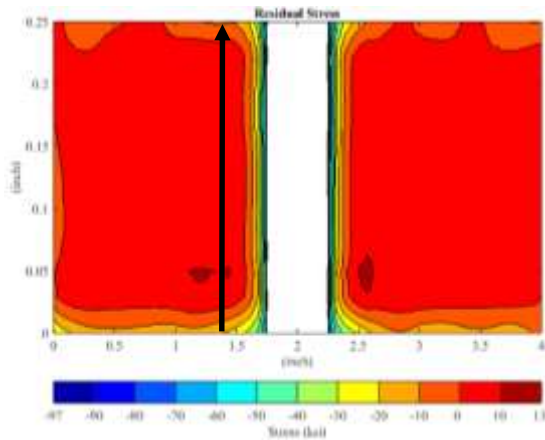
Residual Stresses in 7075-T651

- Line Plots of Stress Through Thickness Near Hole



Residual Stresses in 7075-T651

- Line Plots of Stress Through Thickness Near Hole

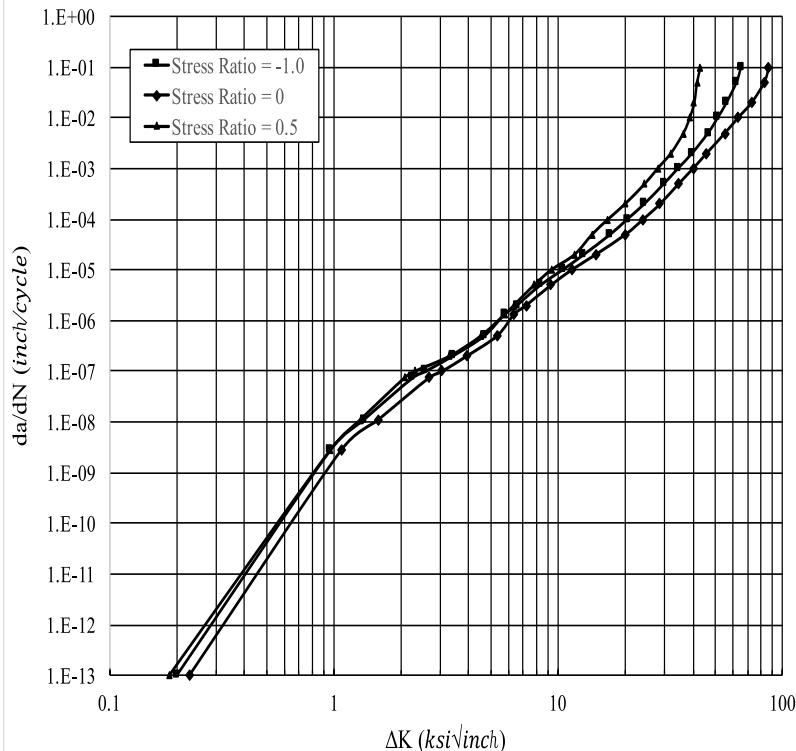


Application of MuPMuC BAMF

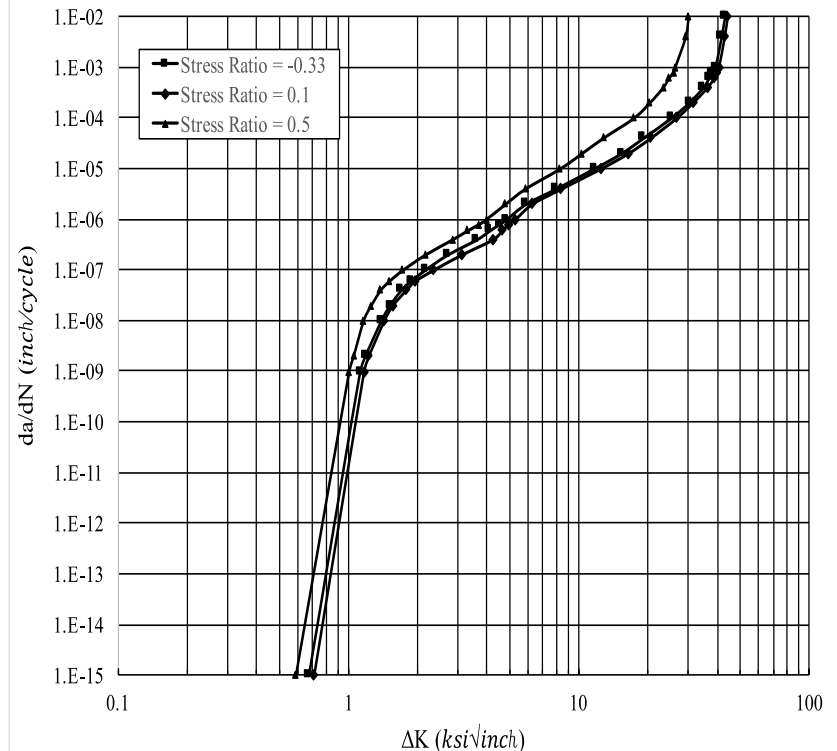
- AFGROW Inputs

- Material file – Tabular look-up file for 2024-T3 and 7075-T6
- Loading – Constant amplitude, $R = 0.1$, 25ksi & 26.5ksi
- Growth increment = 3%

Fatigue Crack Growth Curves for 2024-T351 with Stress Ratios = -1.0, 0.0, and 0.5

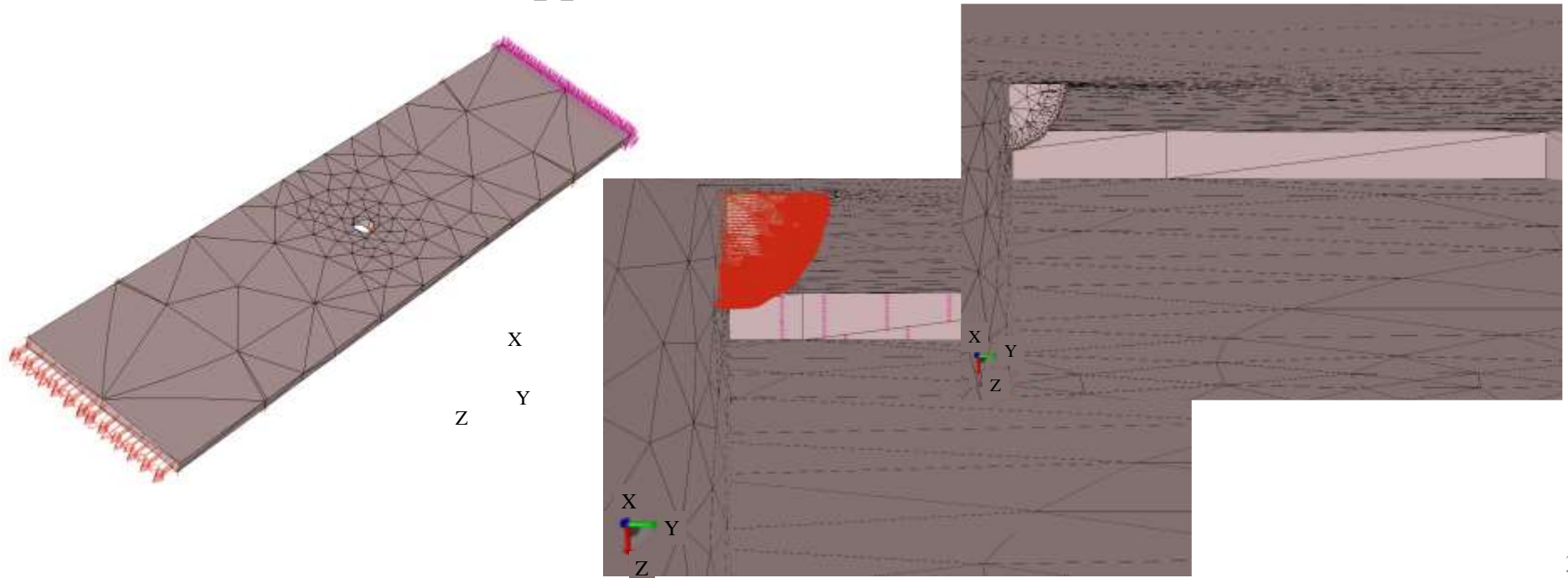


Fatigue Crack Growth Curves for 7075-T651 with Stress Ratios = -0.33, 0.1, and 0.5



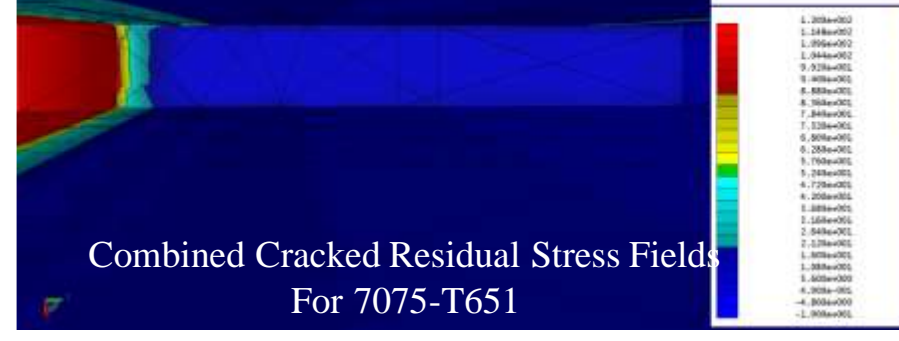
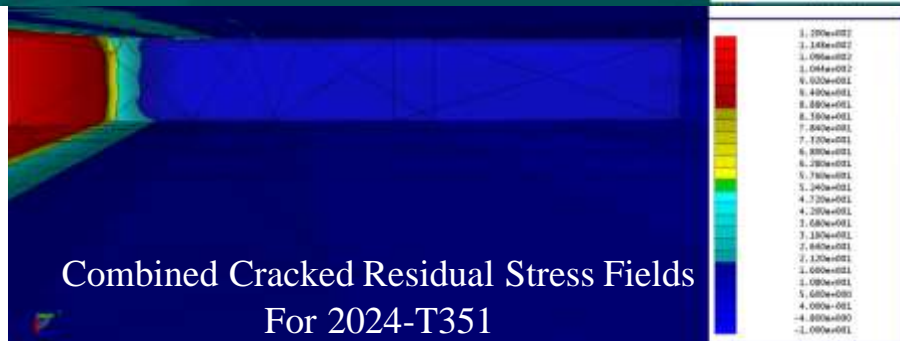
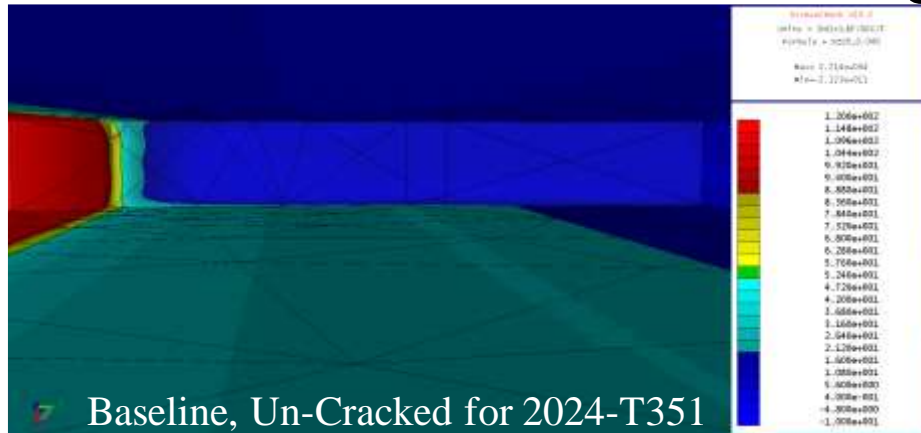
Application of MuPMuC BAMF

- StressCheck[®] Inputs
 - Initial flaw size = 0.0408x0.0486inch (derived via fractography from APES RIF)
 - Fixed constraint and far field traction
 - Meshing defined by BAMF
 - Residual stress applied as a “Crack Face” traction



Development of R.S. Function

- Bi-variant, High Order Polynomial Residual Stress
 - Four variants of residual stress function
 - Baseline, un-cracked
 - Inclusion of effect of fatigue crack
- All Stresses are the Average for the Given Condition



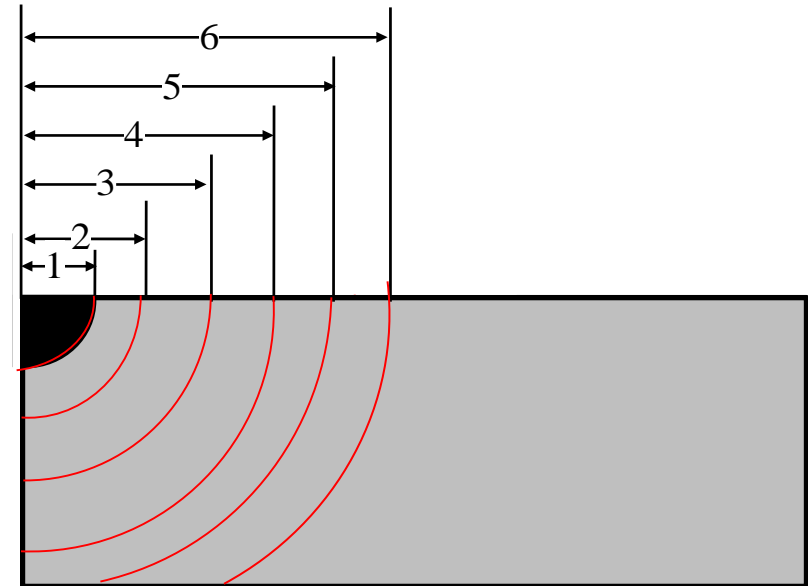
Development of R.S. Function

- Functions were Adjusted to Investigate the Effect of Including the Cracked Residual Stress Fields
 - Approximated shape as quarter-circular (assumption)

Plot Number	Residual Stress from Fautige Cracked Coupons	Distance Applied
1	Baseline Non-Cracked Residual Stress	0.00 - 0.04inch
2	Residual Stress for -01-02 (0.08inch) Crack Length	0.04 - 0.09inch
3	Residual Stress for -03-04 (0.10inch) Crack Length	0.09 - 0.1125inch
4	Residual Stress for -05-06 (0.125inc) Crack Length	0.1125 - 0.1875inch
5	Residual Stress for -07 (0.25inch) Crack Length	0.1875 - 0.375inch
6	Residual Stress for -08 (0.5inch) Crack Length	0.375 - 0.75inch

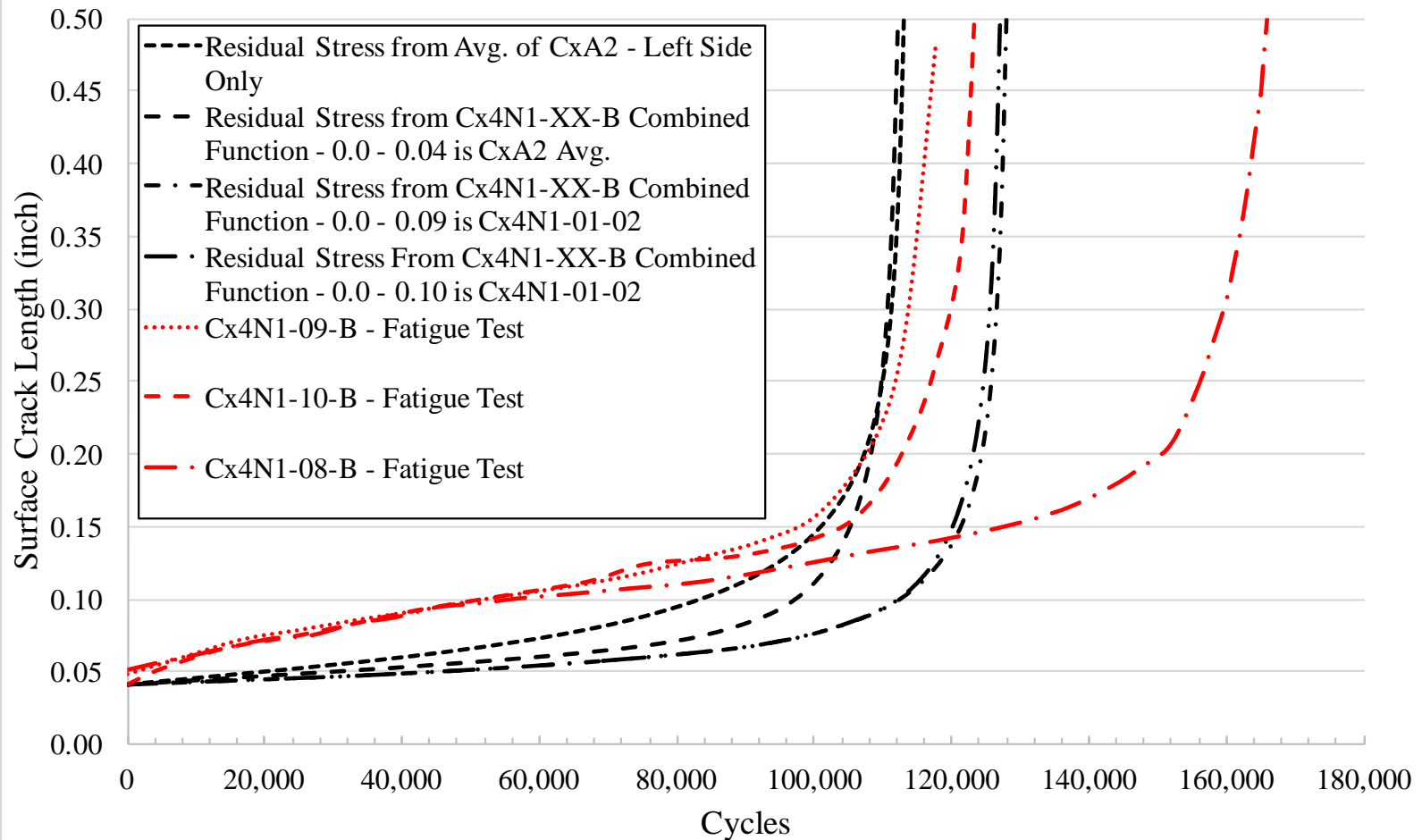
Plot Number	Residual Stress from Fautige Cracked Coupons	Distance Applied
1	Residual Stress for -01-02 (0.08inch) Crack Length	0.00 - 0.09inch
2		
3	Residual Stress for -03-04 (0.10inch) Crack Length	0.09 - 0.1125inch
4	Residual Stress for -05-06 (0.125inc) Crack Length	0.1125 - 0.1875inch
5	Residual Stress for -07 (0.25inch) Crack Length	0.1875 - 0.375inch
6	Residual Stress for -08 (0.5inch) Crack Length	0.375 - 0.75inch

Plot Number	Residual Stress from Fautige Cracked Coupons	Distance Applied
1	Residual Stress for -01-02 (0.08inch) Crack Length	0.00 - 0.10inch
2		
3	Residual Stress for -03-04 (0.10inch) Crack Length	0.10 - 0.125inch
4	Residual Stress for -05-06 (0.125inc) Crack Length	0.125 - 0.25inch
5	Residual Stress for -07 (0.25inch) Crack Length	0.25 - 0.50inch
6	Residual Stress for -08 (0.5inch) Crack Length	0.50 - 0.75inch



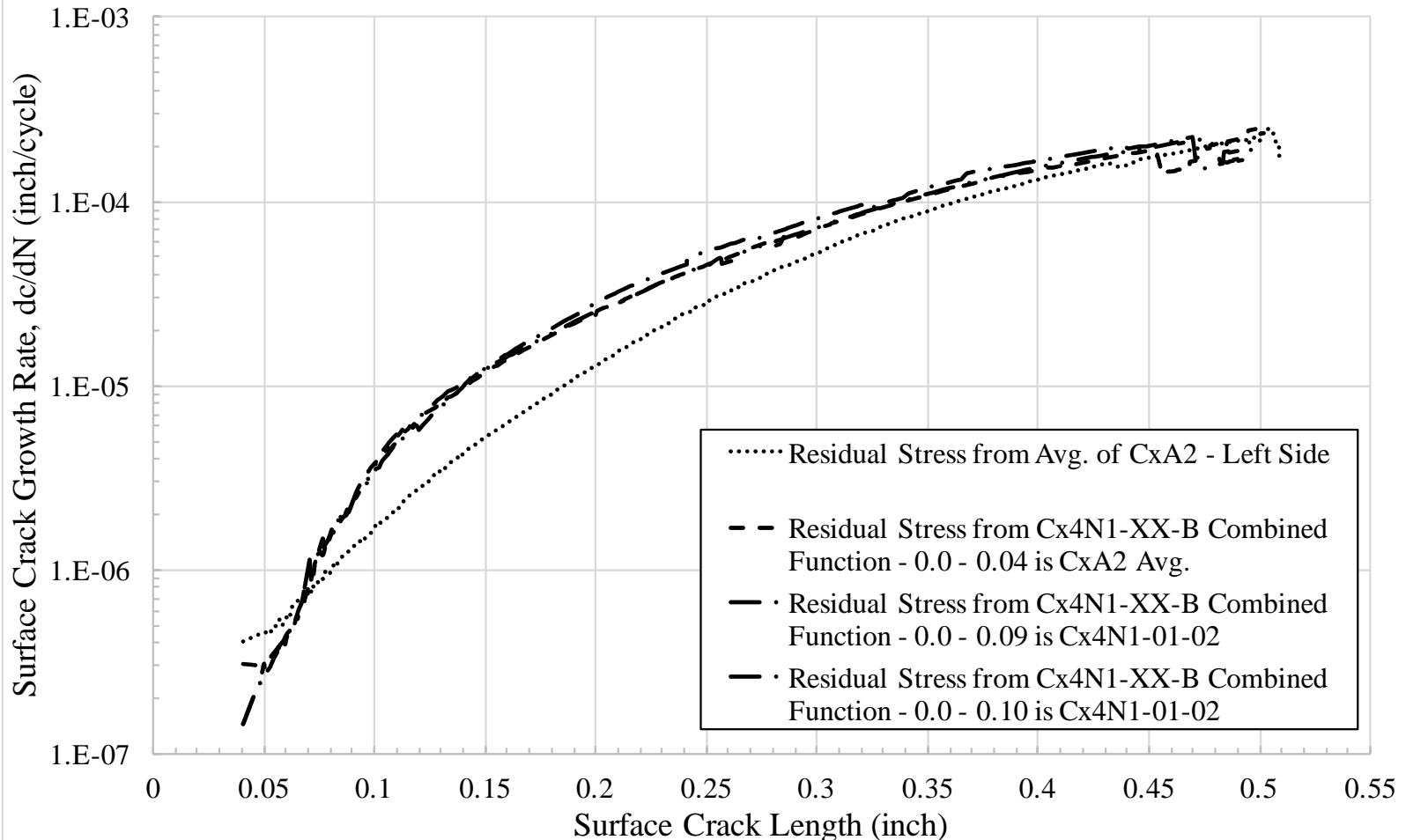
Fatigue Life Predictions

Comparison of Effect of Residual Stress Function to Predict Fatigue Life for the CxA2 "Low" Applied Expansion for 2024-T351 - Material Using Tabular Material File - Coupon - 4.00 inch Wide, 0.25inch Thick, 0.50inch Diameter Hole, Far Field Stress = 25ksi, Stress Ratio = 0.1



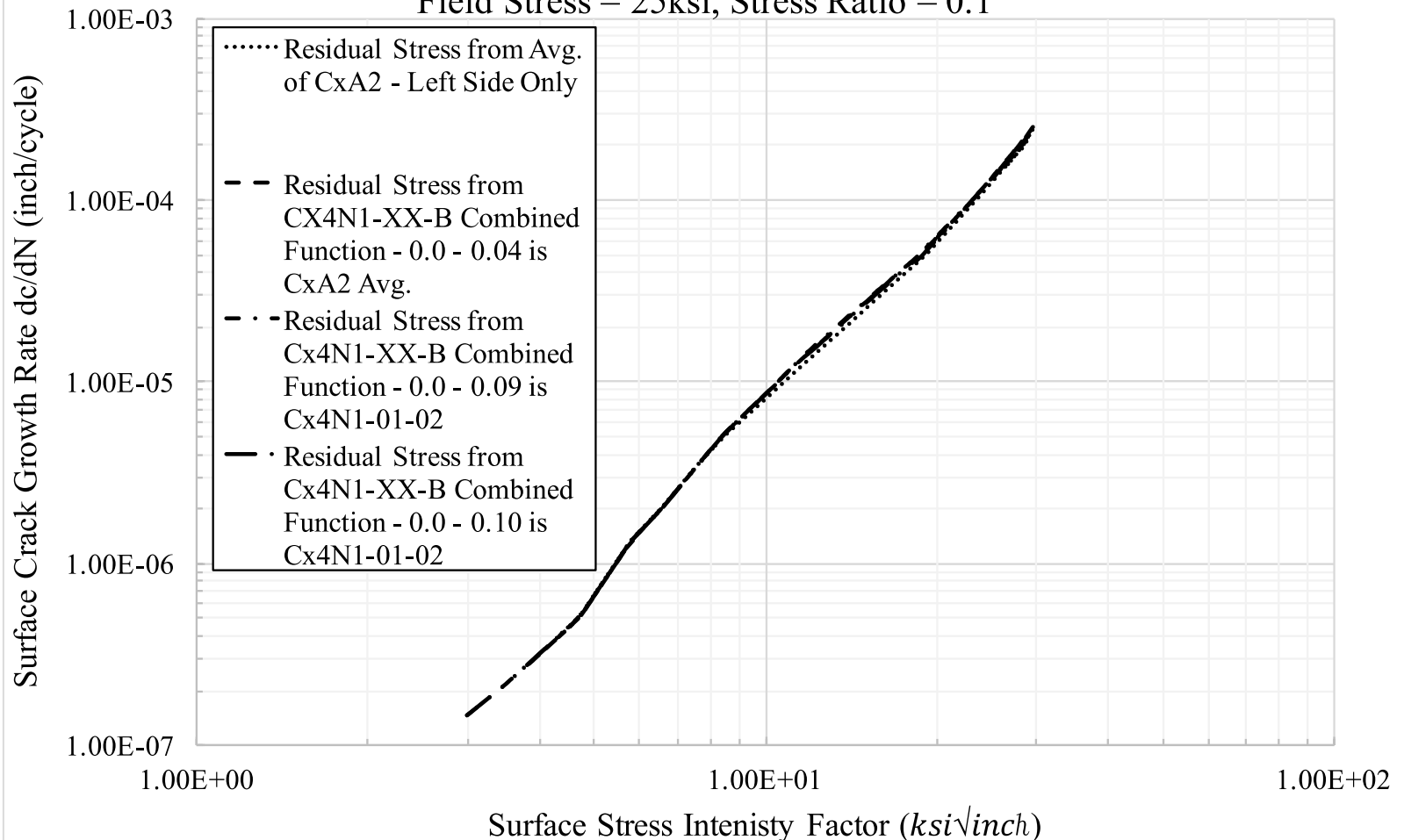
Fatigue Life Predictions

Comparison of Effect Residual Stress Function for the CxA2 "Low" Applied Expansion for 2024-T351 on Crack Growth Rate Material Using Tabular Material File - Coupon - 4.00 inch Wide, 0.25inch Thick, 0.50inch Diameter Hole, Far Field Stress = 25ksi, Stress Ratio = 0.1



Fatigue Life Predictions

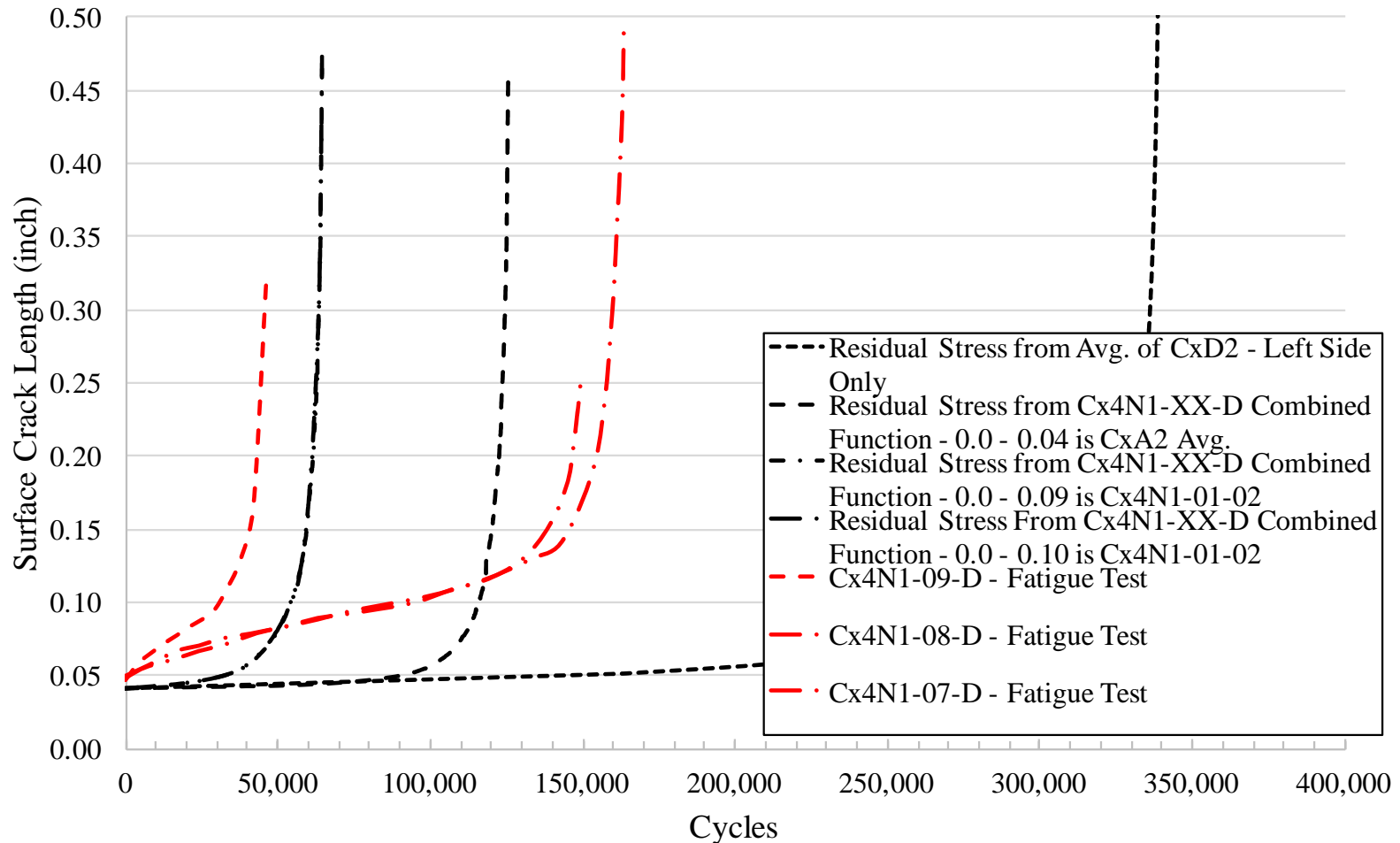
Crack Growth Rate vs Stress Intensity Solution at Entrance Surface Comparing Residual Stress Function for the CxA2 "Low" Applied Expansion for 2024-T351 Material Using Tabular Material - Coupon - 4.00 inch Wide, 0.25inch Thick, 0.50inch Diameter Hole, Far Field Stress = 25ksi, Stress Ratio = 0.1



Fatigue Life Predictions

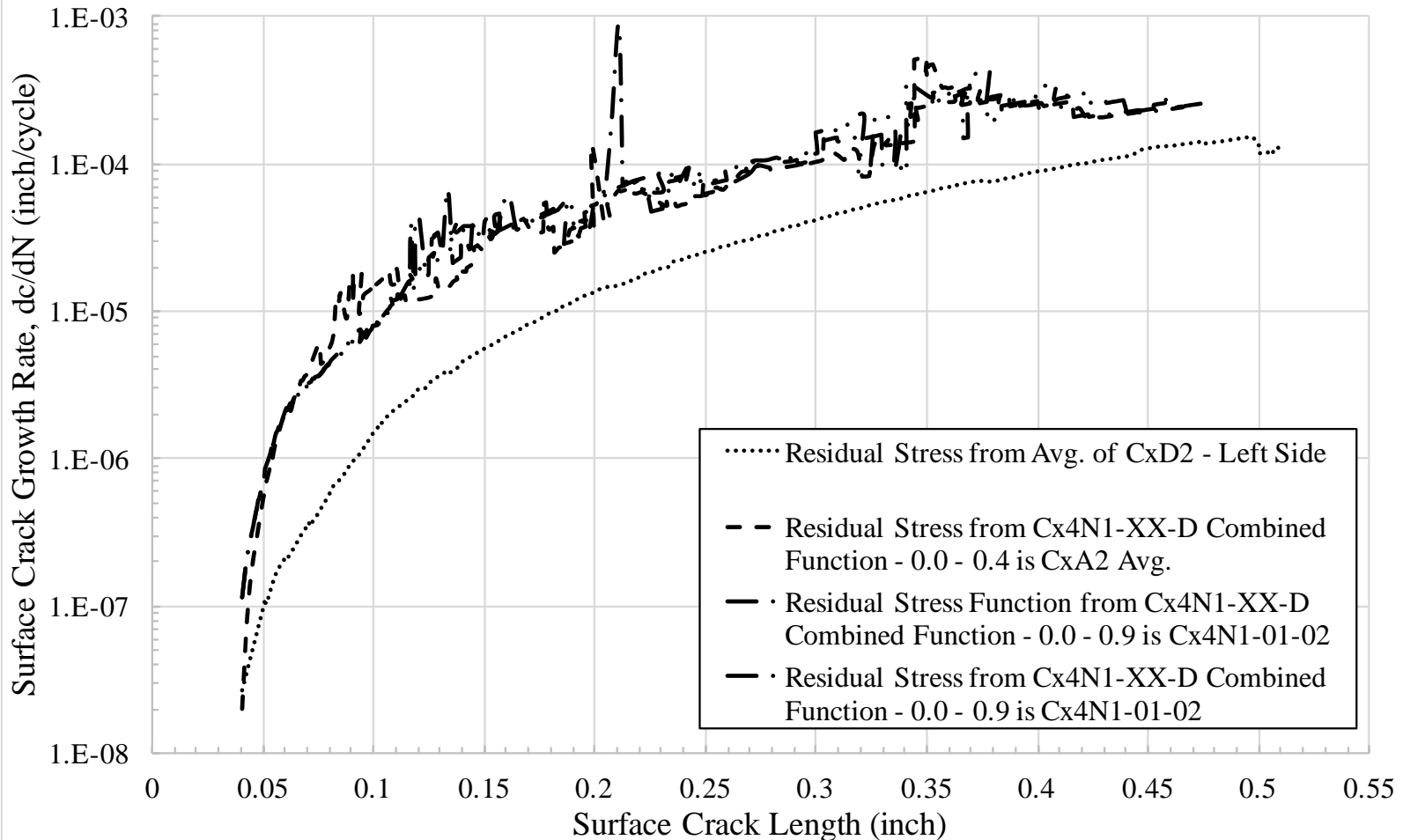
Comparison of Effect of Residual Stress Function to Predict Fatigue Life for the CxD2 "Low" Applied Expansion for 7075-T651 - Material Using Tabular Material File - Coupon - 4.00 inch Wide, 0.25inch Thick, 0.50inch Diameter Hole, Far Field Stress = 26.5ksi, Stress

Ratio = 0.1



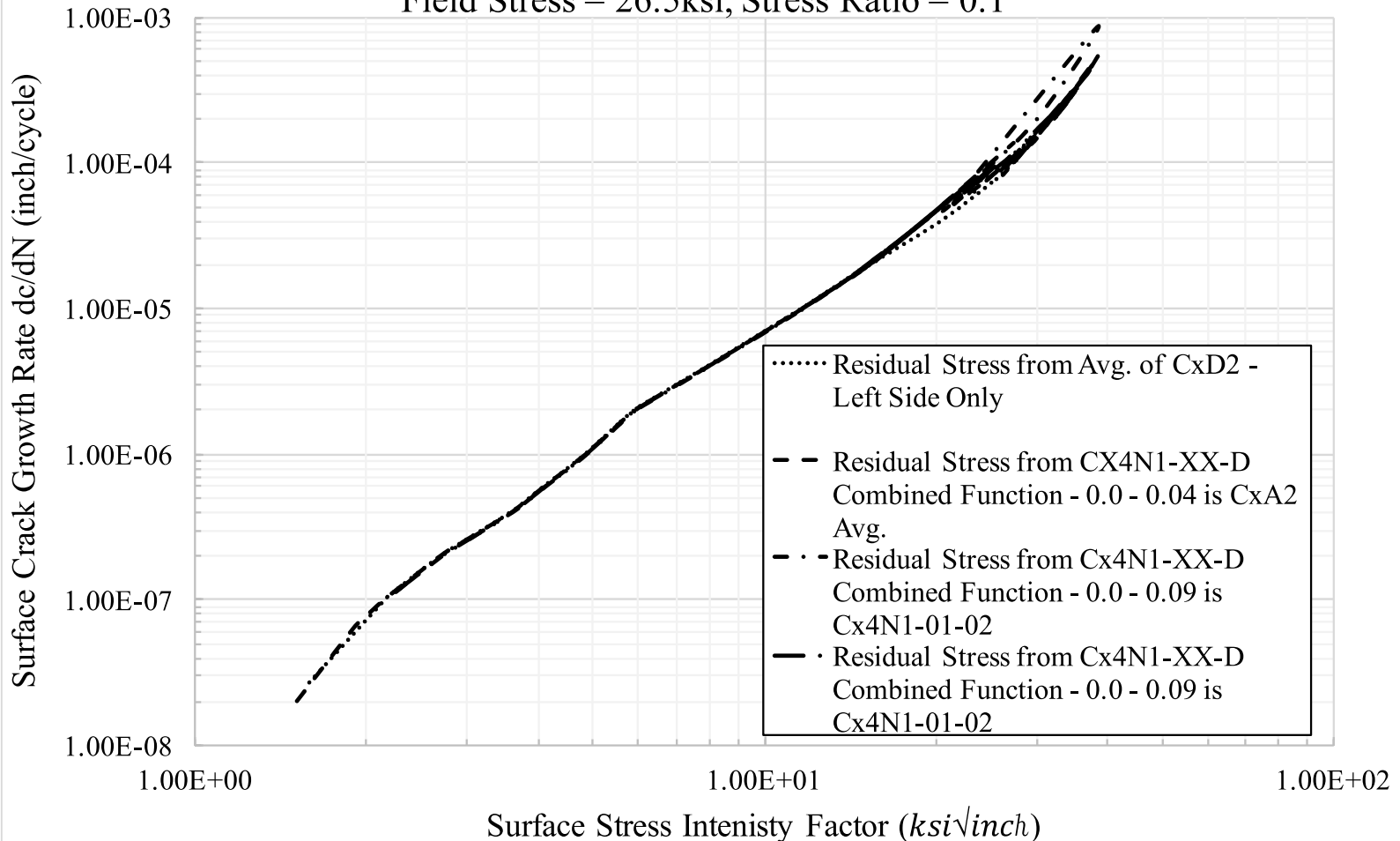
Fatigue Life Predictions

Comparison of Effect Residual Stress Function for the CxD2 "Low" Applied Expansion for 7075-T651 on Crack Growth Rate Material Using Tabular Material File - Coupon - 4.00 inch Wide, 0.25inch Thick, 0.50inch Diameter Hole, Far Field Stress = 26.5ksi, Stress Ratio = 0.1



Fatigue Life Predictions

Crack Growth Rate vs Stress Intensity Solution at Entrance Surface Comparing Residual Stress Function for the CxD2 "Low" Applied Expansion for 7075-T651 Material Using Tabular Material - Coupon - 4.00 inch Wide, 0.25inch Thick, 0.50inch Diameter Hole, Far Field Stress = 26.5ksi, Stress Ratio = 0.1



Conclusions

- It is Possible to Capture the Effect of a Fatigue Crack via the Contour Method
- A Fatigue Crack has an Effect on the Residual Stress Field Introduced via the Cold Expansion (Cx) Process
 - For 2024-T351 the magnitude of the effect is related to crack size
 - For 7075-T651 the magnitude effect is does not seem to be related to the crack size
- Inclusion of the Modified Residual Stress State into a Fatigue Life Prediction Adjusts the Life
 - For both the 2024-T351 and 7075-T651 the effect moves the prediction closer to the average tested fatigue life

Recommendations

- Develop Standard Statistical Methods for Quantifying “Difference” in 2D and 3D Data Fields
- Perform Additional Design Space Measurements of Cracked Coupons to Determine the Bounds of Application
- Develop Mathematical Representation of Effect of Crack in 3D Space
 - Develop methods for adjusting residual stress field to account for the effect of the crack, thus reducing the extensive “measurement” burden
- Look at Different Shape Approximations for Effected Residual Stress Field

Questions?



References

1. Prime, M.B., (2001). “*Cross-Sectional Mapping of Residual Stresses by Measuring the Surface Contour After a Cut*”, Journal of Engineering Materials and Technology, Vol. 123, Issue 2, pg. 162-168.
2. Bueckner, H., (1958). “*The Propagation of Cracks and the Energy of Elastic Deformation*”, Transactions of the American Society of Mechanical Engineers, Vol. 80, pg. 1225-1230.
3. Prime, M.B., DeWald, A.T., (2013). The Contour Method, Chapter 5, Practical Residual Stress Measurement Methods, John Wiley & Sons Ltd., West Sussex, United Kingdom.