

# 2016 AFGROW Workshop

## Application of Uncertainty Quantification for Residual Stress Measurement at a Cold Expanded Hole



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# Acknowledgements

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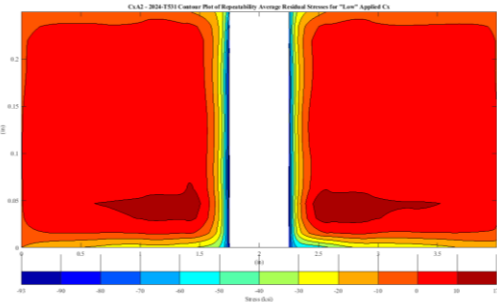
# Presentation Outline

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- Uncertainty and Implementation
- Contour Method – Sources of Uncertainty
- Residual Stress at Cx Holes – “Low” Applied Cx
- Results of Repeatability Measurement Uncertainty
  - Effects of uncertainty on fatigue crack growth predictions
- Results of Single Measurement Uncertainty
  - Effects of uncertainty on fatigue crack growth predictions
- Some Comments on Displacements to Stresses
- Future Work
- Conclusions

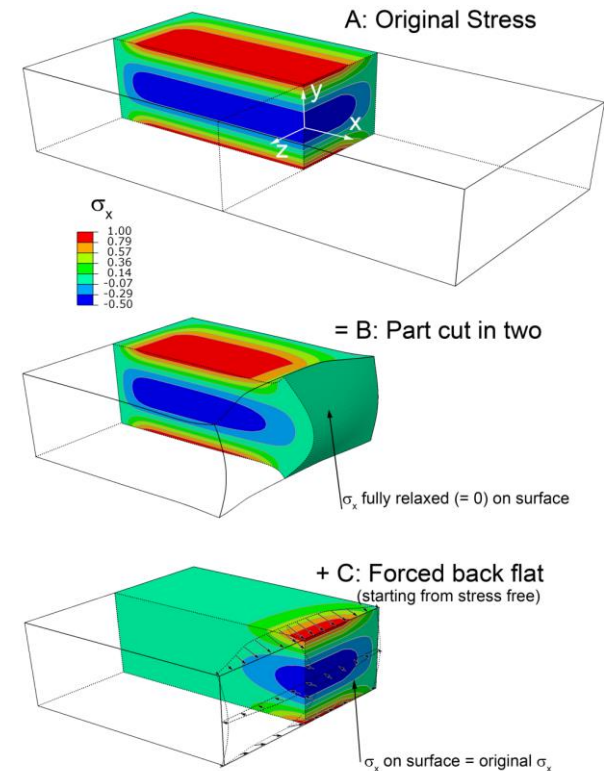
# Keys to Implementation

- Deep Residual Stresses/Self Stresses are a Physics-based Process
  - Plastic deformation
  - Local yielding
- Define/Quantify Parameters of Influence
  - Percent expansion
  - Local stress state
  - Applied loading (tension or compression dominated?)
- Understand and Quantify, **Statistically**, Bounds of Application
  - More accurate modeling of condition
  - Ability to more accurately assess risks and benefits



# Contour Method

- Developed by Prime, M., Hill, M. at Los Alamos Labs
- First Published in 2001<sup>1</sup>
- Based upon the Bueckner's Superposition Principle of Stresses<sup>2</sup>
- Composed of 4 Major Steps
  - Cut using wire EDM
  - Measure using CMM or laser profilometer
  - Perform alignment, averaging, and fitting – [Johnson, G. Dissertation](#)
  - Apply final fit surface as boundary constraints to FEA
  - Solve for stresses within body



Idealized Conceptual Implementation of Contour Method<sup>3</sup>

# Sources of Uncertainty in Contour

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- Two Main Types of Uncertainty or Error
  - Random— *three main causes, lack of equipment sensitivity, noise in measurement, imprecise definition*
  - Systematic— *these can not be revealed through statistical analysis, bulge error, cutting irregularities, metrology*
- Two Types of Random “Uncertainty” Defined Looked at
  - “Modeling” or “Function” uncertainty
  - “Displacement” uncertainty
- Root Sum Square Uncertainty<sup>4</sup>

$$U_{RSS}(x, y) = \sqrt{U^2 U_{Disp}^2(x, y) + U_{Model}^2(x, y)}$$

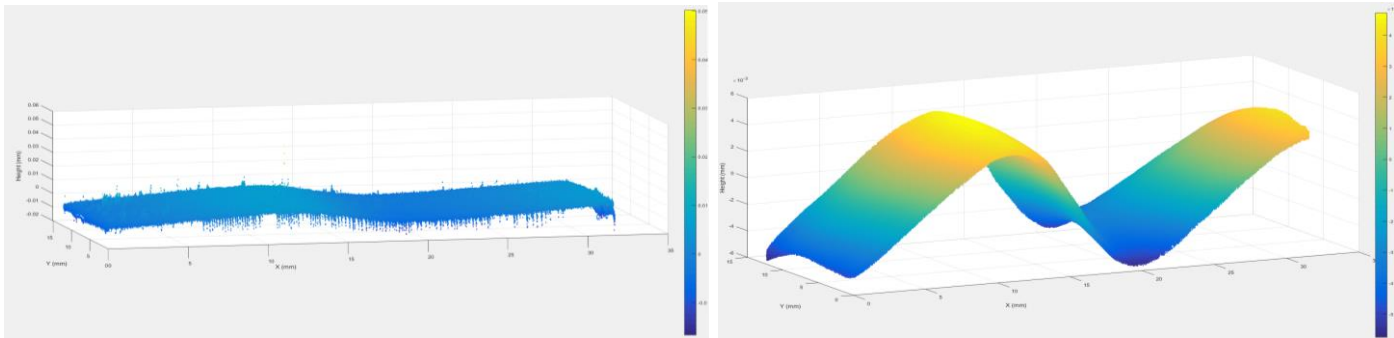
# Residual Stress Results – Key Parameters

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- Data Reduction Key Parameters
  - Both sides of the hole solved together<sup>3</sup> – lesson learned
  - Outliers removed via Modified Thompson Tau method
  - Knot density – 4 knots along short side, 4 knots along long side
  - 3<sup>rd</sup> Order B-Splines within Matlab to fit between hard knot locations
  - 16 Elements through thickness
    - Element type – C3D8I – Incompatible mode eight-node brick
    - Convergence of mesh based on solution and time
  - All averages and standard deviations were solved at exact same node on each model
    - Enables easy calculations of averages and uncertainties

# Removing Noise from Data Cloud

- How to Determine “Noise” from Appropriate Data
  - Data come with inherent noise from surface roughness, effects of the wire cutting, dust, noise from the measurement device
  - Outliers removed via Modified Thompson Tau Method

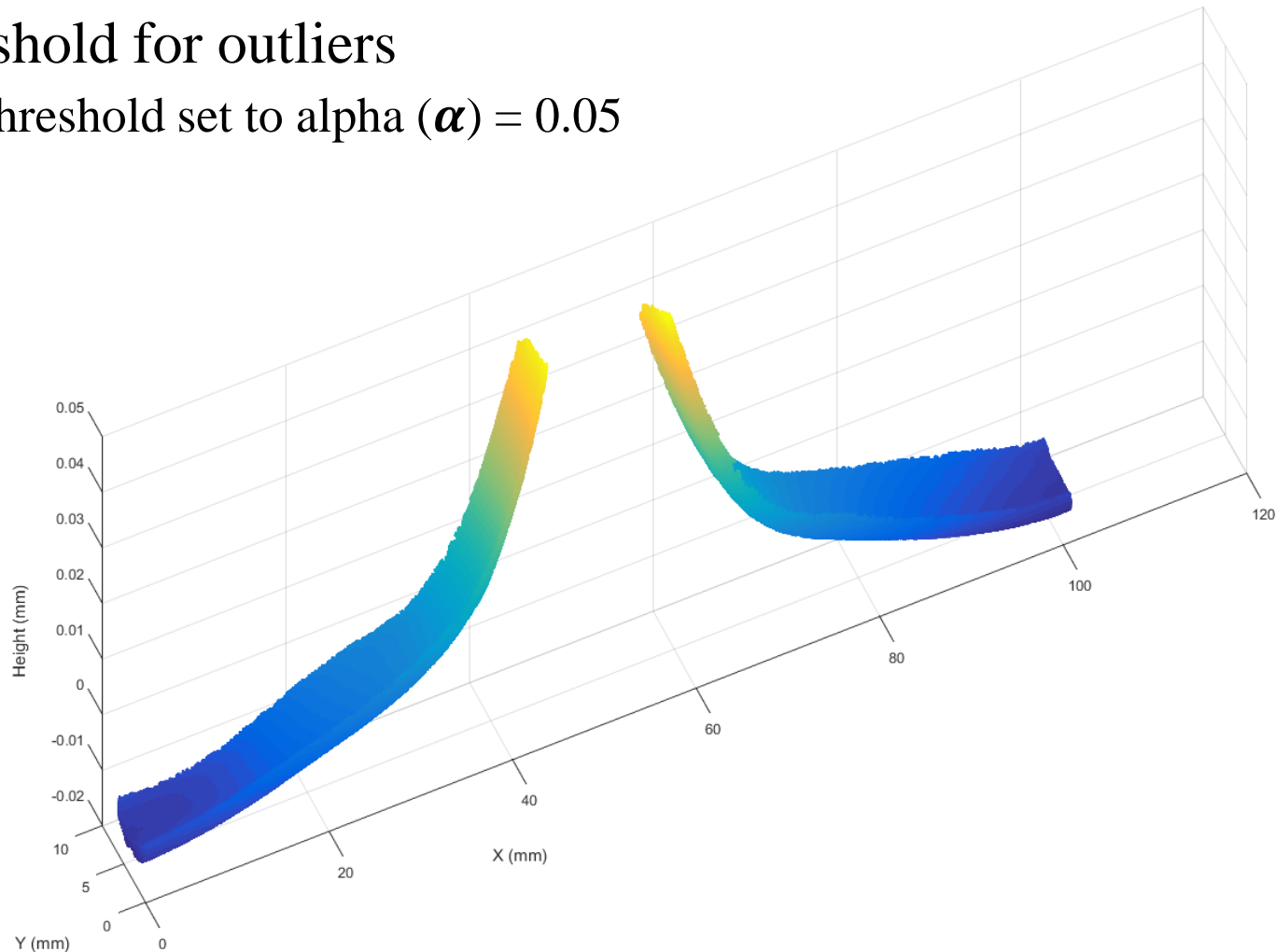


- High potential to remove data that is valid without a process for removing “statistically significant outliers”
- Original AFRL code required each point to be removed by hand and based on “engineering judgement”



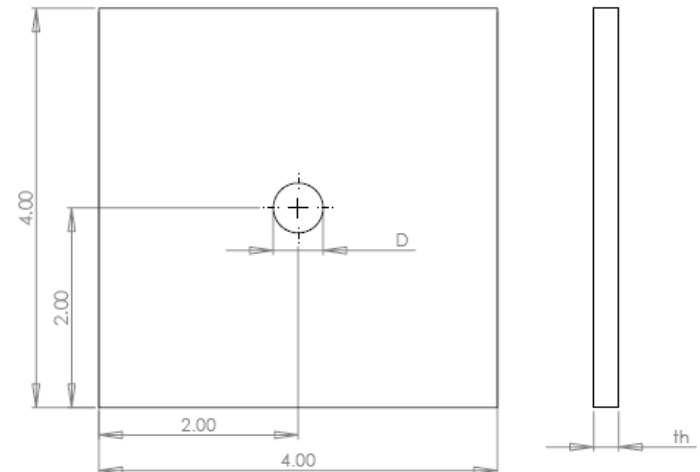
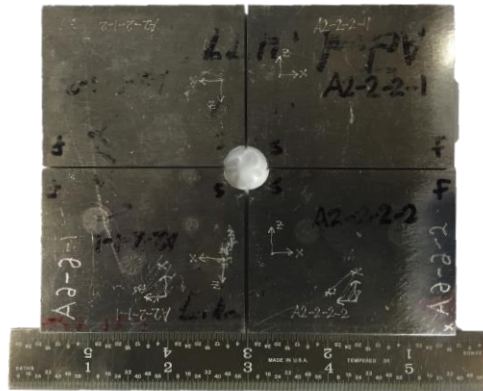
# Modified Thompson Tau Method

- Uses Hypothesis Testing to Determine Outliers
  - ASTM Standard E178 provides recommendations for selecting threshold for outliers
    - Threshold set to alpha ( $\alpha$ ) = 0.05



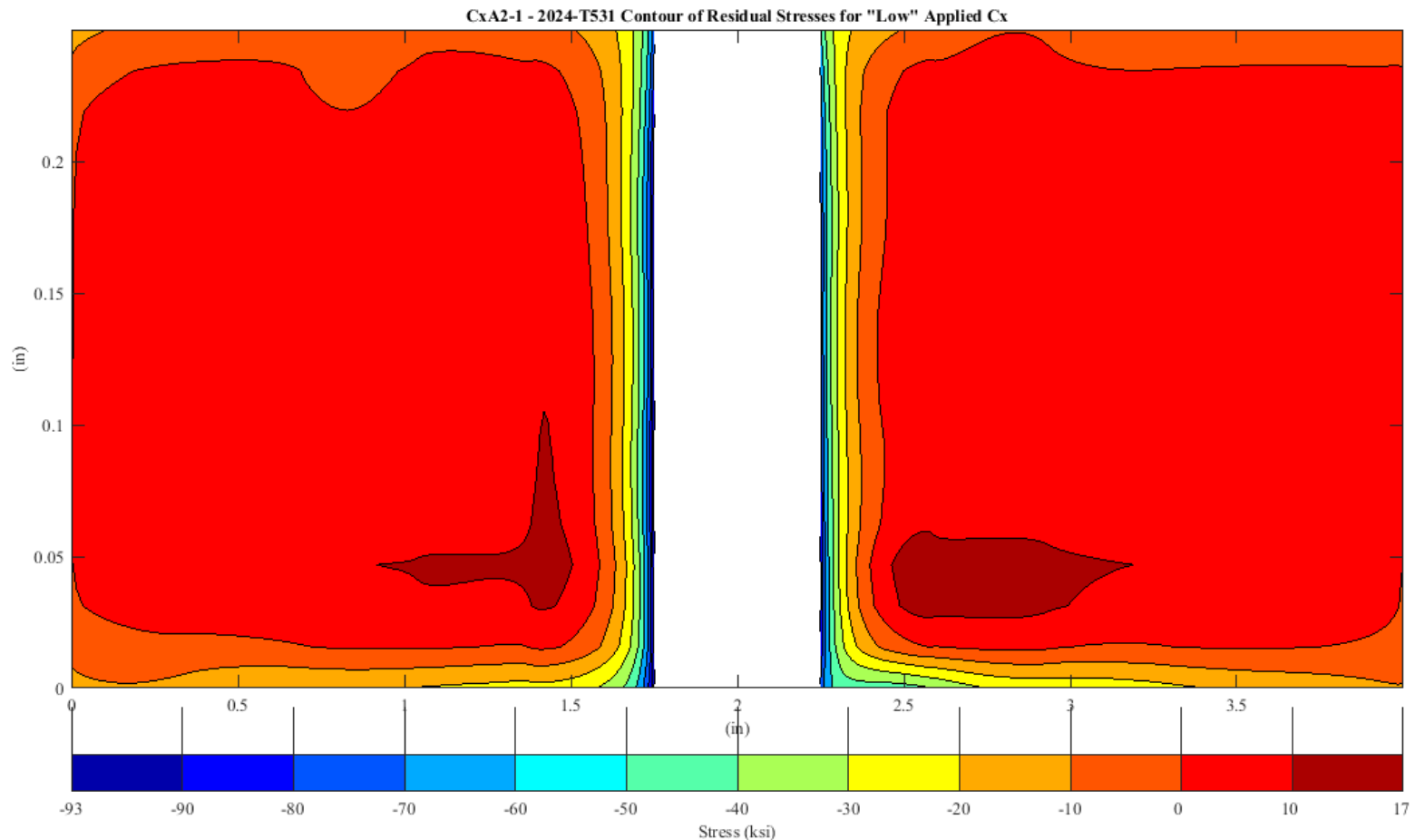
# Results of “Low” Applied Cx

- 5 Replicates Were Produced for the “Low” Applied Cx Level in Al 2024-T351, 0.25in Thick, Approx. 0.50inch Hole Diameter
  - The “low” applied expansion represents 3.14-3.19%
  - Initial hole diameter = 0.4772-0.4774in
  - Mandrel diameter = 0.4684in with sleeve thickness = 0.0120in
  - Post Cx diameter = 0.4876-0.4884in
  - Avg. post Cx diameter = 0.48783-0.48835inch
  - Residual expansion = 2.33%-2.34%

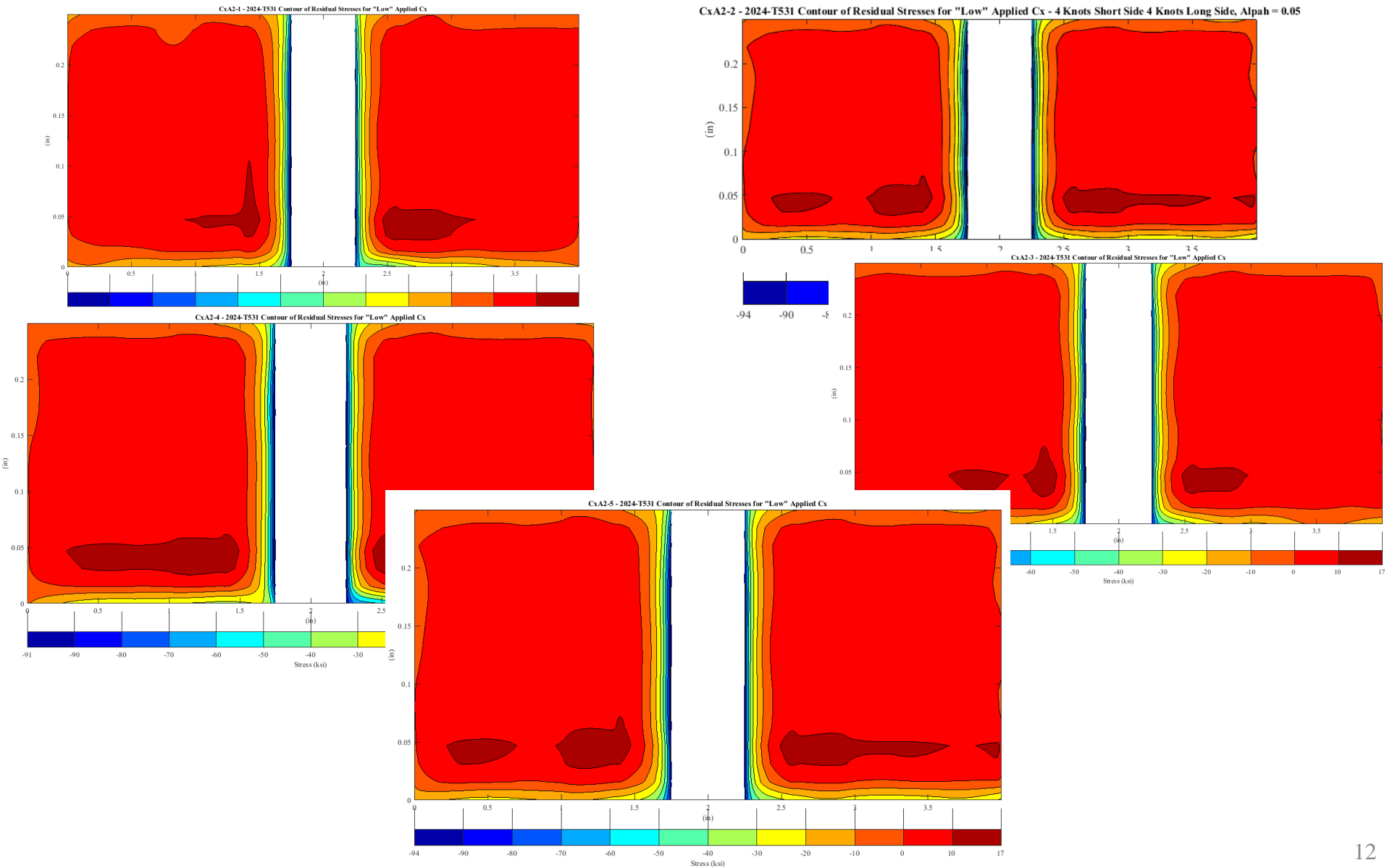


# Repeatability Uncertainty

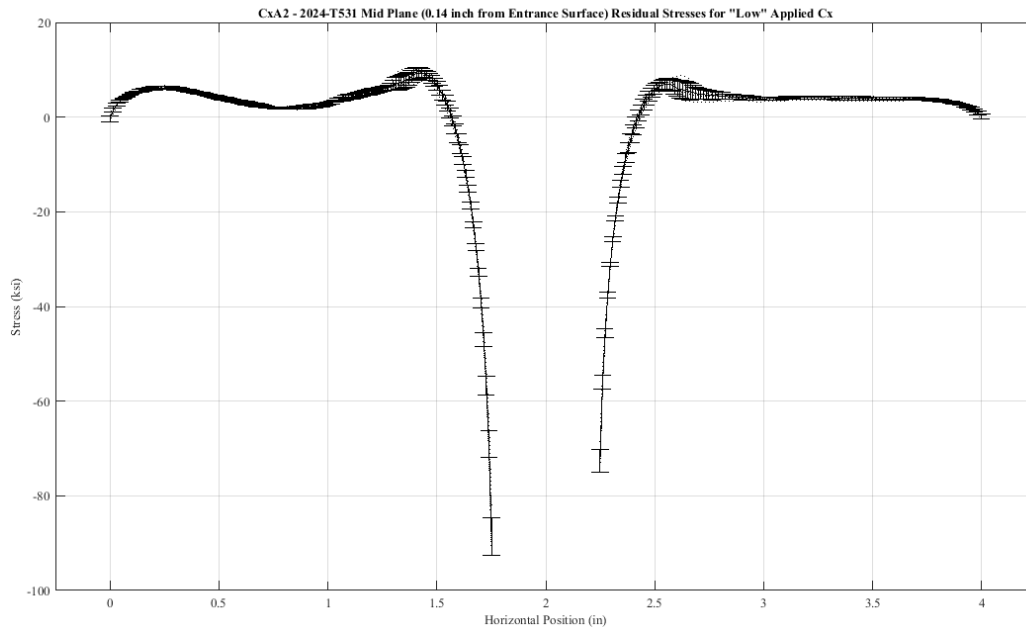
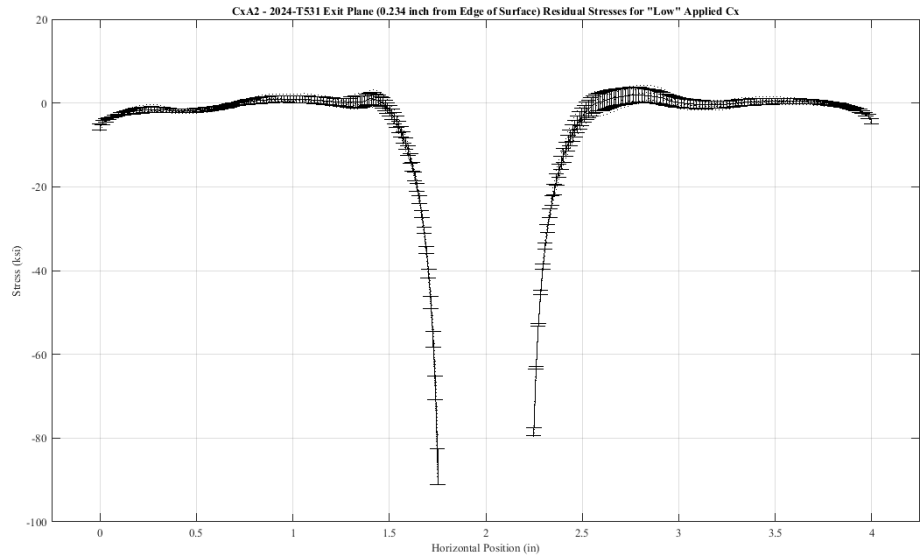
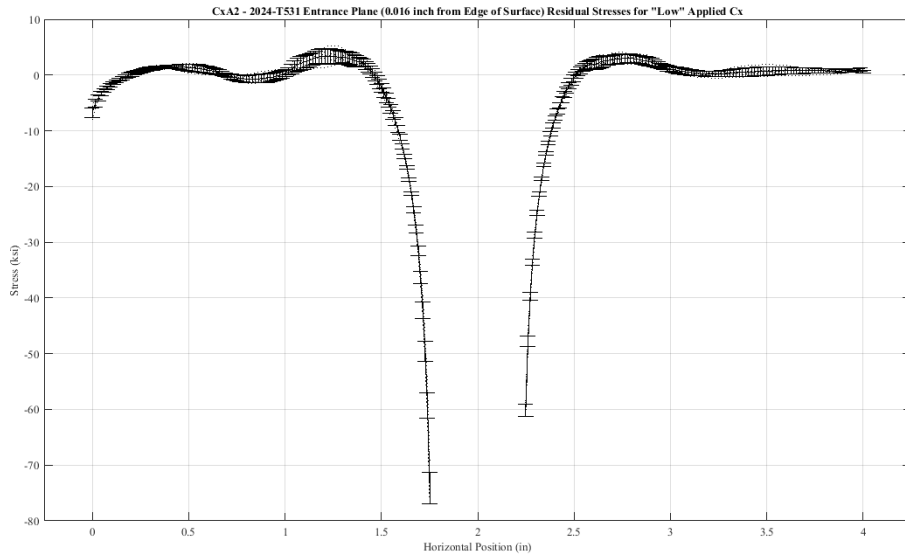
- From Replicate Conditions Each Contour Measurement was Performed Using Same Parameters
- Uncertainty of Single Standard Deviation from Mean



# Residual Stress Results for 2024

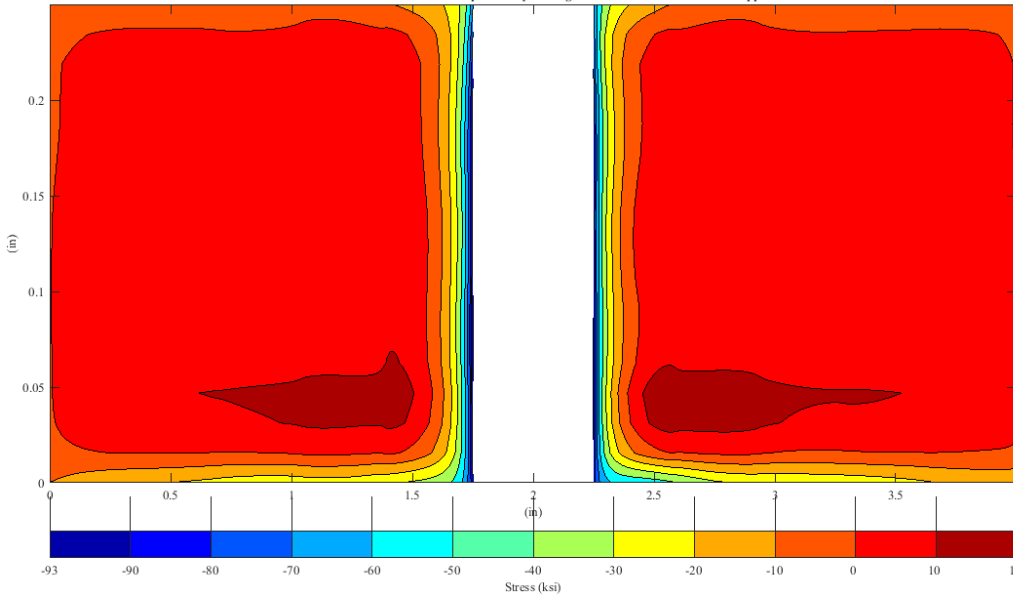


# Residual Stress Results for 2024

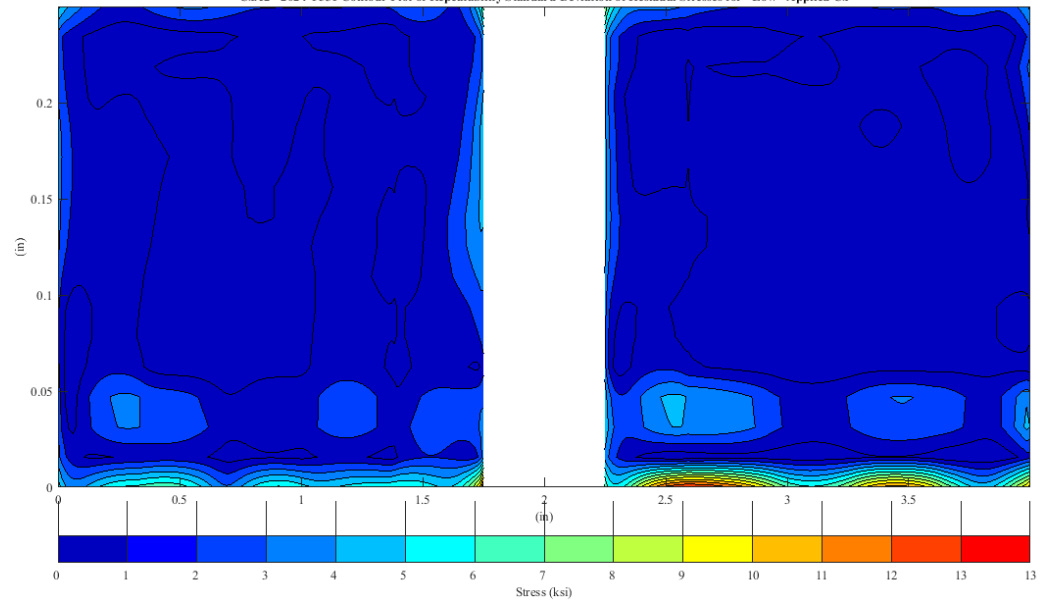


# Average & Standard Deviation

Cx2 - 2024-T531 Contour Plot of Repeatability Average Residual Stresses for "Low" Applied Cx

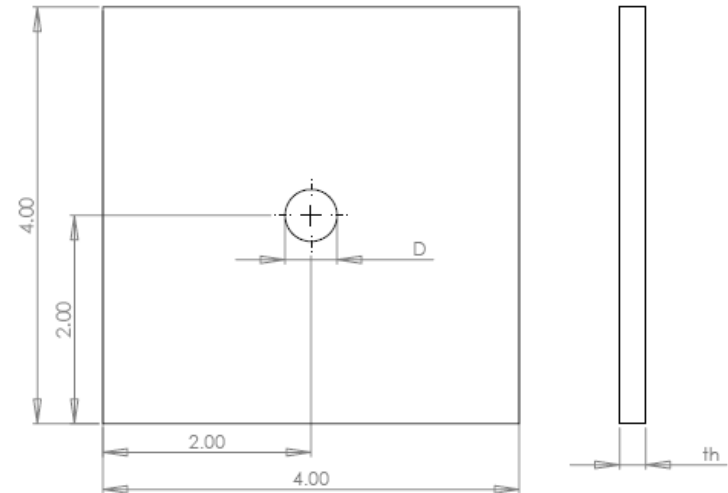
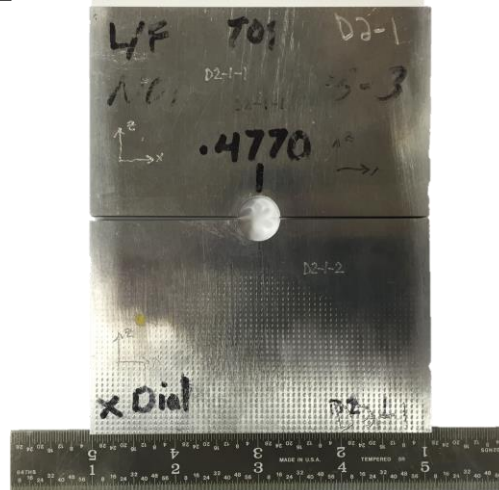


Cx2 - 2024-T531 Contour Plot of Repeatability Standard Deviation of Residual Stresses for "Low" Applied Cx



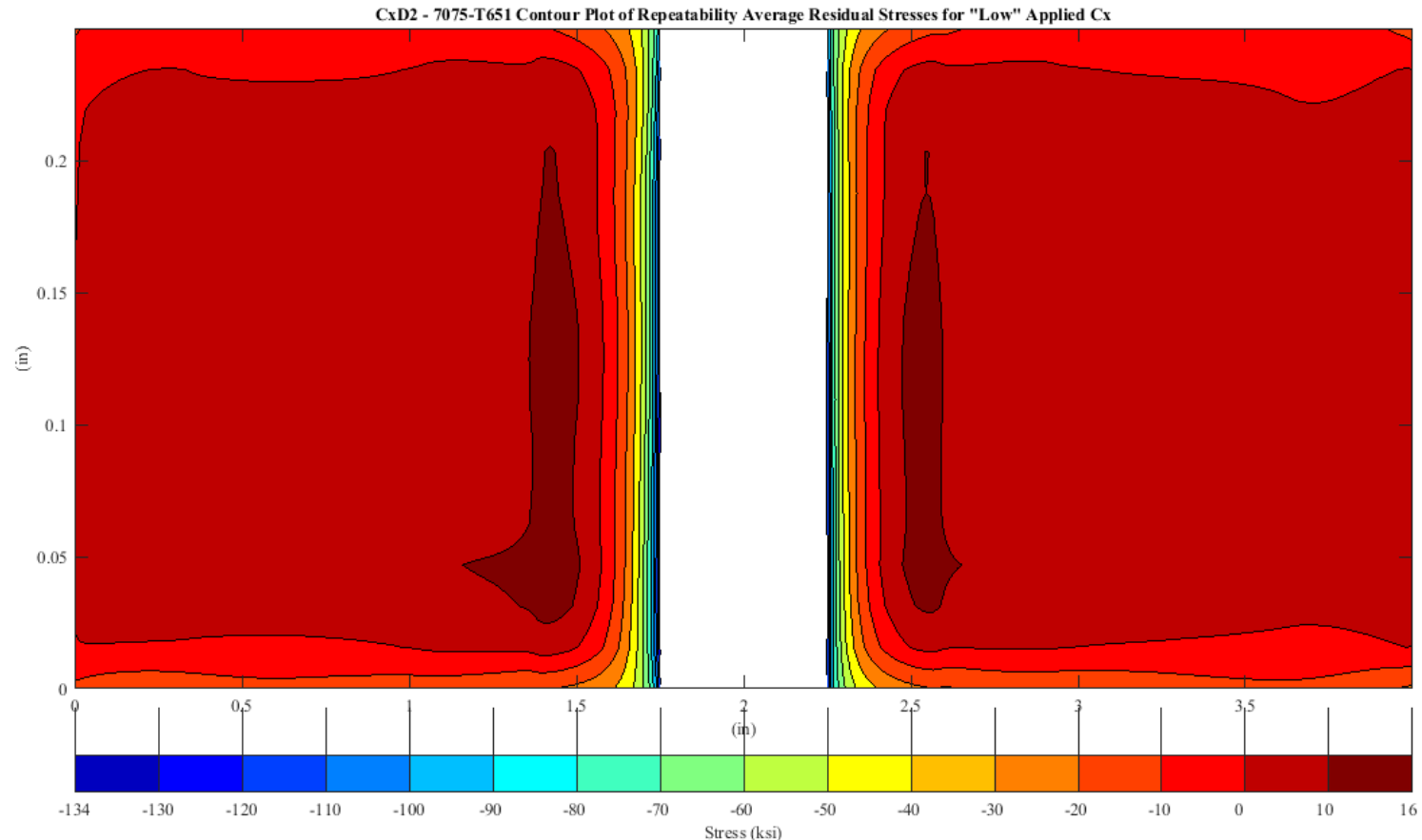
# Results of “Low” Applied Cx

- 3 Replicates Were Produced for the “Low” Applied Cx Level in Al 7075-T651, 0.25in Thick, Approx. 0.50inch Hole Diameter
  - The “low” applied expansion represents 3.23%
  - Initial hole diameter = 0.4767-0.4769in
  - Mandrel diameter = 0.4684in with sleeve thickness = 0.0120in
  - Avg. post Cx diameter = 0.4859-0.4862in
  - Residual expansion = 1.87%-1.92%



# Repeatability Uncertainty

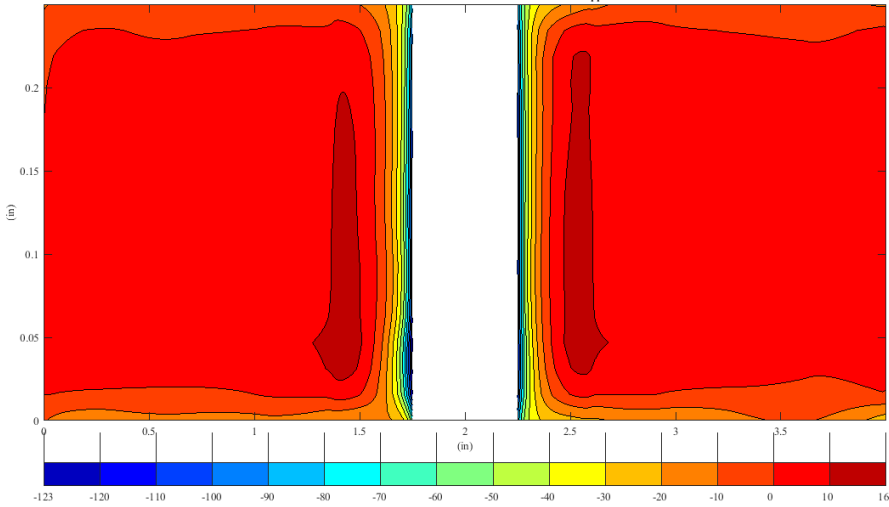
- From Replicate Conditions Each Contour Measurement was Performed Using Same Parameters
- Uncertainty of Single Standard Deviation from Mean



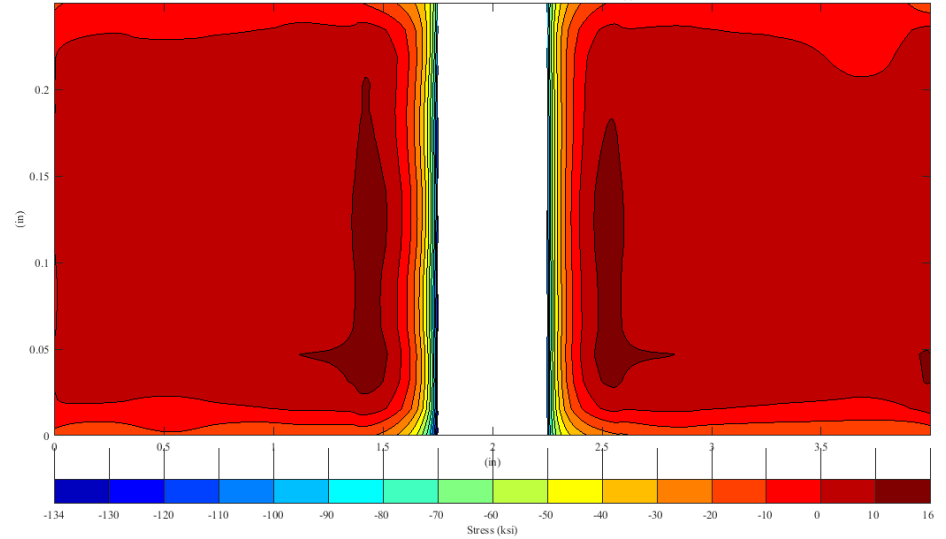


# Residual Stress Results for 7075

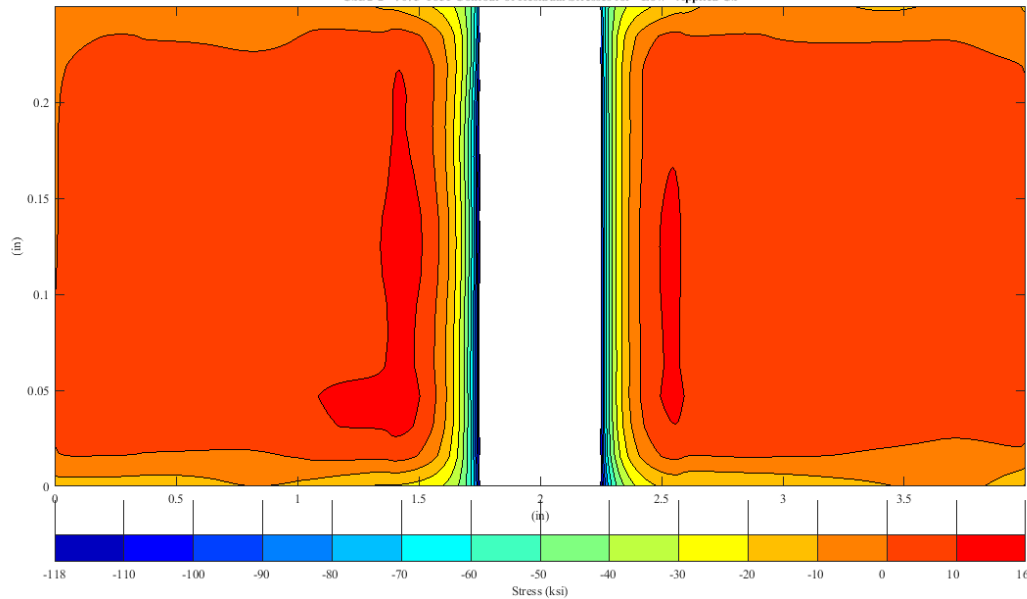
CxD2-1 - 7075-T651 Contour of Residual Stresses for "Low" Applied Cx



CxD2-3 - 7075-T651 Contour of Residual Stresses for "Low" Applied Cx

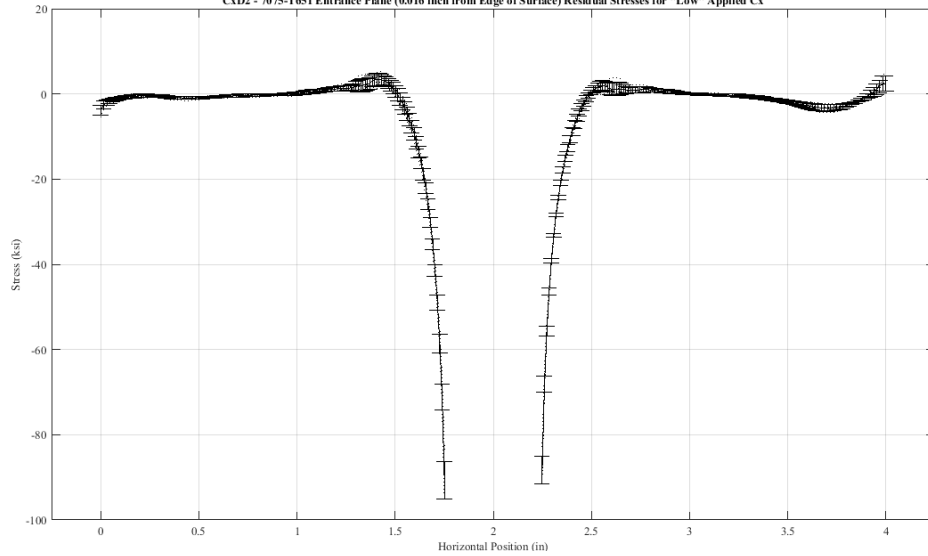


CxD2-2 - 7075-T651 Contour of Residual Stresses for "Low" Applied Cx

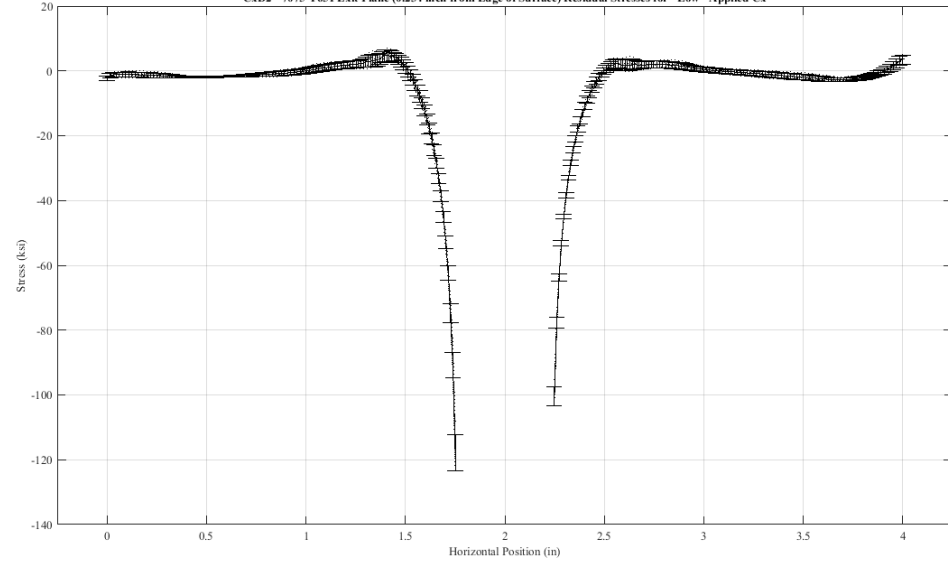


# Residual Stress Results for 7075

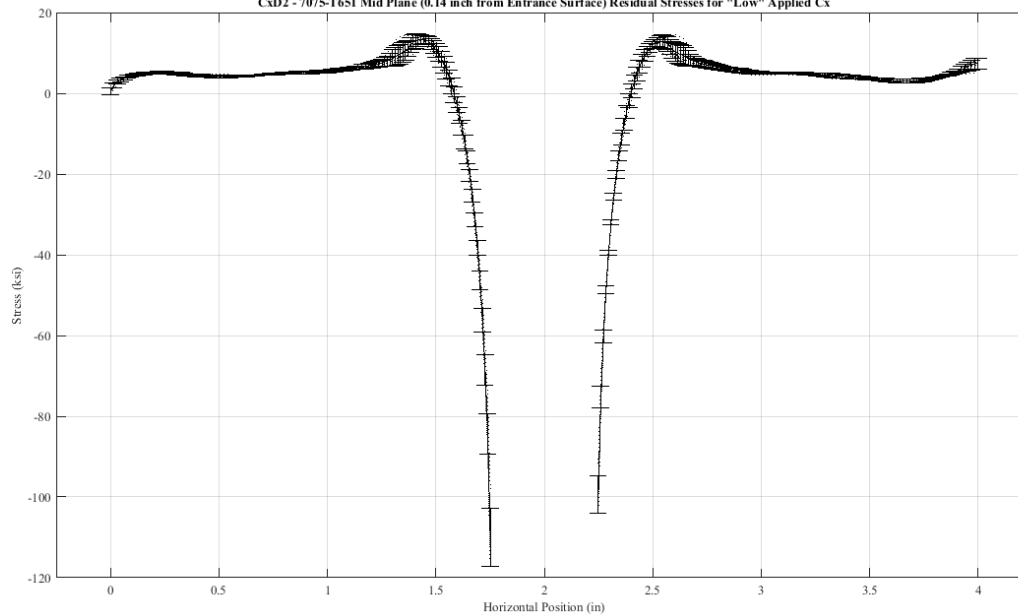
CxD2 - 7075-T651 Entrance Plane (0.016 inch from Edge of Surface) Residual Stresses for "Low" Applied Cx



CxD2 - 7075-T651 Exit Plane (0.234 inch from Edge of Surface) Residual Stresses for "Low" Applied Cx

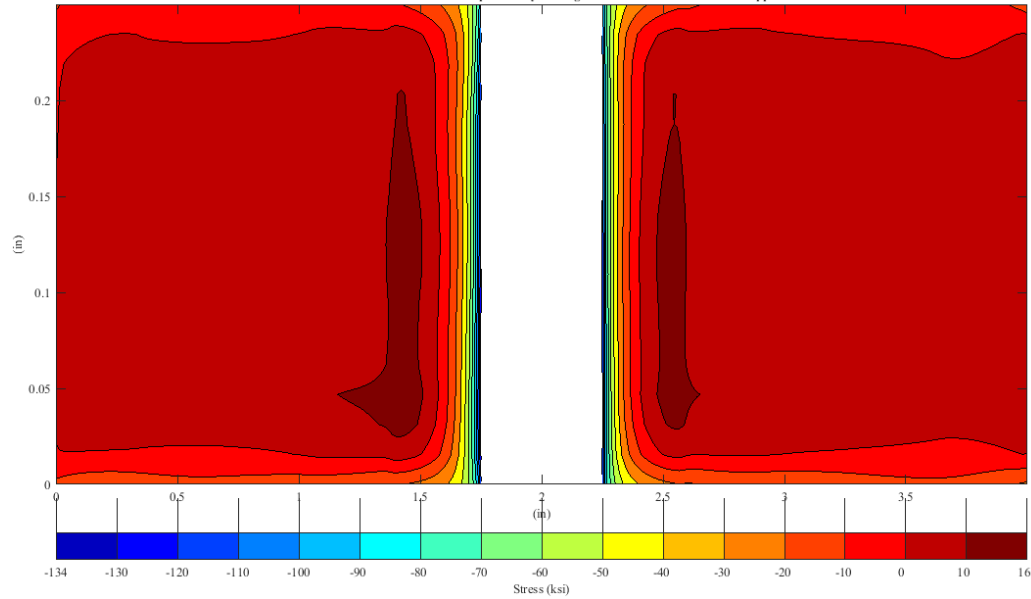


CxD2 - 7075-T651 Mid Plane (0.14 inch from Entrance Surface) Residual Stresses for "Low" Applied Cx

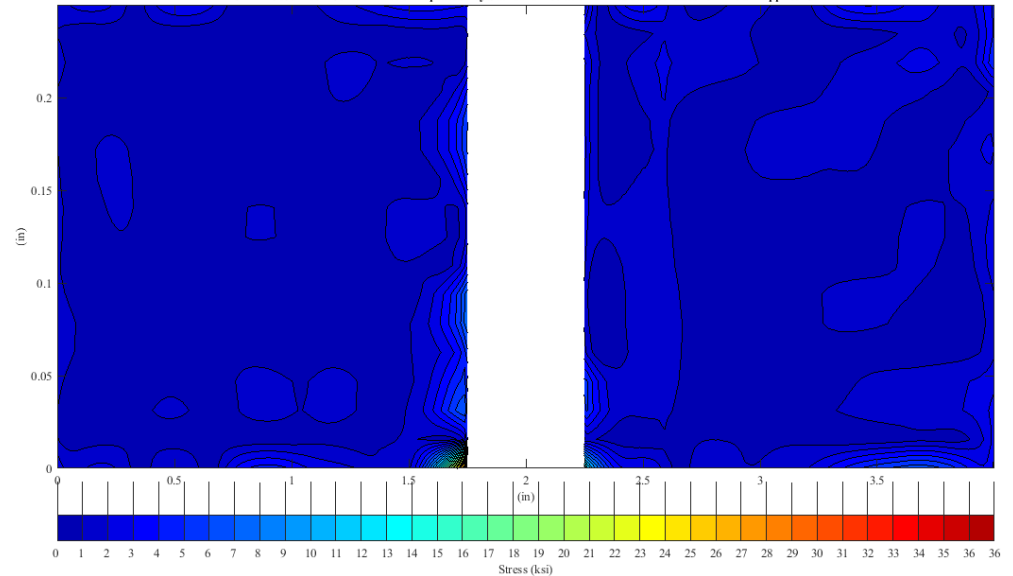


# Average & Standard Deviation

CxD2 - 7075-T651 Contour Plot of Repeatability Average Residual Stresses for "Low" Applied Cx



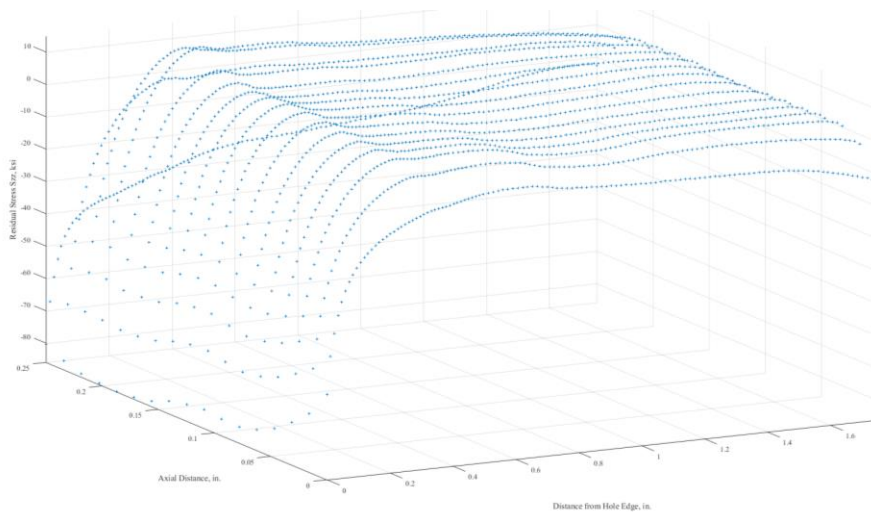
CxD2 - 7075-T651 Contour Plot of Repeatability Standard Deviation of Residual Stresses for "Low" Applied Cx



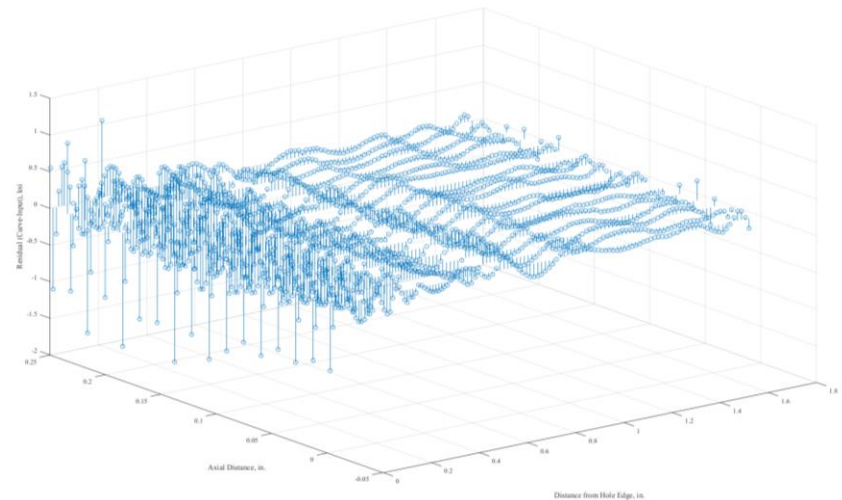
# Crack Face Traction Function Developed

- Each Side Averaged Together for One Stress Field
- 15<sup>th</sup> Order Polynomial Used to Fit Residual Stress Field
- Optimized to Have <1ksi Residual Between Fit and Data
- Function Placed in StressCheck<sup>®</sup> Model for BAMF

Polynomial Function Fit to Residual Stress Field

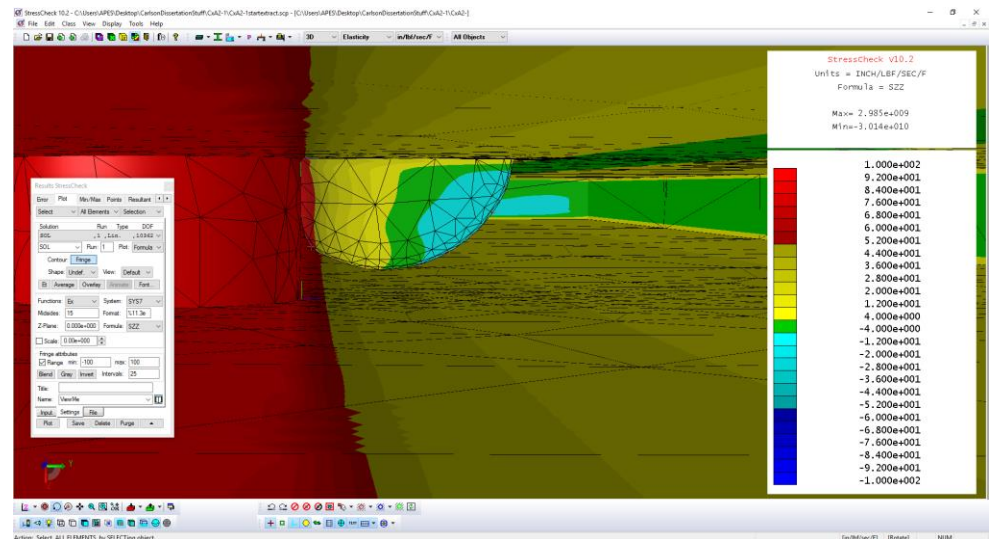
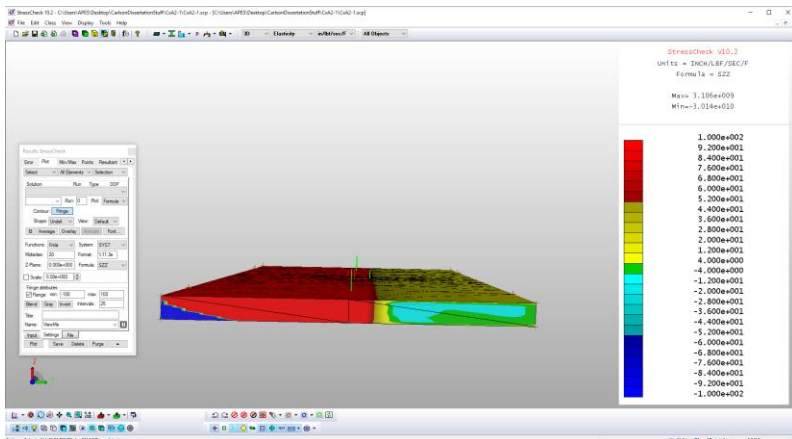


Residuals Between Fit and Actual



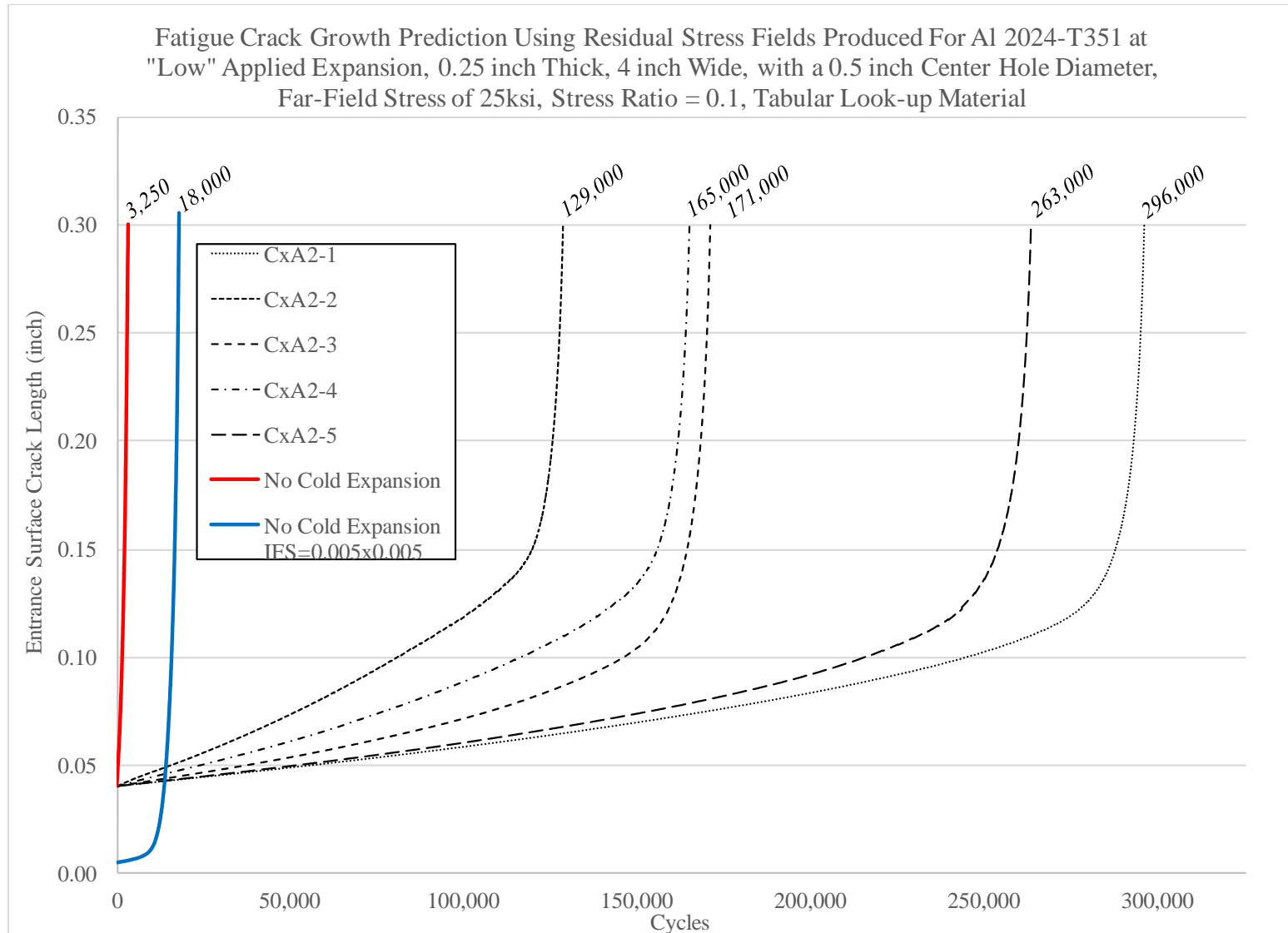
# Application of MUCMUP BAMF

- Function Inserted at Crack Face as a Traction
- Material File for 2024-T351 – Tabular Look-up File
- Material File for 7075-T651 – Forman Equation
  - Extrapolated  $\Delta K$  low to 0.001
- Loading – 25ksi, R=0.1
- All Cracks Nucleated on Entrance Side of Hole
- IFS for 2024 approx.  $0.05 \times 0.05$ , 7075 was  $0.075 \times 0.075$



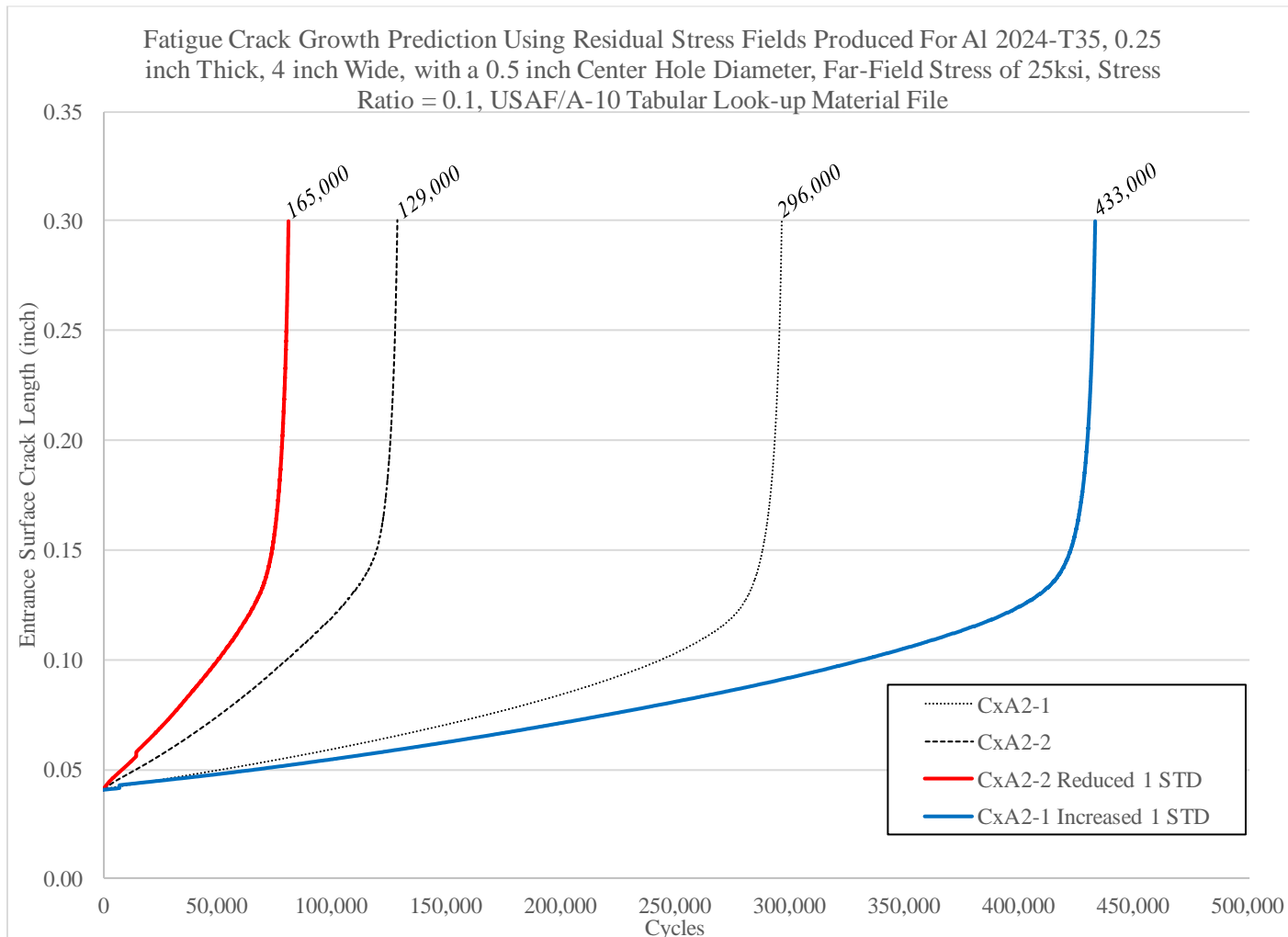
# Fatigue Life Predictions

- All 2024-T351 Residual Stress Fields



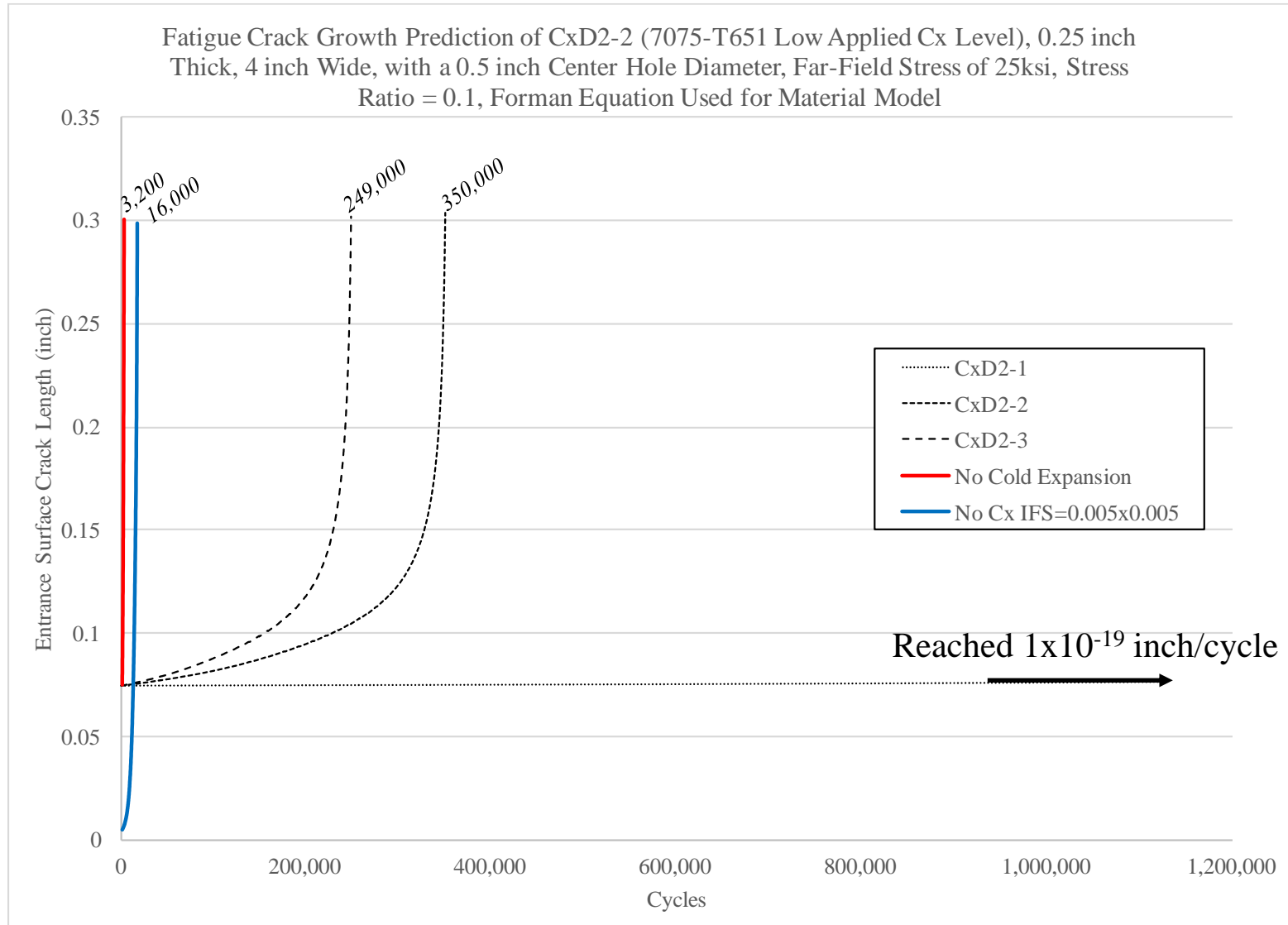
# Fatigue Life Predictions

- Adjust Shortest and Longest Life Residual Stress Fields by 1 Standard Deviation



# Fatigue Life Predictions

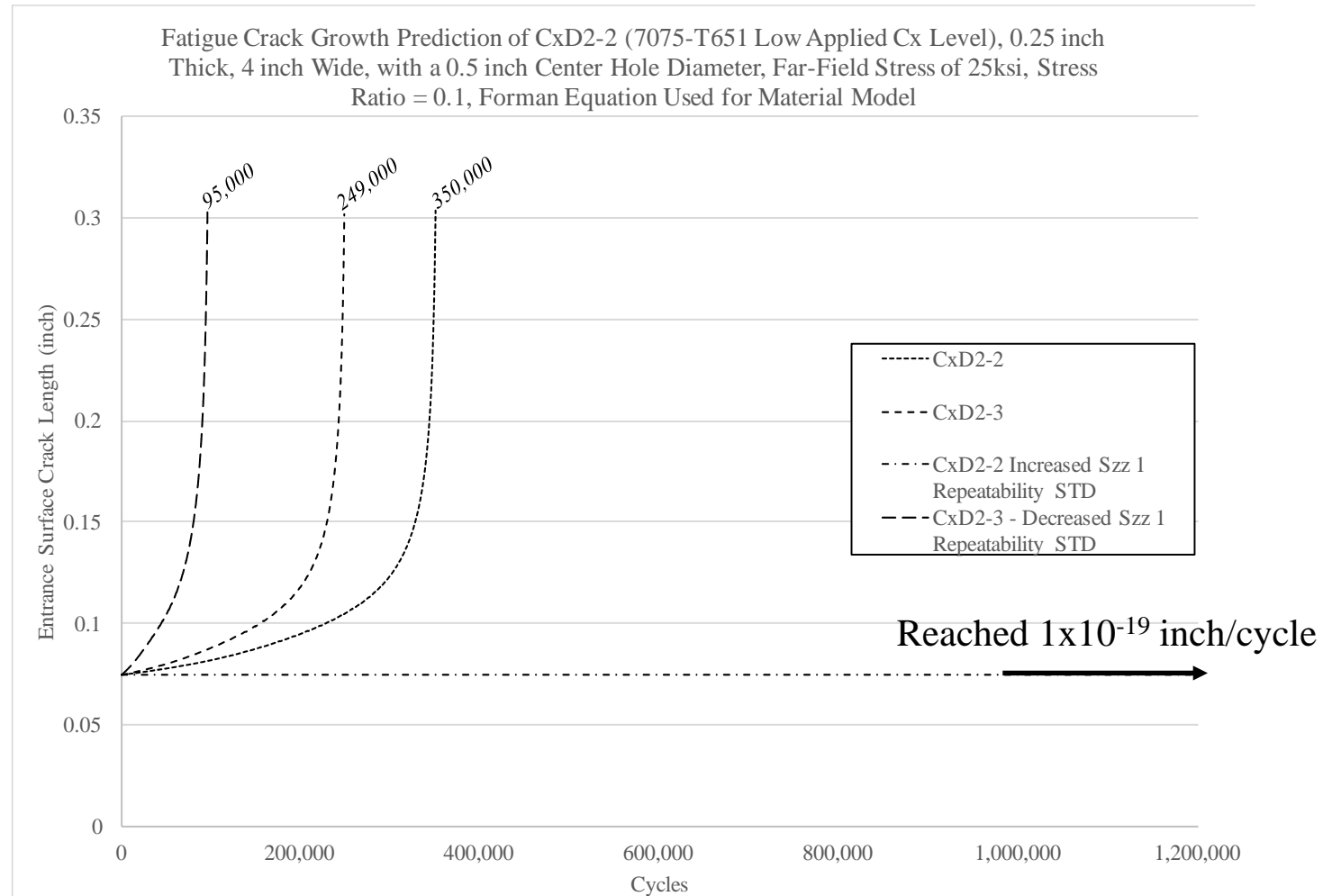
- All 7075-T651 Residual Stress Fields





# Fatigue Life Predictions

- Adjust Shortest and Longest Life (that would run)  
Residual Stress Fields by 1 Standard Deviation



# Single Measurement Uncertainty

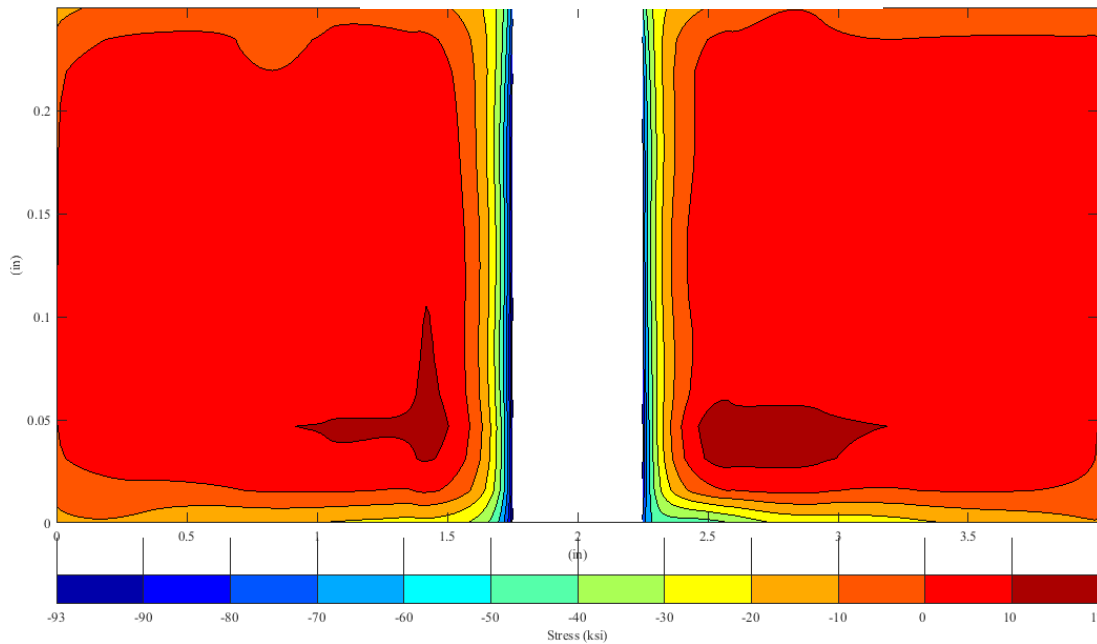
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- Application of Single Measurement Uncertainty
  - Adjust knot density along short and long side from optimal knot density
    - Short side knot density = 4
    - Long side knot density = 4
    - Adjusted knot densities for short and long sides 3-4, 4-3, 4-4, 4-5, 5-4
    - Total of 5 individual data reductions performed
  - Performed Monte Carlo simulation of optimal condition with added, normally distributed “Noise” to averaged-smooth displacement surface
    - Noise represents “the inherent surface roughness of the EDM cuts as well as the measurement error present in the displacement measurement signal.”<sup>4</sup>
    - Convergence criteria – 50 simulations were performed

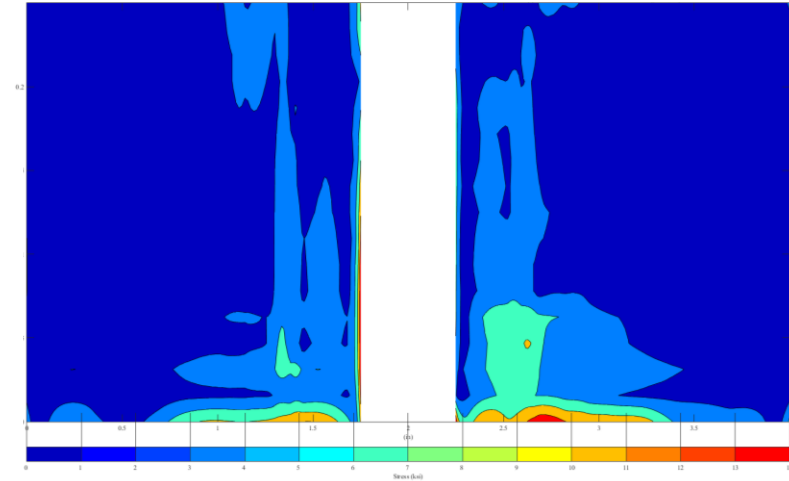
# Total Single Measurement Uncertainty

- 2024-T351 Measurement for A2-1
  - 1<sup>st</sup> 2024-T351 part measured

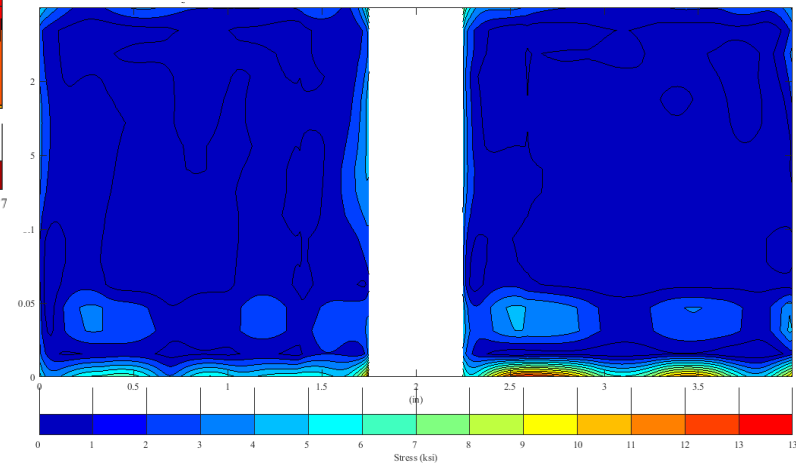
Measured Residual Stress



Single Measurement Uncertainty

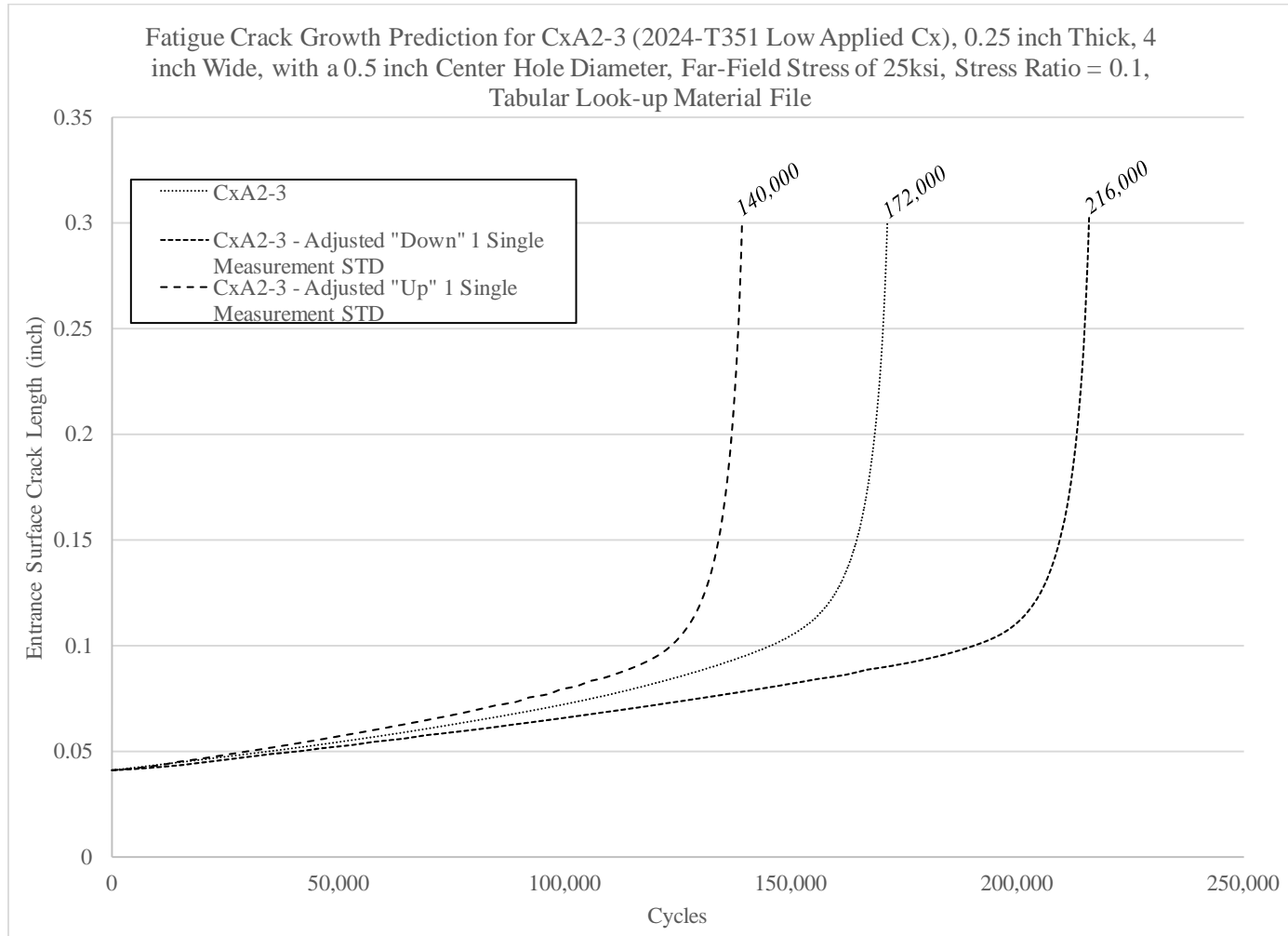


Repeatability Uncertainty



# Impacts to Fatigue Life Predictions

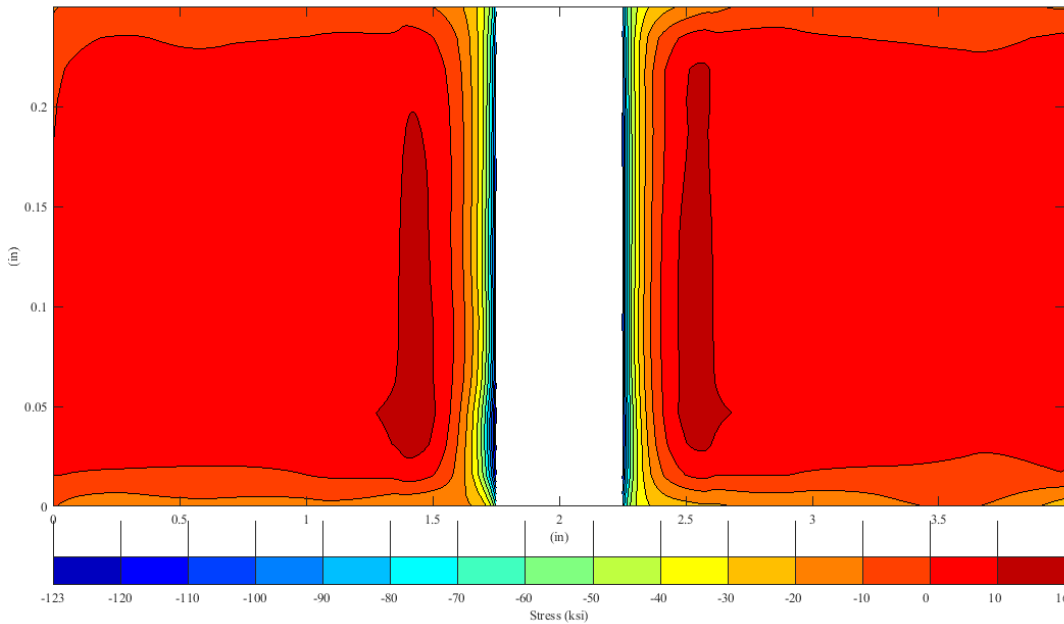
- 2024-T351 Measurement for A2-1
  - Adjusted A2-1 residual stress field “up” and “down” one STD



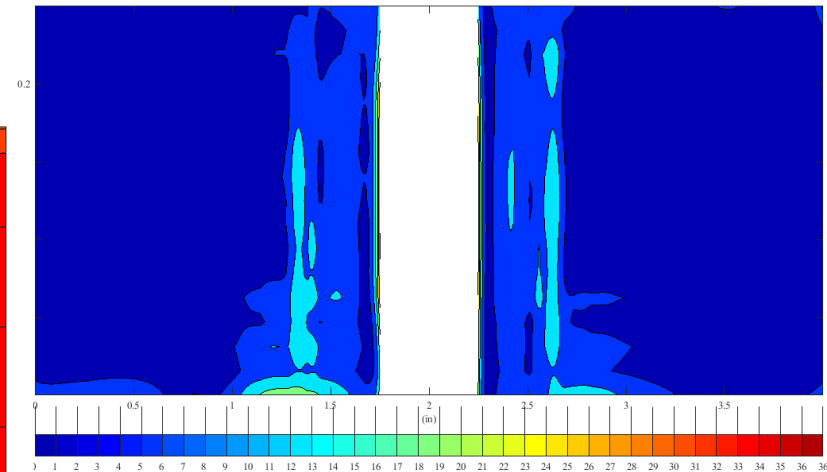
# Total Single Measurement Uncertainty

- 7075-T651 Measurement for D2-1
  - 1<sup>st</sup> 7075-T651 part measured

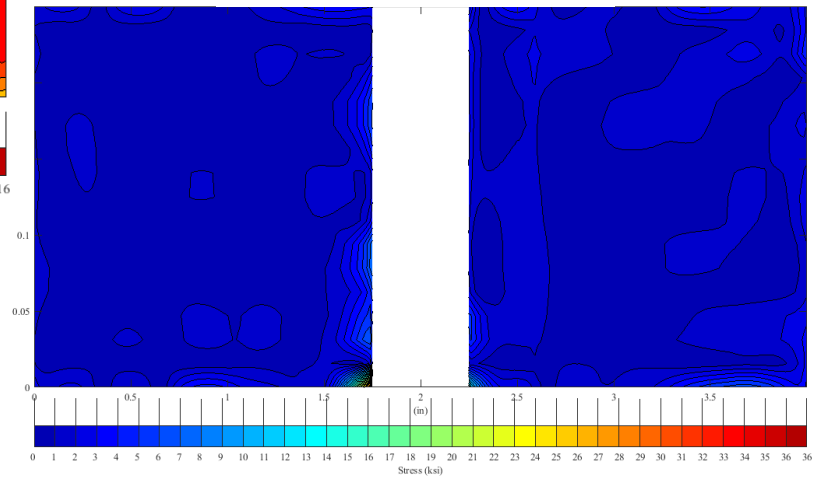
Measured Residual Stress



Single Measurement Uncertainty

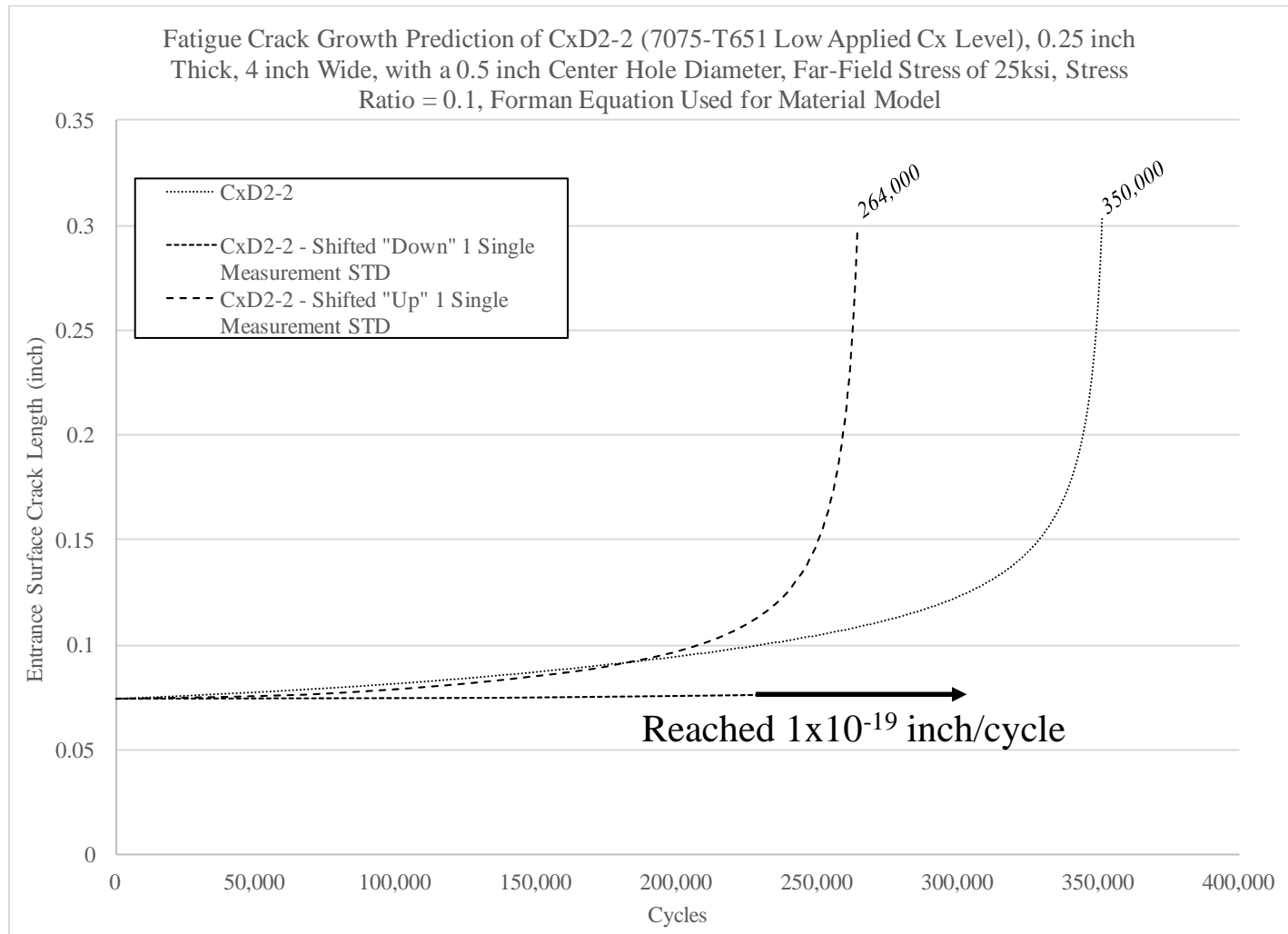


Repeatability Uncertainty



# Total Single Measurement Uncertainty

- 7075-T651 Measurement for D2-1
  - Adjusted D2-1 residual stress field “up” and “down” one STD



# Conclusions from Repeatability UQ

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- Higher Levels of Uncertainty are Found at "Near-Surface" and Very "Local" Locations
  - Range of repeatability uncertainty for 2024-T351 = <1 – 13ksi
  - Range of repeatability uncertainty for 7075-T651 = <1 – 36ksi
- Effect of Shift of Repeatability STD on Fatigue Life Prediction
  - 2024-T351 life prediction range from 165,000 – 430,000 cycles
  - 7075-T651 life prediction range from 95,000 cycle – infinite life

**Important Note: All BAMF Runs with 7075-T651 Tabular Look-up Files Produced Infinite Life – Why Forman Equation was Used – Provides a Starting Point for Life Predictions – Work Continues**

# Conclusions from Single Measurement UQ

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- Magnitudes of Uncertainty Similar to Repeatability  
Uncertainty
  - Total uncertainty driven by “Modeling” uncertainty
  - “Displacement” uncertainty symmetric around hole
- Locations of Peaks Not the Same
- Effect of Shift of Repeatability STD on Fatigue Life  
Prediction
  - 2024-T351 life prediction range from 140,000 – 216,000 cycles
    - Starting life cycle number = 172,000 cycles
  - 7075-T651 life prediction range from 264,000 cycle – infinite life
    - Starting life cycle number = 350,000 cycles



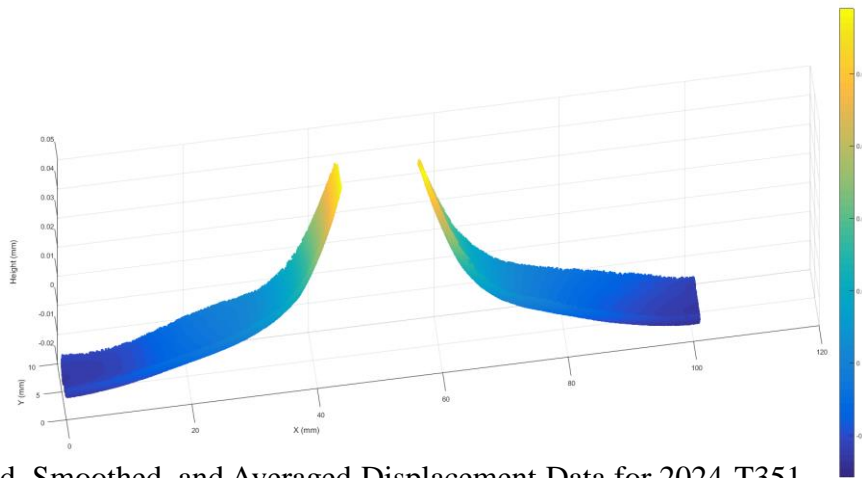
# General Conclusions

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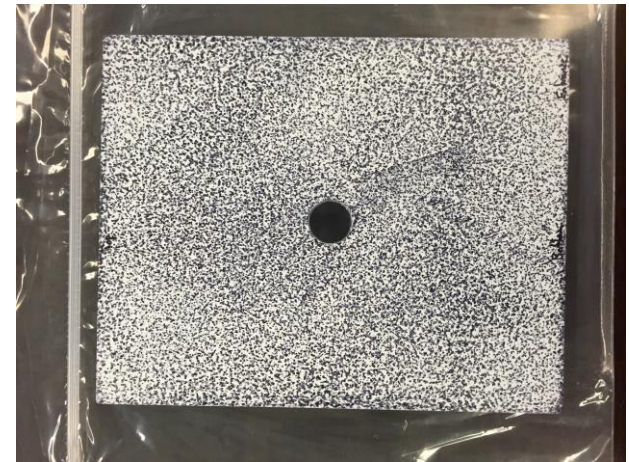
- Single Measurement does not Capture Breadth of Uncertainty Seen in Repeatability Uncertainty
  - Looks like it's better to have multiple measurements
- Single Measurement and Repeatability are Statistically Not Equal and are Independent via Chi-Squared Test
  - Potential to combine to capture uncertainty associated with Cx process and data reduction process “contour method”
- Confirming Independence via Hypothesis Testing on Differences of Means
- Repeatability Shifts of STD Create Greater Difference in Fatigue Life Predictions
- 7075-T651 is More Sensitive to these Shifts
  - Material model is a problem now – working on that

# Questions Unanswered

- Large Displacements Along Entrance and Exit Surfaces
  - Potentially due to plane stress/plane strain effect from cutting



Aligned, Smoothed, and Averaged Displacement Data for 2024-T351, CxA2-1



- Potential use of DIC to “Correct” for Surfaces
  - Causes higher compressive residual stresses than expected



# Inter-Laboratory Cx Work

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- Working to Have Multiple Labs Perform Residual Stress Measurement of Cx Condition
  - Does data processing methods make significant impact?
  - Does cutting methods cause significant impact on stress results?
- Working with 5 Labs for Inter-Laboratory Data Reduction of 4-Pt. Bend Condition<sup>7,8</sup>
  - Coupons tested at SwRI, cut at Hill Eng. LLC.
  - Data sent to individuals at Hill Eng., Los Alamos Labs, StressMap (UK), Hill AFB, Hydro-Quebec Research Institute
  - Is not trying to capture cutting and displacement measurement errors
- Need to Provide Users with Understanding of Uncertainty if Contract goes to “*Lowest Cost, Technically Acceptable*”
- Potential to have Inter-Laboratory Total Uncertainty “Too High” – Would Limit Usefulness of Method

# Future Work

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- Quantification of Total Uncertainty is Essential for Future Work
  - Enables confidence in isolating out effect being investigated
- Effect of a Fatigue Crack on the Residual Stress Field
- Effect of Peak Compression Cycles on Residual Stress Field
- Effect of Steel Pin Installation During Cyclical Loading
- Effect of Bearing & Bypass Loading
- Application of DIC for Measurement of Strain/Stress During Cx-Through-Testing-Crack Propagation Process
  - Look to correlate to Contour Method data
  - Potential for surface correction to improve Contour Method data
- Integrate all Aspects into Fatigue Life Prediction at Critical Airframe Locations Across Fleet - USAF-wide

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# Questions?



# References

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2. Bueckner, H., (1958). “The Propagation of Cracks and the Energy of Elastic Deformation”, *Transactions of the American Society of Mechanical Engineers*, Vol. 80, pg. 1225-1230.
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